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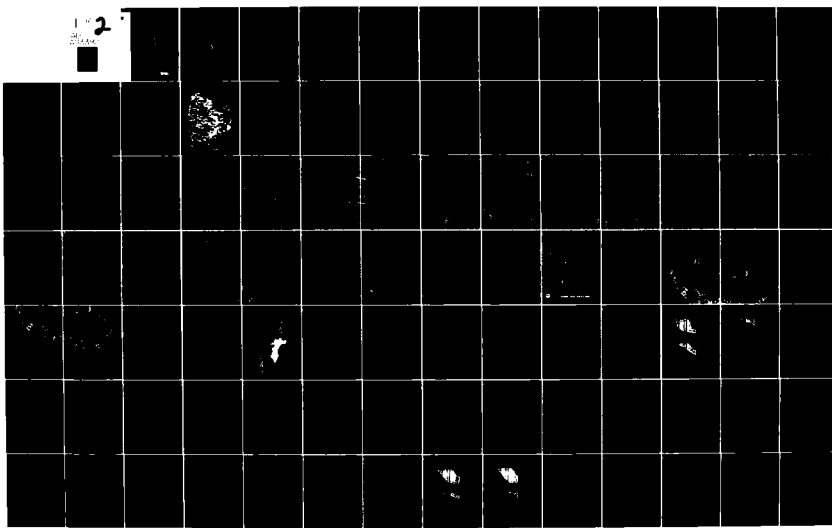
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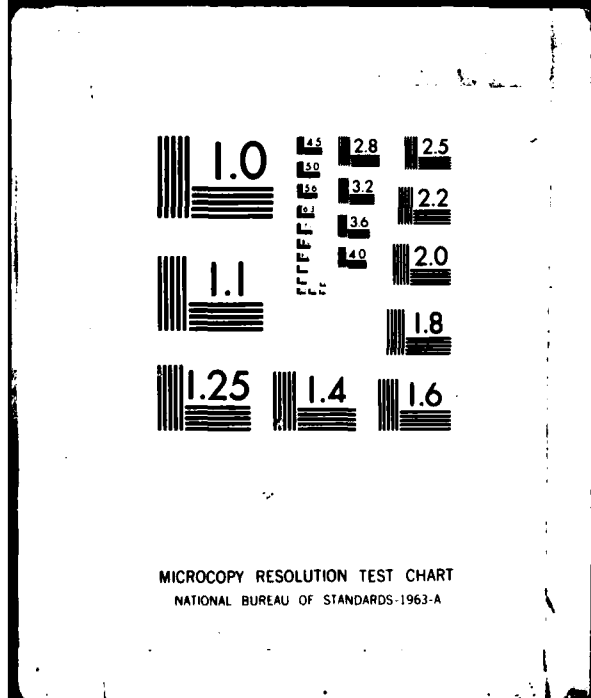
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**MX SITING INVESTIGATION
GEOTECHNICAL EVALUATION**

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**VERIFICATION STUDY
WAH WAH VALLEY, UTAH
VOLUME I - SYNTHESIS**

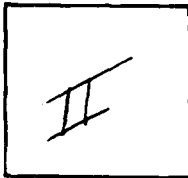
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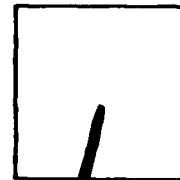
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| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report presents the results of the geotechnical studies which were conducted in Wah Wah Valley, Utah. Included are base data consisting of depth to rock, depth to water, seismic refraction surveys, electrical resistivity surveys, boring and trench logs, and soil profiles. | | |

FOREWORD

This report was prepared for the U.S. Department of the Air Force, Ballistic Missile Office (BMO), in compliance with Contract No. F04704-80-C0006, CDRL Item 004A6. It contains an evaluation of the suitability of Wah Wah Valley, Utah for siting the MX Land Mobile Advanced ICBM system and presents the geological, geophysical, and soils engineering data upon which the evaluation is based. It is one of a series of reports covering the results of Verification studies in the Nevada-Utah region.

Verification studies, which were started in 1979, are the final phase of a site selection process which was begun in 1977. The Verification objectives are to define sufficient area suitable for deployment of the MX system and to provide preliminary soils engineering data. Previous phases of the site selection process were Screening, Characterization, and Ranking. In preparing this report, it has been assumed that the reader will be familiar with the previous studies.

Volume I of this report is a synthesis of the data obtained during the study. It contains discussions relative to the horizontal and vertical shelter basing modes. Volume II is a compilation of the data which may be used for independent interpretations or analyses.

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1.0 INTRODUCTION

1.1 PURPOSE AND BACKGROUND

This report presents the results of the geotechnical studies which were conducted in Wah Wah Valley, Utah, during the summer of 1980. The work was done as part of Fugro National Inc.'s (FNI) Verification studies which have two major objectives:

1. Verify and refine suitable area boundaries for two proposed basing modes (horizontal and vertical shelter) for the MX missile system; and
2. Provide preliminary physical and engineering characteristics of the soils.

The report contains two volumes. This volume is a synthesis of the data collected during the studies. The data obtained as a result of the field and laboratory work are compiled by activity in Volume II.

The Verification program is the final phase of a site-selection process which started in 1977. The objective of the site-selection process is to identify and rank geotechnically suitable areas which are sufficiently large for deployment of the Missile-X (MX), an advanced intercontinental ballistic missile system. The phases are called Screening, Characterization, Ranking, and Verification. Screening used existing information from literature to identify areas which appeared to be suitable for deployment of MX based on geotechnical, cultural, and environmental criteria. Potentially usable regions were identified in seven western states. Both Characterization and Verification

programs use field studies as well as published information. Following Screening and Characterization, the available geotechnical data were used to rank the seven regions. The ranking, based on relative construction costs, was made for various basing modes. Characterization studies emphasized collection of information to characterize geologic units with respect to construction of the MX basing options. Verification studies also obtain information on construction properties of the geologic units, but special emphasis is given to refining the usable area boundaries that were drawn during the Screening studies. The investigative techniques being employed during Verification studies are summarized in Table 1-1.

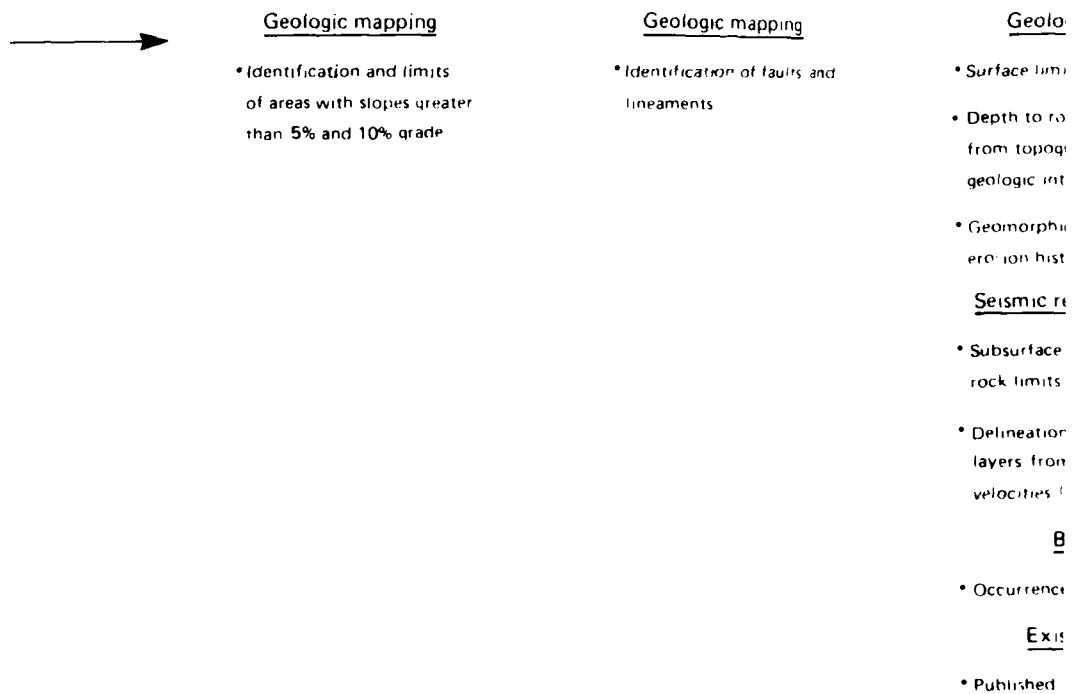
Figure 1-1 shows the site-selection schedule and identifies the FNI technical report for each element in the process. Based on the results of Screening, Characterization, and Ranking, contiguous portions of Nevada and Utah were selected as a candidate siting region for the MX system, and Verification studies were started in 1978. As shown, the Verification program is continuing, and field work should be completed in 1981. The areas for which reports have been issued on the Verification studies are shown in Figure 1-2. The present usable area boundaries for the Nevada-Utah siting region are shown in Drawing 1-1. The boundaries will be adjusted as Verification studies are completed.

1.2 SCOPE OF STUDY

The field work in Wah Wah Valley was done in 1980. Table 1-2 lists the types and number of field activities that were



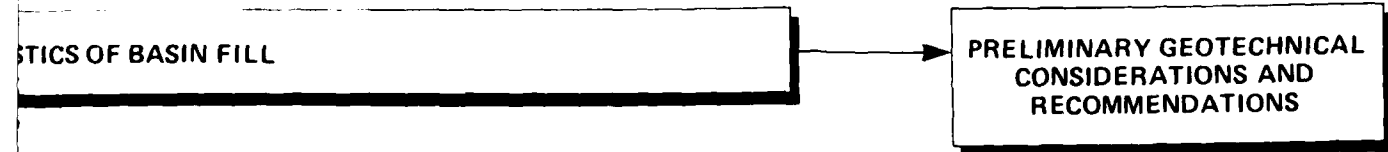
FIELD TECHNIQUES AND APPLICATIONS





| | | | |
|--|--|---|--|
| <u>Geologic mapping</u> • Surface limits of rock • Depth to rock • From topographic and geologic interpretation • Morphologic expression and erosion history <u>Seismic refraction surveys</u> • Subsurface projection of rock limits • Delineation of high velocity layers from p-wave velocities (> 7000 fps) <u>Borings</u> • Occurrence of rock <u>Existing data</u> • Published literature | <u>Geologic mapping</u> • Obtain water depths from wells in study area <u>Borings</u> • Occurrence of ground water <u>Electrical resistivity seismic refraction surveys</u> • Provide supplemental data to support presence or absence of ground water <u>Existing data</u> • Published literature | <u>Geologic mapping</u> • Extent of surficial soil units • Surficial soil types <u>Borings</u> • Identification of subsurface soil types • In situ soil density and consistency • Samples for laboratory testing <u>Trenches and test pits</u> • Identification of surface and subsurface soil types • Degree of induration and cementation of soils • In situ moisture and density of soil • Samples for laboratory testing <u>Cone penetrometer tests</u> • In situ soil strength <u>Laboratory tests</u> • Physical properties • Engineering properties - shear strength, compressibility • Chemical properties | <u>Seismic refraction surveys</u> • Compressional wave velocities • Layering of soil <u>Electrical resistivity surveys</u> • Electrical conductivity of soil • Layering of soil |
|--|--|---|--|

2



ROAD DESIGN DATA

EXCAVATABILITY AND STABILITY

Trenches and test pits

- Identification of soil types
- In situ soil density and moisture
- Cone penetrometer tests
- In situ soil strength
- Thickness of low strength
- Surface soil

Laboratory tests

- Physical properties
- Compaction and CBR data
- Suitability of soils for use as road subgrade, subbase or base

Existing data

- Suitability of soils for use as road subgrade, subbase, or base
- Behavior of compacted soils

Borings

- Subsurface soil types
- Presence of cobbles and boulders
- In situ density of subsurface soils
- Stability of vertical walls

Trenches and test pits

- Subsurface soil types
- Subsurface soil density and cementation
- Stability of vertical walls
- Presence of cobbles and boulders

Laboratory tests

- Physical properties
- Engineering properties

Geologic mapping

- Distribution of geologic units

Seismic refraction surveys

- Excavatability

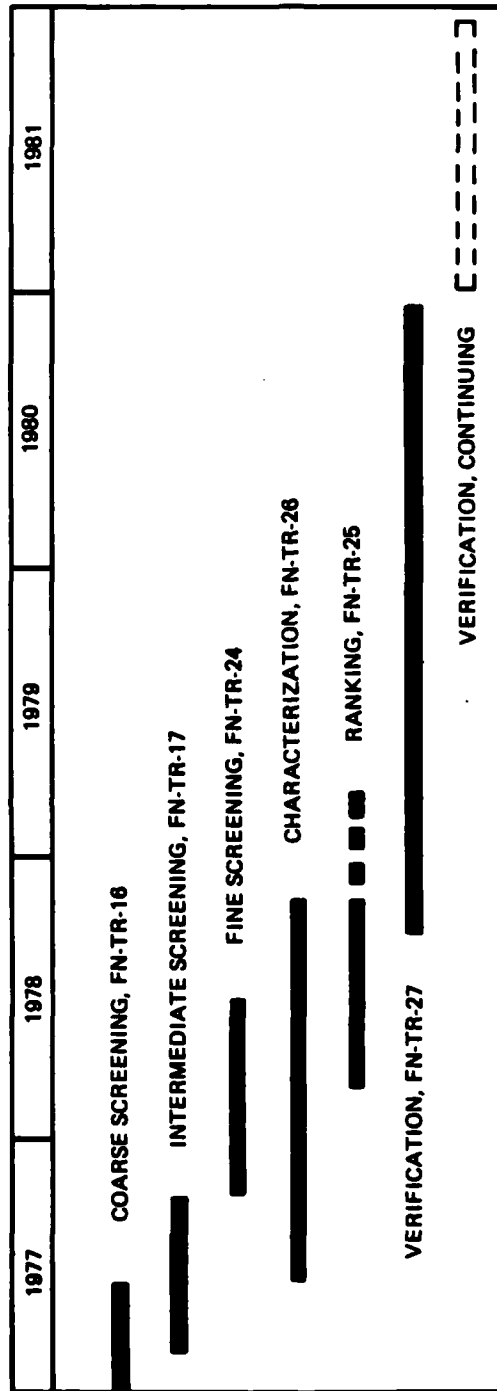
FIELD TECHNIQUES VERIFICATION STUDIES

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - DMO

TABLE

11

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SUMMARY OF SITE-
SELECTION SCHEDULE

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SMO

FIGURE
1-1

FUGRO NATIONAL, INC.

GEOLOGY AND GEOPHYSICS— FIELD ACTIVITIES

| TYPE OF ACTIVITY | NUMBER OF ACTIVITIES |
|---------------------------|-------------------------|
| Geologic mapping stations | 73 |
| Shallow refraction | 21 |
| Electrical resistivity | 21 |

ENGINEERING—LABORATORY TESTS

| TYPE OF TEST | NUMBER OF TESTS |
|------------------------|--------------------|
| Moisture/density | 147 |
| Specific gravity | 7 |
| Sieve analysis | 146 |
| Hydrometer | 7 |
| Atterberg limits | 50 |
| Consolidation | 1 |
| Unconfined compression | 2 |
| Triaxial compression | 12 |
| Direct shear | 7 |
| Compaction | 16 |
| CBR | 16 |
| Chemical analysis | 10 |

ENGINEERING—FIELD ACTIVITIES

| ACTIVITY | NO. | NOMINAL DEPTH - FEET (METERS) |
|-------------------------|-----|-------------------------------------|
| Borings | 1 | 200 (61) |
| | 3 | 160 (49) |
| | 1 | 153 (47) |
| | 2 | 54 (16) |
| Trenches | 13 | 10-14 (3-4) |
| | 7 | 3-9 (1-3) |
| Test pits | 19 | 5 (2) |
| | 1 | 2.5 (1) |
| Surficial soil samples | 24 | 3 (1) |
| | 8 | 2 (1) |
| Cone Penetrometer Tests | 72 | 1-55 (0.3-17) |
| Field CBR tests | 8 | 1-4 (0.3-1) |

SCOPE OF ACTIVITIES WAH WAH VALLEY, UTAH

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - BMO

TABLE
1-2

FUGRO NATIONAL, INC.

performed in Wah Wah Valley. The techniques of investigation are discussed in the appendix.

Access to public lands in Wah Wah Valley was arranged through the Richfield and Cedar City, Utah, district offices of the Bureau of Land Management (BLM) and the Utah Division of State Lands and Forestry. At their request, all field activities were performed along existing roads or trails to minimize site disturbance. In some cases, this restriction prevents distributing activities in an optimum pattern for analysis of geotechnical conditions. Archaeological and environmental surveys were performed at each proposed activity location. Activity locations were moved from those few places where a potential environmental or archaeological disturbance was identified.

1.3 DISCUSSION OF ANALYSIS TECHNIQUES

1.3.1 Determination of Suitable Area

The number of field activities performed during this investigation established a relatively small data base for characterizing such a large area, especially in view of its complex geology and frequent soil variations. In some cases, the environmental restrictions limited the ability to achieve an optimum distribution of data points. Nevertheless, care has been taken to optimize the information that could be obtained within specified cost and time constraints of the project. The determination of suitable area is based on the exclusion criteria given in Appendix A2.0. The main attention was focused on the study of depth to rock, depth to water, terrain conditions, and near-surface soil characteristics. Maps showing the results of these

studies are included in Section 3.0 and the composite map of suitable area is included in Section 2.0.

a. Depth to rock: For a Verification study, the depth to rock is estimated, and areas where the depths are less than 50 and 150 feet (15 and 46 m) are outlined by contours (Drawing 3-3). These contours are interpreted from published well data, geologic literature, boring logs, and geophysical data. The interpretation considers the presence or absence of range-bounding faults, bedding plane attitudes, topographic slopes, evidence of erosional features such as pediments, and the presence or absence of young volcanic rocks.

b. Depth to Water: The depth-to-water map (Drawing 3-4) is based on data from wells listed in Table II-2-1 (Volume II). Data compiled in Table II-2-1 came from: FNI water resources program wells, well logs on file with the State of Utah Engineer's Office, and literature describing the valley hydrology. Whenever possible, the depth to water listed for a well represents the depth to the first, shallow water-bearing zone, not the static water level. Static levels can be higher than first-encountered water depths, since many valleys contain artesian aquifers for which the static water level is above the aquifer. The well data are plotted on a map and used to define the 50- and 150-foot- (15- and 46-m-) depth-to-water contours.

c. Terrain: The terrain map (Drawing 3-5) was compiled to show areas unsuitable for either vertical or horizontal shelters due to either high surface slopes or frequent deep drainage

incisions (criteria are described in Appendix Table A2-1). The interpretation of terrain exclusions is based on a combination of field- and office-derived data. Field data include the visual information obtained by visiting the areas and making measurements of typical drainage incision depths. Visits frequently result in recognition of areas with locally steep slopes (for example, the sides of large and deeply incised drainages) that are not recognizable from data available in the office. Office-determined data consist of: 1) interpretation of 1:60,000-scale black and white and 1:25,000-scale color aerial photographs to determine terrain exclusions in areas lacking road access; and 2) topographic map analysis to define areas of greater than 10 percent slope.

d. Faults: The faults shown on the geologic map (Drawing 3-2) are primarily mapped from high resolution photogeologic studies and field reconnaissance. These faults are primarily Quaternary age but some late Tertiary faults may also be included. Generally, those within alluvial deposits are of Quaternary age. The faults shown within rocks in the mountain blocks or at the mountain-valley contact are of unknown age but are almost certainly of late Tertiary and/or Quaternary age and have been active under the present tectonic regime. Published maps show numerous other faults within the rocks of the mountain blocks, and some of these also may have been active under the present tectonic regime. Since they are not within the siting areas, they have not been studied. The published maps also show

numerous inferred faults buried under the alluvium along the mountain-valley contacts. These faults are commonly verified by geophysical studies and may represent earthquake hazards. Since they have no surface expression, they cannot be verified by the reconnaissance methods employed in the fault studies.

1.3.2 Determination of Basin-Fill Characteristics

In addition to the primary objective of refining suitable area boundaries, a secondary objective was to provide preliminary physical and engineering properties of the basin-fill materials. These data will be used for preliminary engineering design studies, will assist in planning future site-specific studies, and will be used by other MX participants.

The geologic map (Drawing 3-2) showing the distribution of surficial soils is based on the interpretation of aerial photographs, field mapping, and information from trenches, test pits, and surficial soil samples.

The investigations of engineering properties were designed primarily to obtain information needed for construction activities. For Verification studies, surficial soil conditions as related to road construction, a major cost item, received particular emphasis. Emphasis was placed also on soil conditions in the upper 20 feet (6 m) to provide information to the approximate depth of excavation for the horizontal shelter basing mode.

Data obtained from borings, trenches, test pits, seismic refraction lines and laboratory tests were used to estimate soil

properties to a depth of 20 feet (6 m). The data are limited since the field activities consisted of only 20 trenches, 20 test pits, seven borings, and 21 seismic lines. Seven of 20 trenches were less than 9 feet (2.7 m) deep because they encountered hard cementation and/or cobbles. There may be soil conditions in the upper 20 feet (6 m) that were not encountered by these 68 data points. The number of data points available for description of the surficial soils was increased to 172 by using 32 surface samples and 72 cone penetrometer (CPT) soundings.

The soil parameters between a depth of 20 and 160 feet (6 and 49 m) are based on data obtained from only seven borings. The spacing between borings ranged from 4 to 7 miles (6 to 10 km), therefore, the data presented may not be representative of the entire valley.

The length of the seismic refraction lines was chosen to investigate the velocity profile to a depth of at least 150 feet (46 m), which is the depth of interest for the vertical shelter basing mode.



FN-TR-27-WA-I

MX SITING INVESTIGATION
GEOTECHNICAL EVALUATION
VERIFICATION STUDY - WAH WAH VALLEY
UTAH
VOLUME I - SYNTHESIS

Prepared for:

U. S. Department of the Air Force
Ballistic Missile Office (BMO)
Norton Air Force Base, California 92409

Prepared by:

Ertec Western, Inc.
3777 Long Beach Blvd.
Long Beach, California 90807

24 March 1981

2.0 RESULTS AND CONCLUSIONS

2.1 SUITABLE AREA

The results of the interpretation of suitable area for Wah Wah Valley are listed in Table 2-1 and shown in map form in Drawing 2-1. The exclusion criteria used to make this interpretation are discussed in Appendix A2.0.

The total area of basin-fill materials in Wah Wah Valley is 320 square miles (mi^2) (829 square kilometers [km^2]). Twenty-five percent of this area is excluded for the horizontal shelter basing mode, leaving a suitable area of 241 mi^2 (624 km^2). For the vertical shelter basing mode, 38 percent of the total area is excluded, leaving 197 mi^2 (510 km^2) of suitable area.

2.2 BASIN-FILL CHARACTERISTICS

This section contains brief descriptions of the soils in Wah Wah Valley. More detailed information is presented in Sections 3.3 and 3.4.

2.2.1 Surficial Soils

Coarse-grained granular soils are the predominant surficial soils, covering approximately 80 to 90 percent of the area. They consist of sandy and silty gravels and gravelly, silty and/or clayey sands. Generally sandy gravels and gravelly sands occur sporadically along the mountain fronts. Cobbles and boulders are prevalent along the mountain fronts and particularly in the southern portion of the valley.

FN-TR-27-WA-I

| VERIFICATION VALLEY | STATE | AREA MI ² (KM ²) | | |
|------------------------|-------|---|---------------|-----------|
| | | BEGINNING AREA * | SUITABLE AREA | |
| | | | HORIZONTAL | VERTICAL |
| WAH WAH | UTAH | 320 (829) | 241 (624) | 197 (510) |

| EXCLUSIONS | AREA MI ² (KM ²) | PERCENT REDUCTION** |
|------------------------------|---|---------------------|
| < 50 FEET (15M) TO ROCK | 48 (124) | 15 |
| < 150 FEET (46M) TO ROCK | 85 (220) | 27 |
| < 50 FEET (15M) TO WATER | 13 (34) | 4 |
| < 150 FEET (46M) TO WATER | 24 (62) | 7 |
| TERRAIN | 18 (47) | 6 |

- BEGINNING AREA COMPOSED OF BASIN-FILL MATERIALS EXCLUDING ALL ROCK OUTCROPS. ALL LARGE SQUARE MILE AREAS ARE ROUNDED OFF TO NEAREST ONE SQUARE MILE INCREMENT. METRIC CONVERSIONS ARE ROUNDED OFF TO NEAREST ONE SQUARE KILO-METER INCREMENT.
- ** PERCENT REDUCTIONS, BASED ON BEGINNING AREA, ARE ROUNDED OFF TO NEAREST WHOLE PERCENT. GROUND WATER DATA FROM FUGRO NATIONAL, INC. (1979b).

ESTIMATED SUITABLE AREA
WAH WAH VALLEY, UTAH

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - BMO

TABLE
2-1

FUGRO NATIONAL, INC.

Downslope from the valley margins, the surficial soils grade to silty and/or clayey sands. The sands and gravels are generally poorly graded and have various degrees of calcium-carbonate cementation.

Fine-grained soils cover from 10 to 20 percent of the area. They consist of sandy silts, silts, sandy clays, and clays. The fine-grained soils are mainly in the active playa and at the edge of Sevier Lake in the northern portion of the valley. This playa is an active remnant of Lake Bonneville. Plasticity of the fine-grained soils ranges from nonplastic to highly plastic.

2.2.2 Subsurface Soils

Soils in the subsurface are also predominantly coarse-grained consisting of sandy gravels, clayey gravels, gravelly sands, sands, silty sands, and clayey sands. Gravels and gravelly sands commonly occur along the mountain fronts and grade to finer soils toward the valley axis. Cobbles and boulders occur throughout the southern portion of the valley and along the mountain fronts. The coarse-grained soils are generally dense to very dense below 10 to 15 feet (3.0 to 4.6 m) and are usually poorly graded. They contain gravel and/or coarse to fine sand, exhibit low compressibilities, and possess moderate to high shear strengths. Variation in the areal extent of playas in the geologic past has resulted in local interfingering of coarse- and fine-grained deposits in the subsurface near active playa margins. This occurs in the northern portion of the valley which has an active playa. Fine-grained soils (silts and

clays) are interpreted to occur in about 25 to 35 percent of the subsurface. These soils are generally associated with both exposed and buried lacustrine deposits in the northern portion of the valley. This relatively high percentage of fine-grained sediments indicates that lacustrine environments have been more extensive in Wah Wah than in most other valleys in the siting region. The fine-grained soils are nonplastic to highly plastic with low to moderate compressibilities and shear strengths. The highly plastic clays are predominant in the northern part of the valley. Variable calcium-carbonate cementation exists in all the subsurface soils throughout the valley.

2.3 CONSTRUCTION CONSIDERATIONS

Geotechnical factors and conditions pertaining to construction of the MX system in suitable areas are discussed in this section. Both the horizontal shelter and vertical shelter basing modes are considered.

2.3.1 Grading

Mean surficial slopes in the suitable area are approximately three percent. Surface gradients exceed five percent in about 10 percent of the suitable area. This area is mostly along the mountain fronts. Therefore, preconstruction grading will be minimal for most of the valley. More extensive grading will be necessary near the mountain fronts where surface slopes range from five to nine percent.

2.3.2 Roads

The predominant coarse-grained surficial soils will generally provide good subgrade support for roads where they are in a

dense state. However, most of these soils are not dense near the surface and, therefore, exhibit low strength to an average depth of 3 feet (0.9 m). The subgrade supporting properties of these low-strength, coarse-grained soils are inadequate but can be improved by mechanical compaction. Compaction to moderate depths of 3 to 4 feet (0.9 to 1.2 m) appears to be necessary in a majority of the suitable area. Compaction to greater depth may be required in approximately 20 percent of the granular soil area. Based on results of laboratory CBR tests, compacted granular soils will provide good to very good support for roads.

Fine-grained surficial soils, covering 10 to 20 percent of the suitable area, exhibit low-strength characteristics to an average depth of 6 feet (1.8 m). The maximum observed thickness of low-strength soils is about 12 feet (3.7 m). Supporting qualities of these soils are inadequate for direct support of the base or subbase course of the road system. Results of laboratory CBR tests indicate that mechanical compaction will not adequately strengthen these fine-grained soils for use as a subgrade, but a select granular subbase layer over the compacted fine-grained surficial soils will give the required support.

Well-graded gravelly sands and sandy gravels with less than 25 percent fines (passing a No. 200 sieve) can be used for road subbase and base courses. These soils are present both in the surface and subsurface; however, their extent is not known.

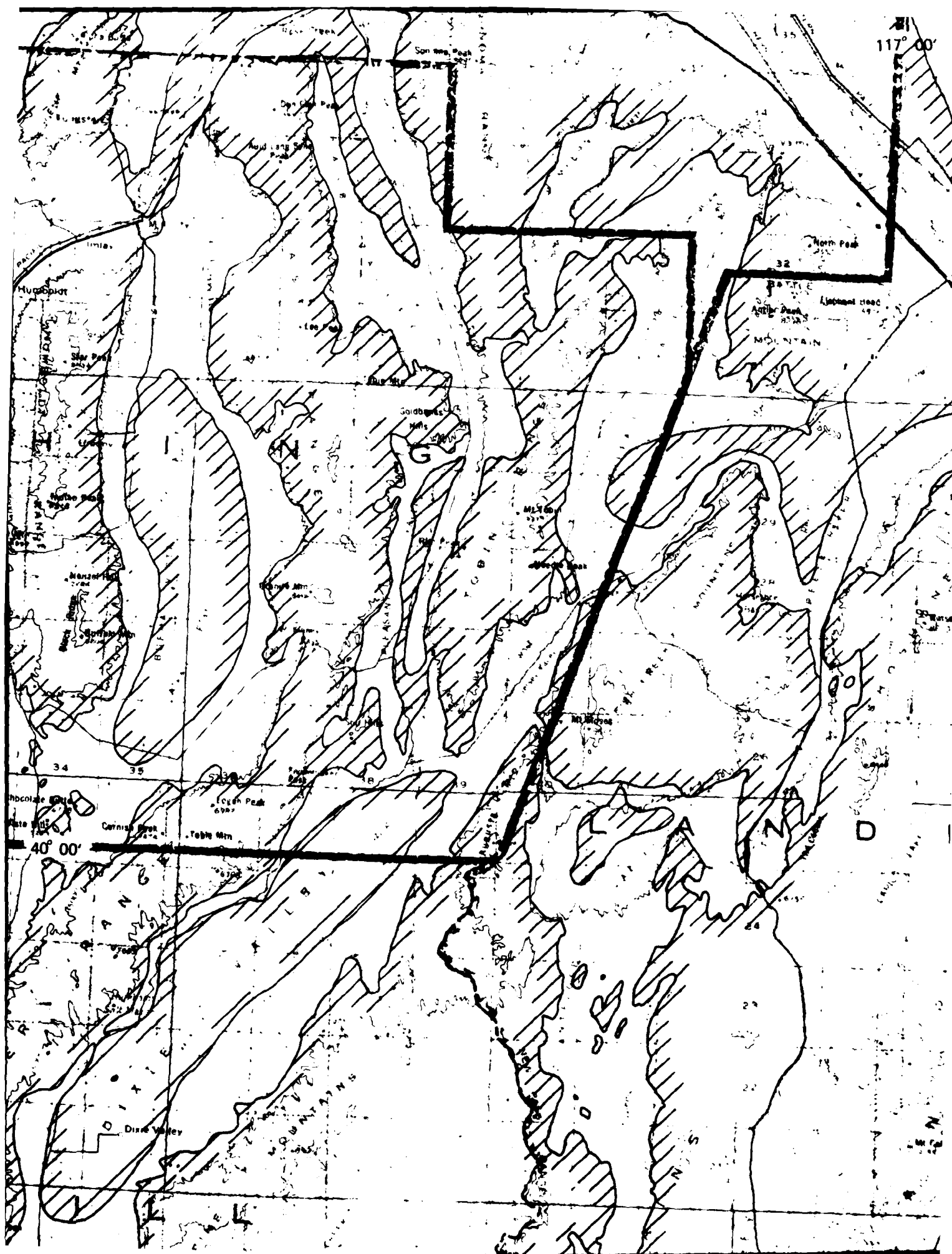
Drainage incision depths appear to be generally less than 6 feet (1.8 m) within 80 to 90 percent of the suitable area.

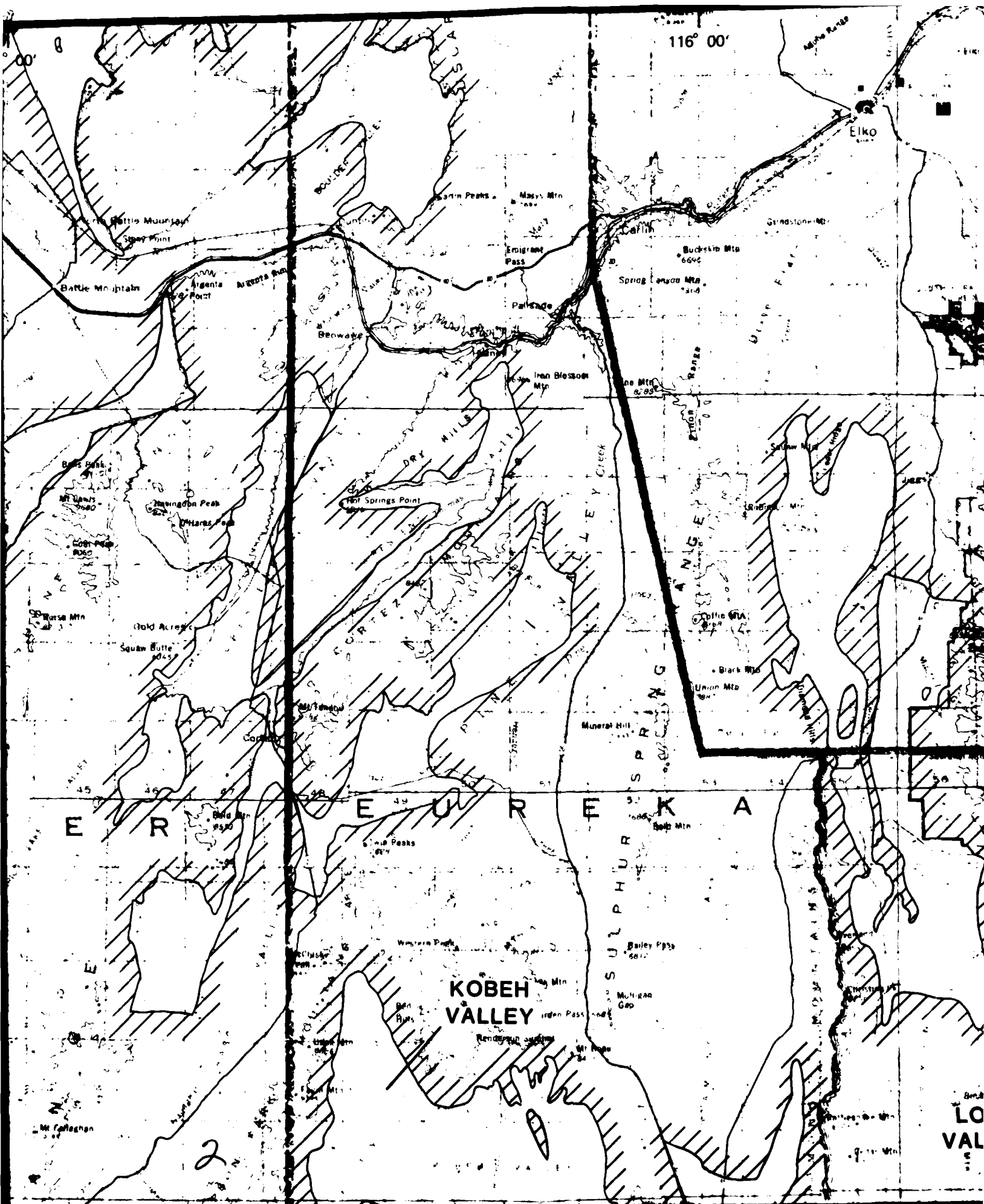
Therefore, the overall cost of drainage structures for roads will be low. Incision depths are greater around the valley perimeter.

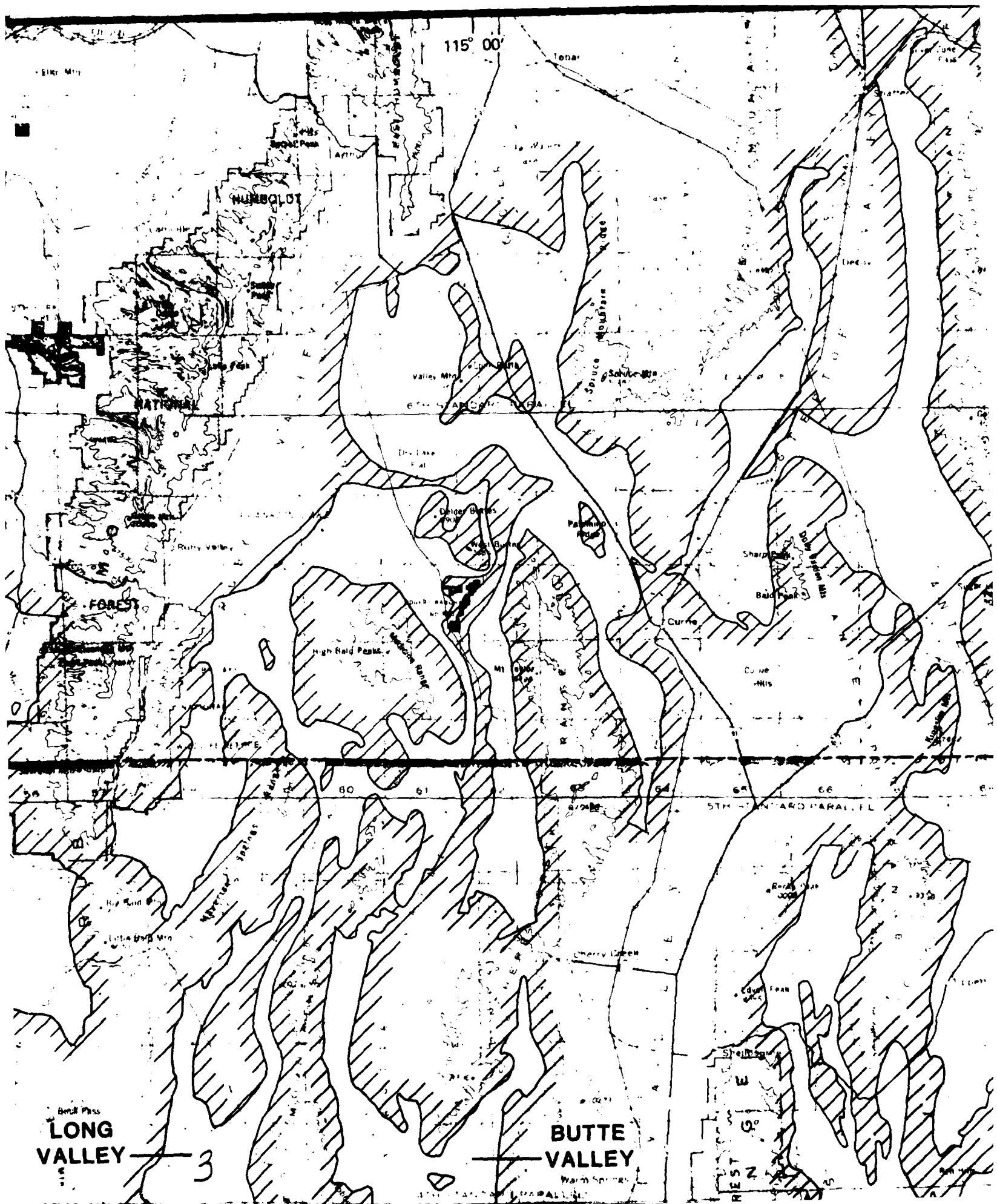
2.3.3 Excavatability and Stability

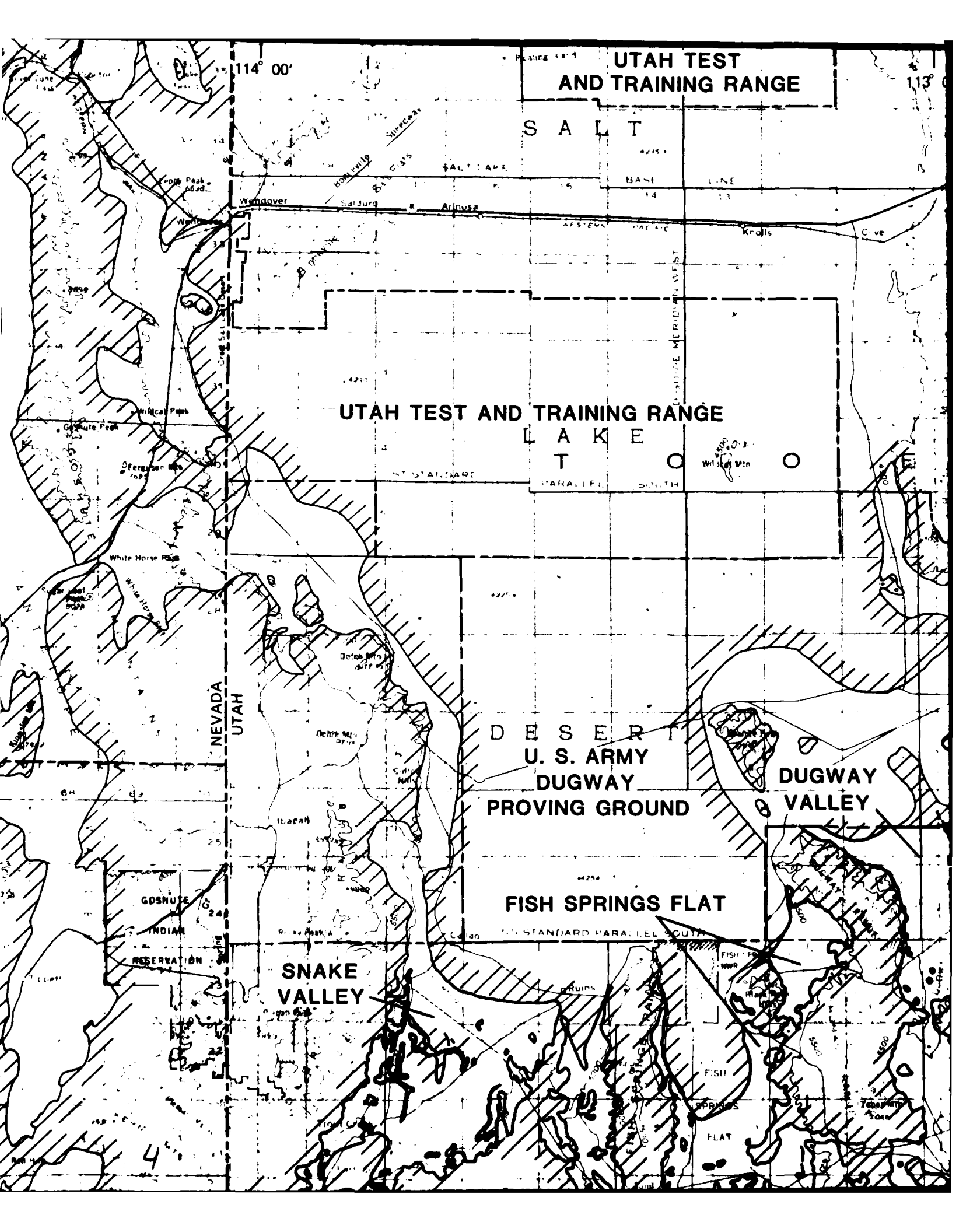
The soils in the construction zone are generally dense to very dense and possess various degrees of calcium carbonate cementation. Fine-grained soils occur in 25 to 35 percent of the subsurface.

Horizontal Shelter: Excavation for the horizontal shelter can be done using conventional equipment such as scrapers, backhoes, and bulldozers. Excavation will be easy in approximately 20 to 30 percent of the area; however, excavation will be moderately difficult to difficult in the remaining area due to cobbles, boulders, and strong calcium-carbonate cementation in the subsurface. Difficult excavation is generally limited to the areas adjacent to the mountain fronts and the southern portion of the valley. The soils investigation indicates that excavations for construction of shelters should be cut back to slopes ranging from 3/4:1 to 1 1/2:1 (horizontal:vertical) for stability. Variations in density and shear strength, which depend on soil composition and the degree of cementation, cause the wide variation in slope angle. Stability decreases slightly in old lacustrine deposits. Because of low-strength surficial soil, the top 2 to 5 feet (0.6 to 1.5 m) in all excavations will generally have to be cut back to 2:1 slope or flatter.









UTAH TEST
AND TRAINING RANGE

S A L T

UTAH TEST AND TRAINING RANGE

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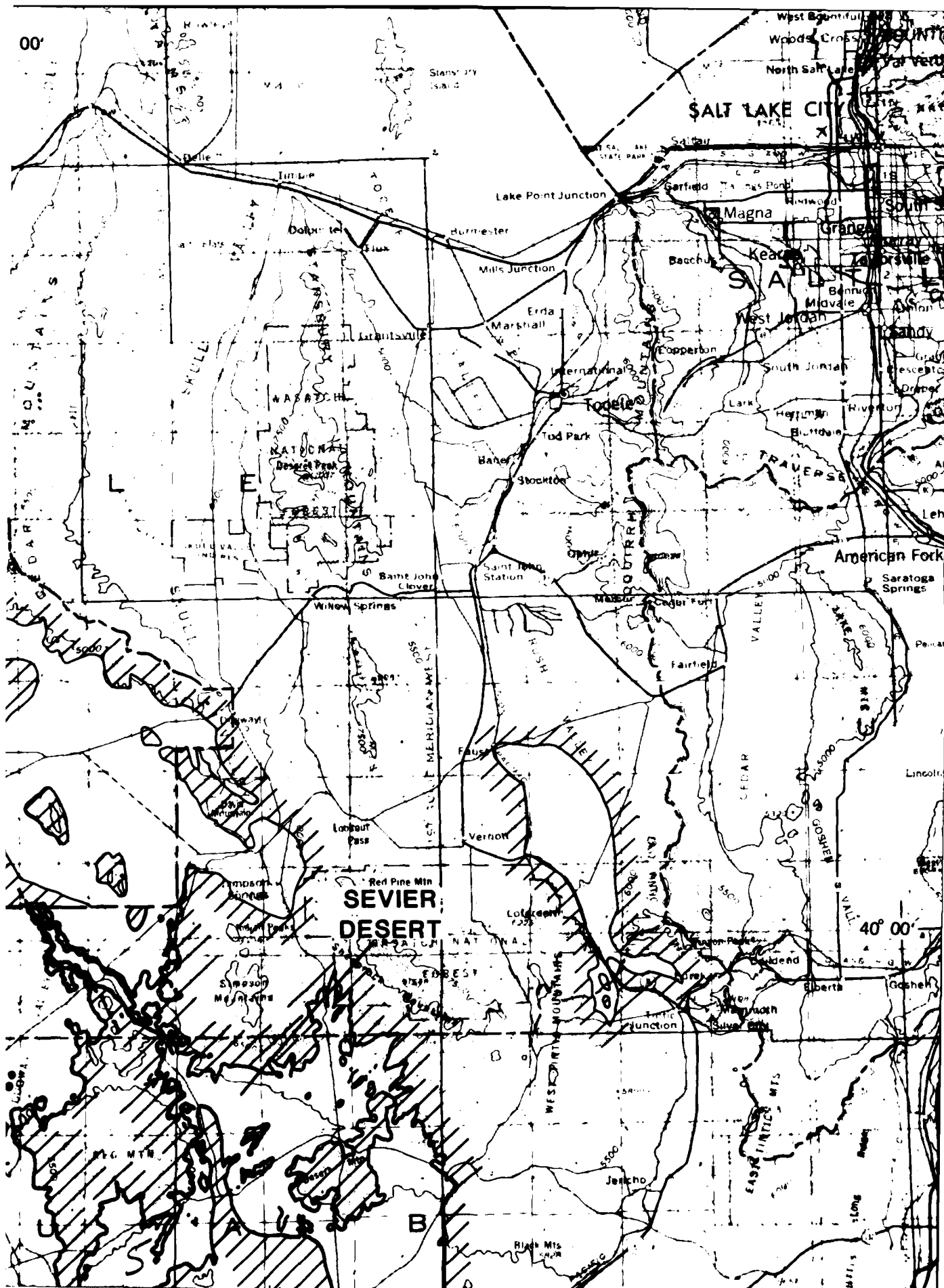
DESERT
U. S. ARMY
DUGWAY
PROVING GROUND

DUGWAY
VALLEY

FISH SPRINGS FLAT

SNAKE
VALLEY

GOSHUTE
INDIAN
RESERVATION



LO
VAL

**MONITOR
VALLEY -**

ANTELOPE
VALLEY

EUREKA

**NEWARK
VALLEY**

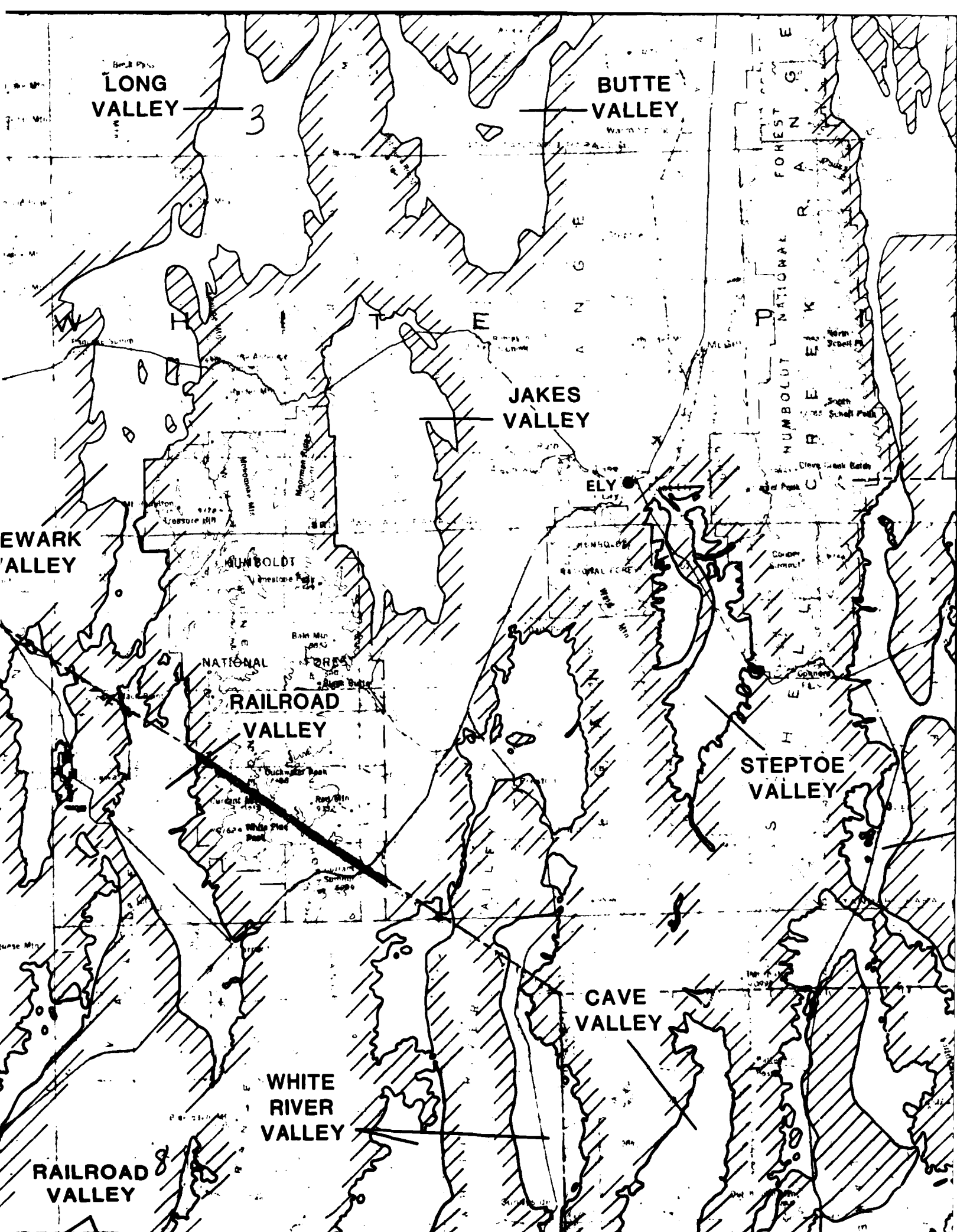
**LITTLE SMOKY
VALLEY**

BIG SAND SPRINGS VALLEY

**HOT CREEK
VALLEY**

STONE CABIN VALLEY

RAILROAD
VALLEY



LONG VALLEY

3

BUTTE VALLEY

JAKES VALLEY

ELY VALLEY

HUMBOLDT

RAILROAD VALLEY

STEPTOE VALLEY

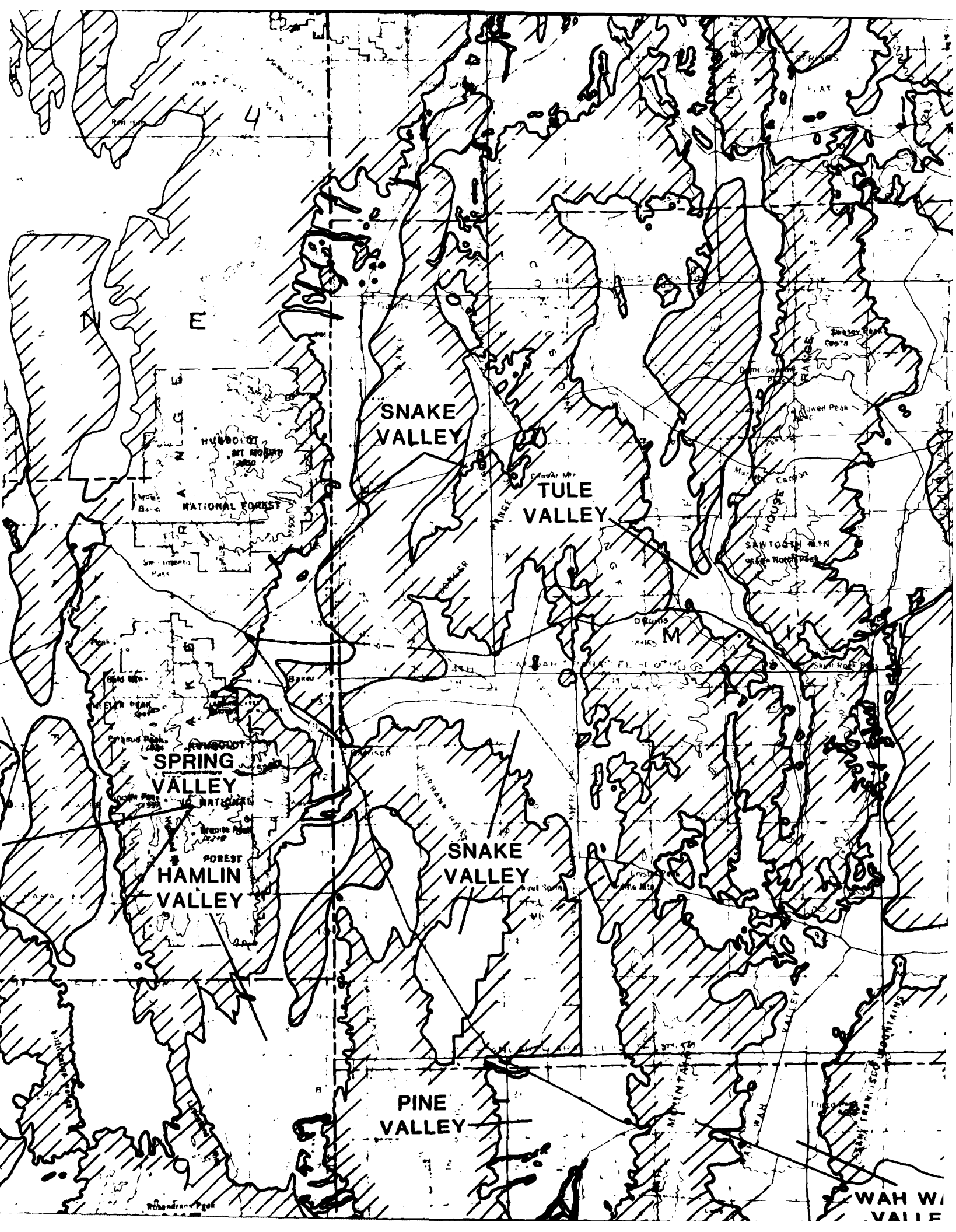
CAVE VALLEY

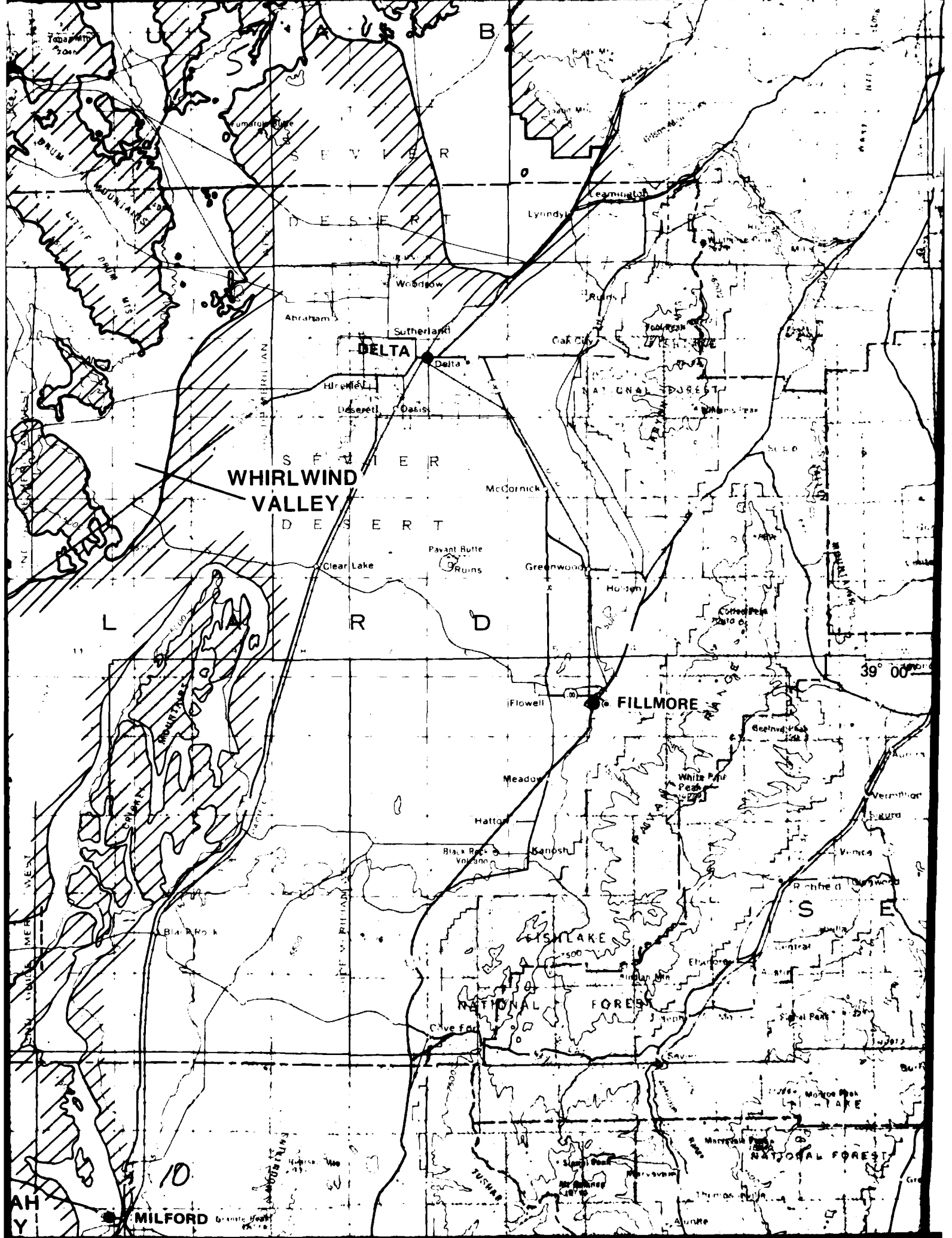
WHITE RIVER VALLEY

RAILROAD VALLEY

HUMBOLDT NATIONAL FOREST

ELY





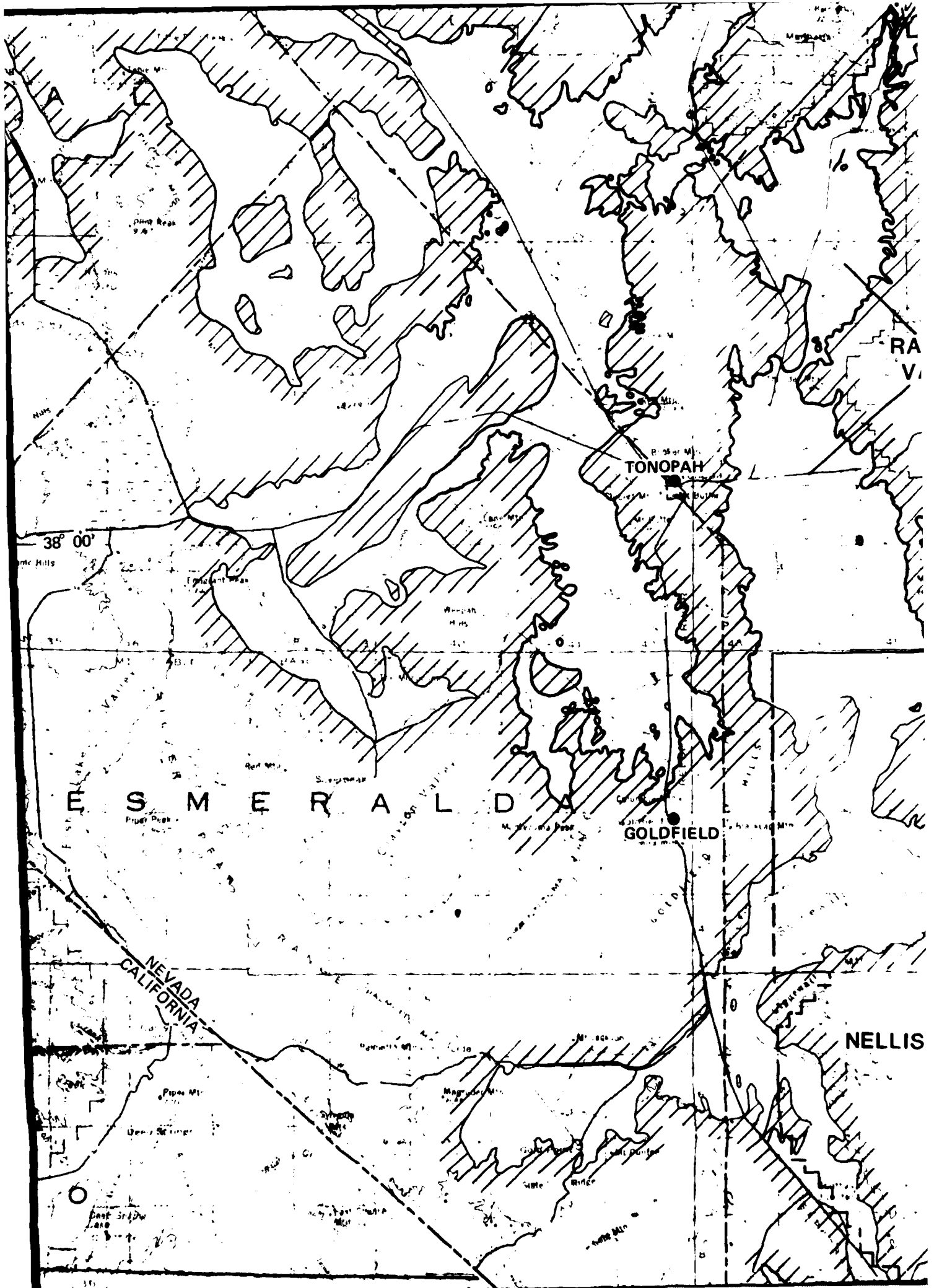
WHIRLWIND
VALLEY

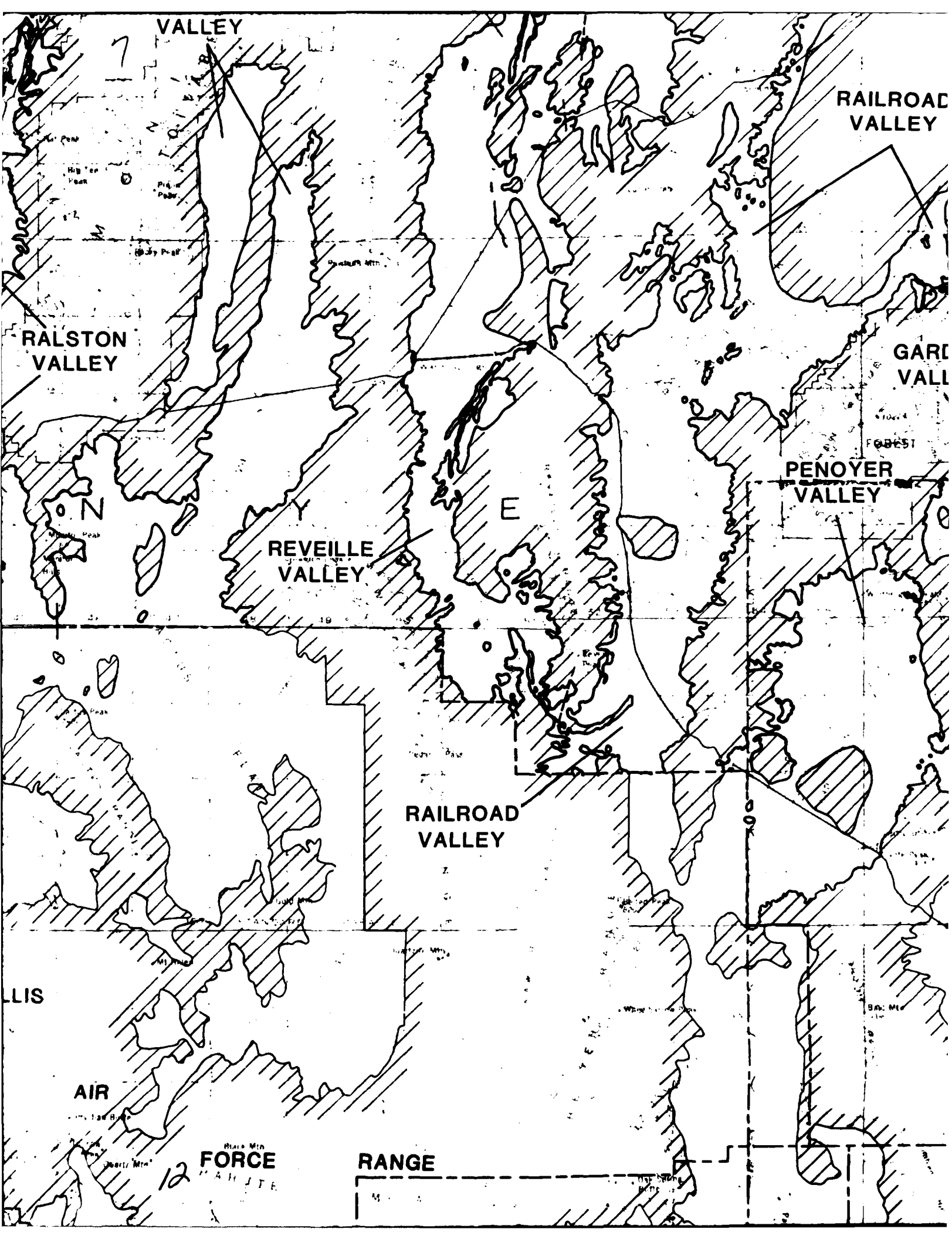
DELTA

FILLMORE

FISHLAKE
NATIONAL FOREST

MILFORD





VALLEY

RAILROAD VALLEY

RALSTON VALLEY

GAR VAL

PENOYER VALLEY

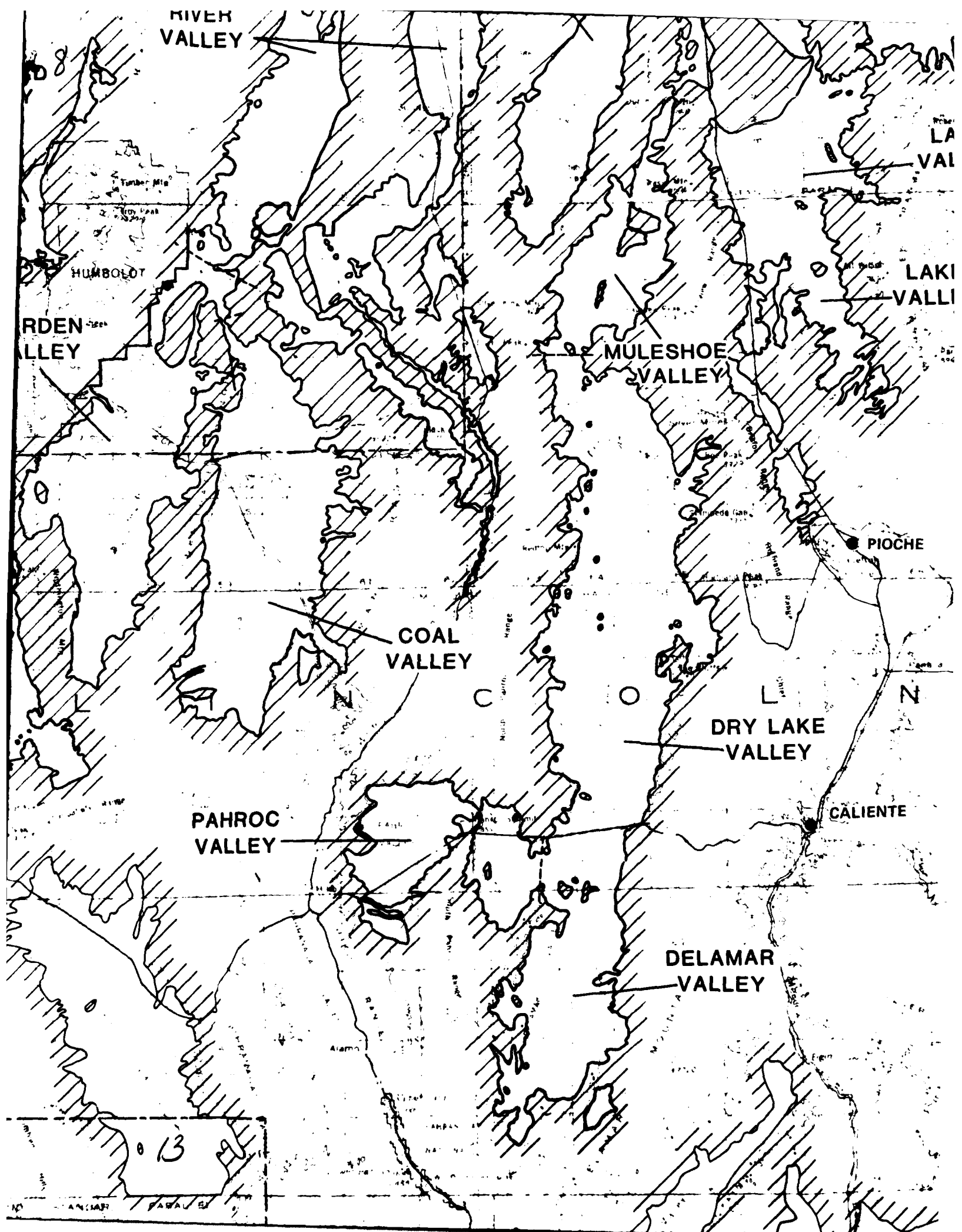
REVEILLE VALLEY

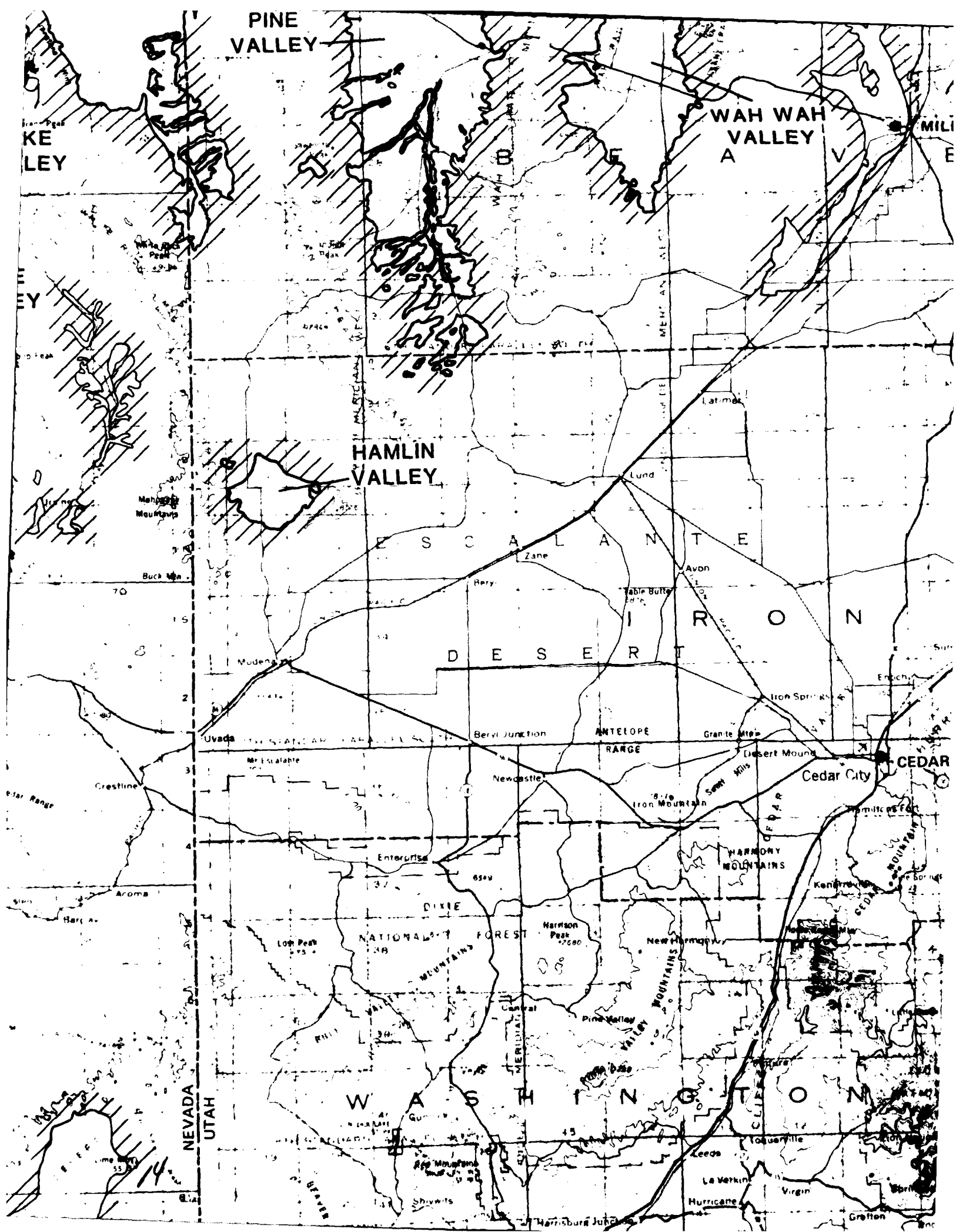
RAILROAD VALLEY

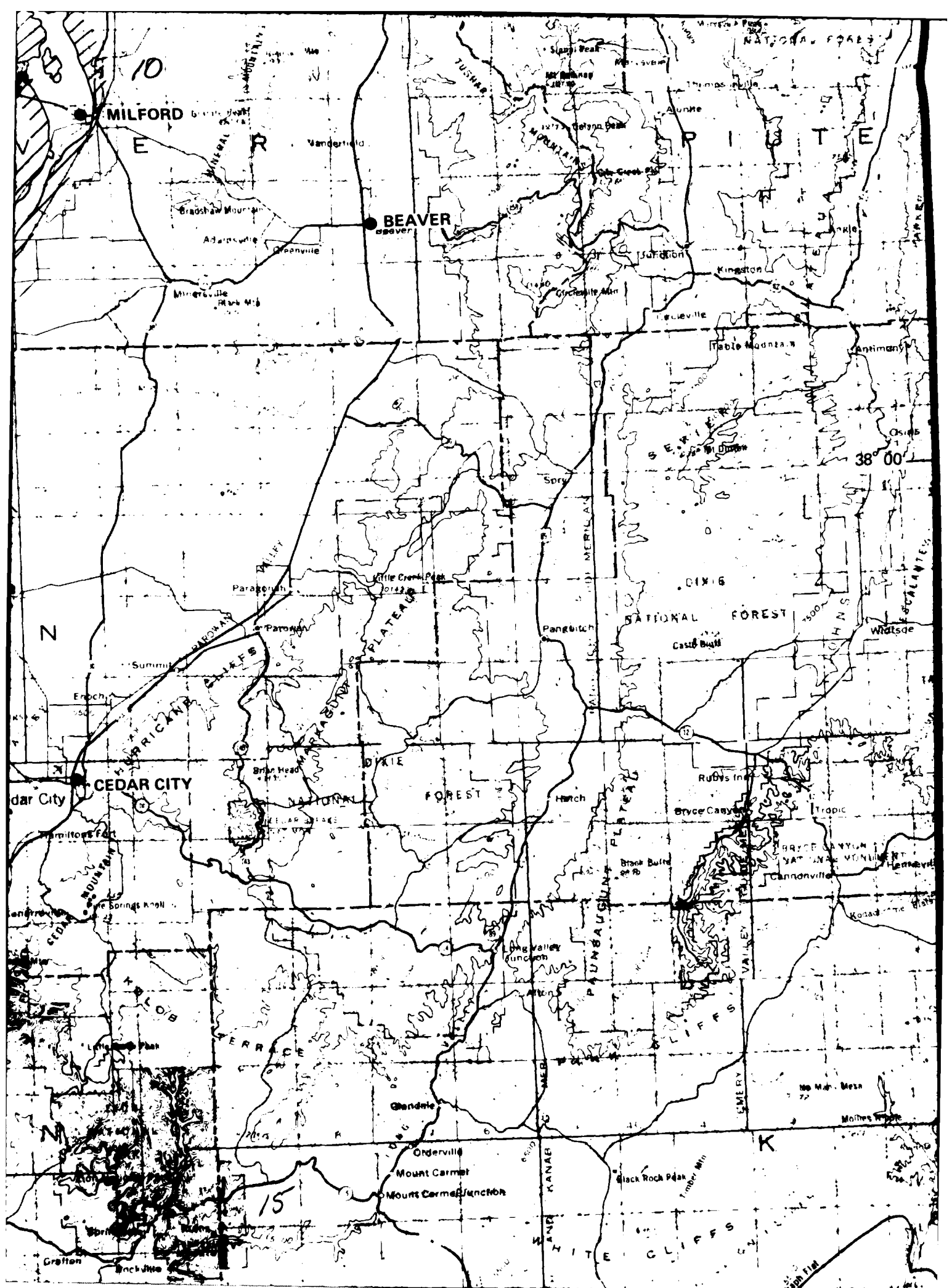
AIR

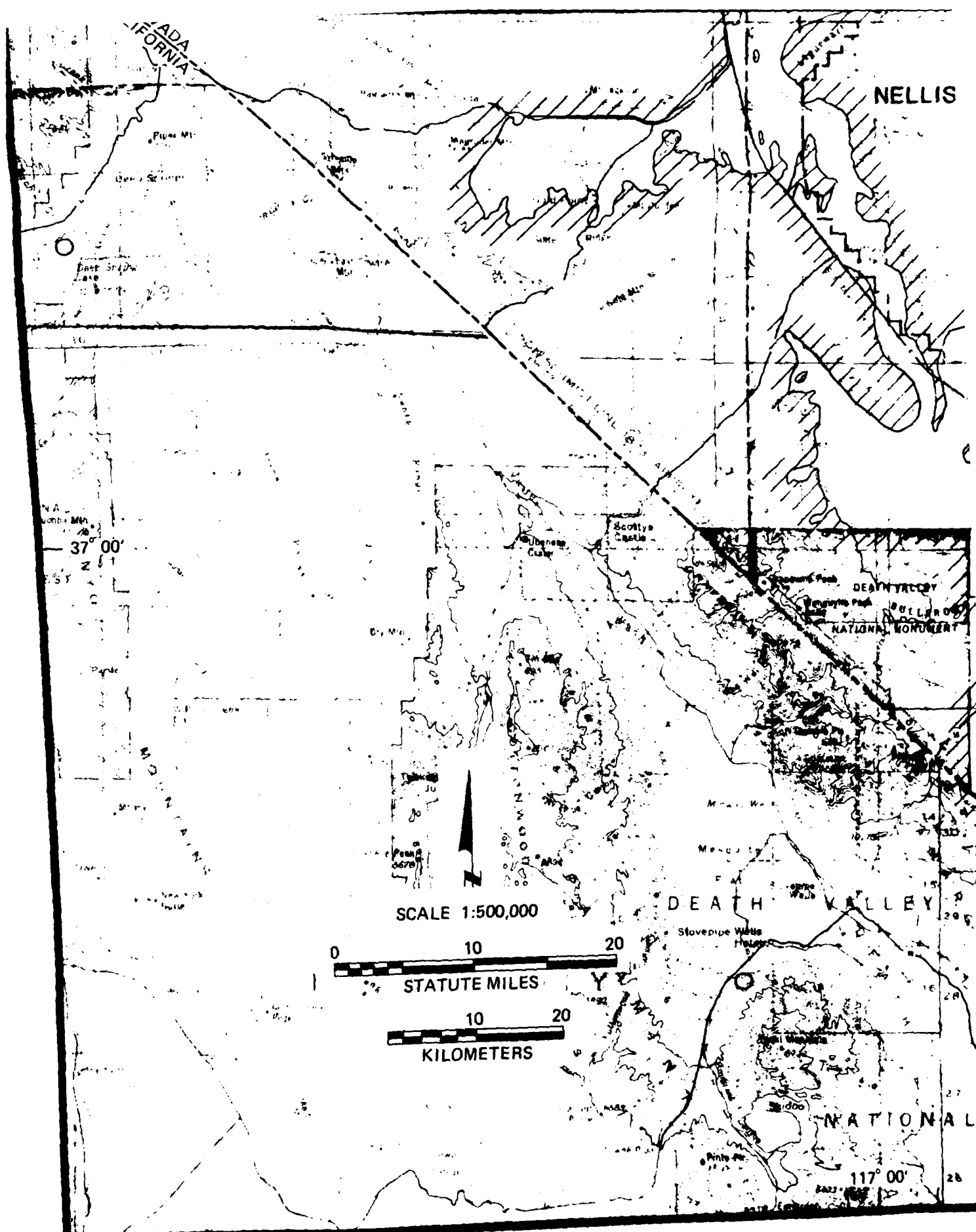
FORCE

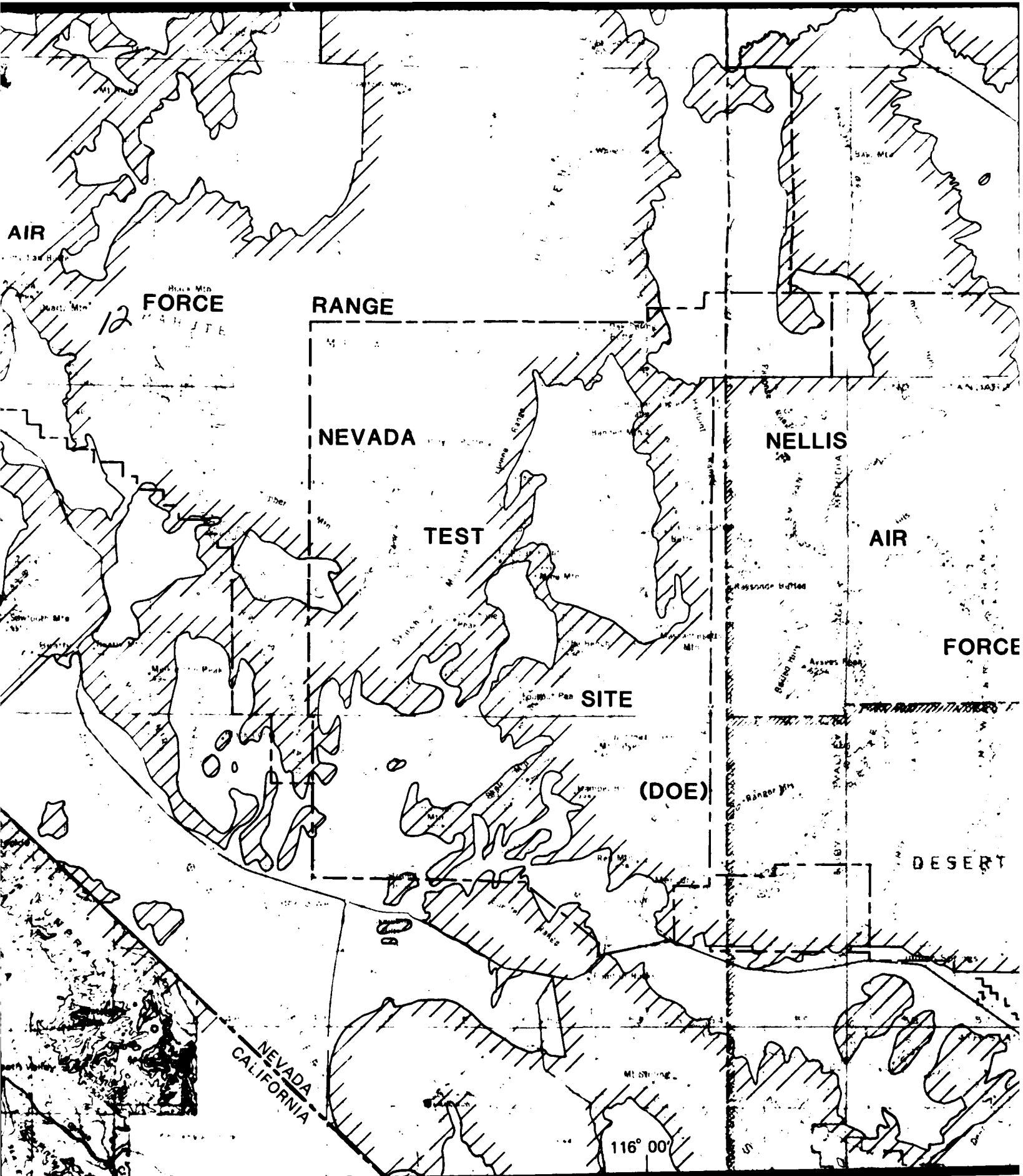
RANGE

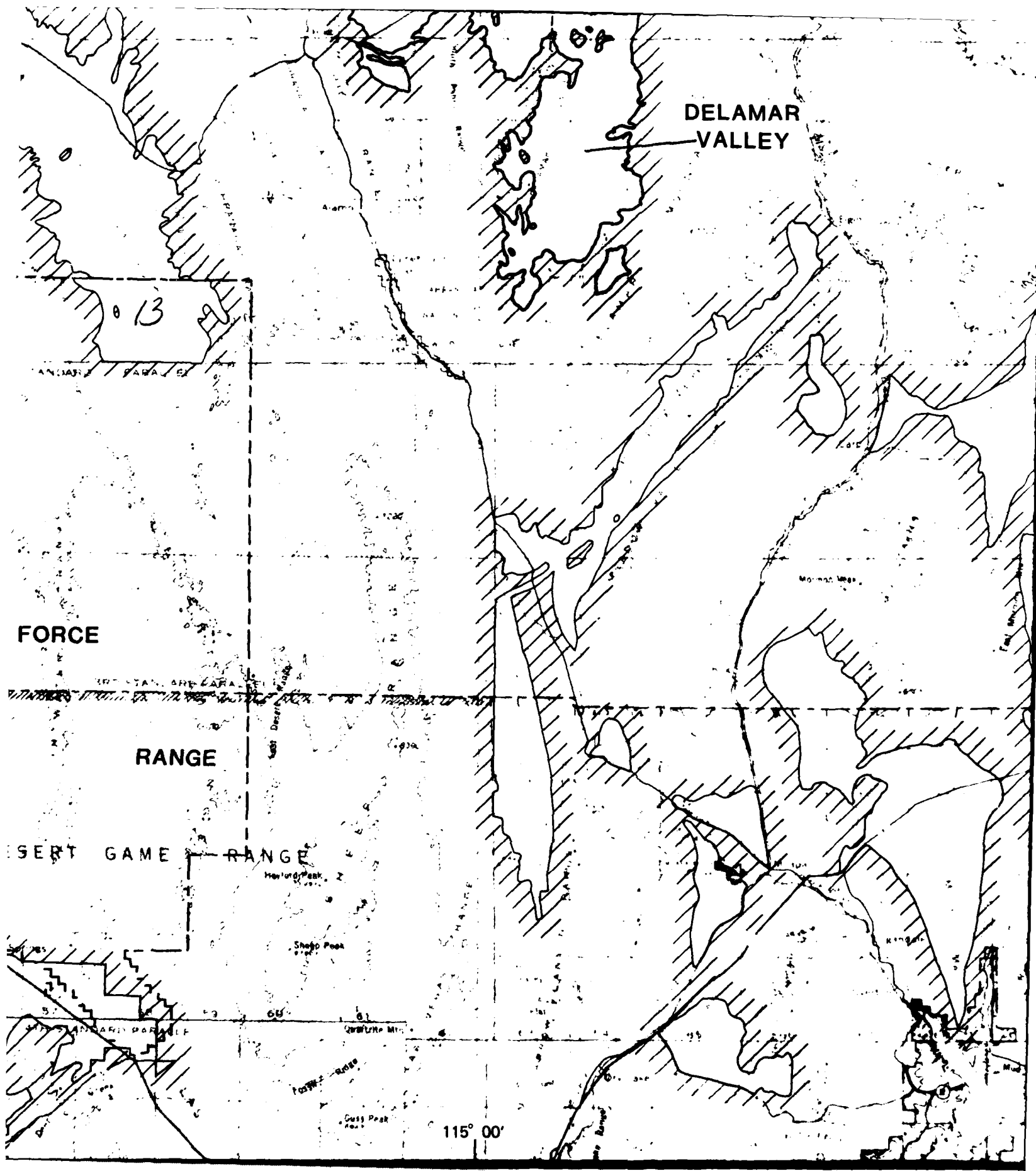


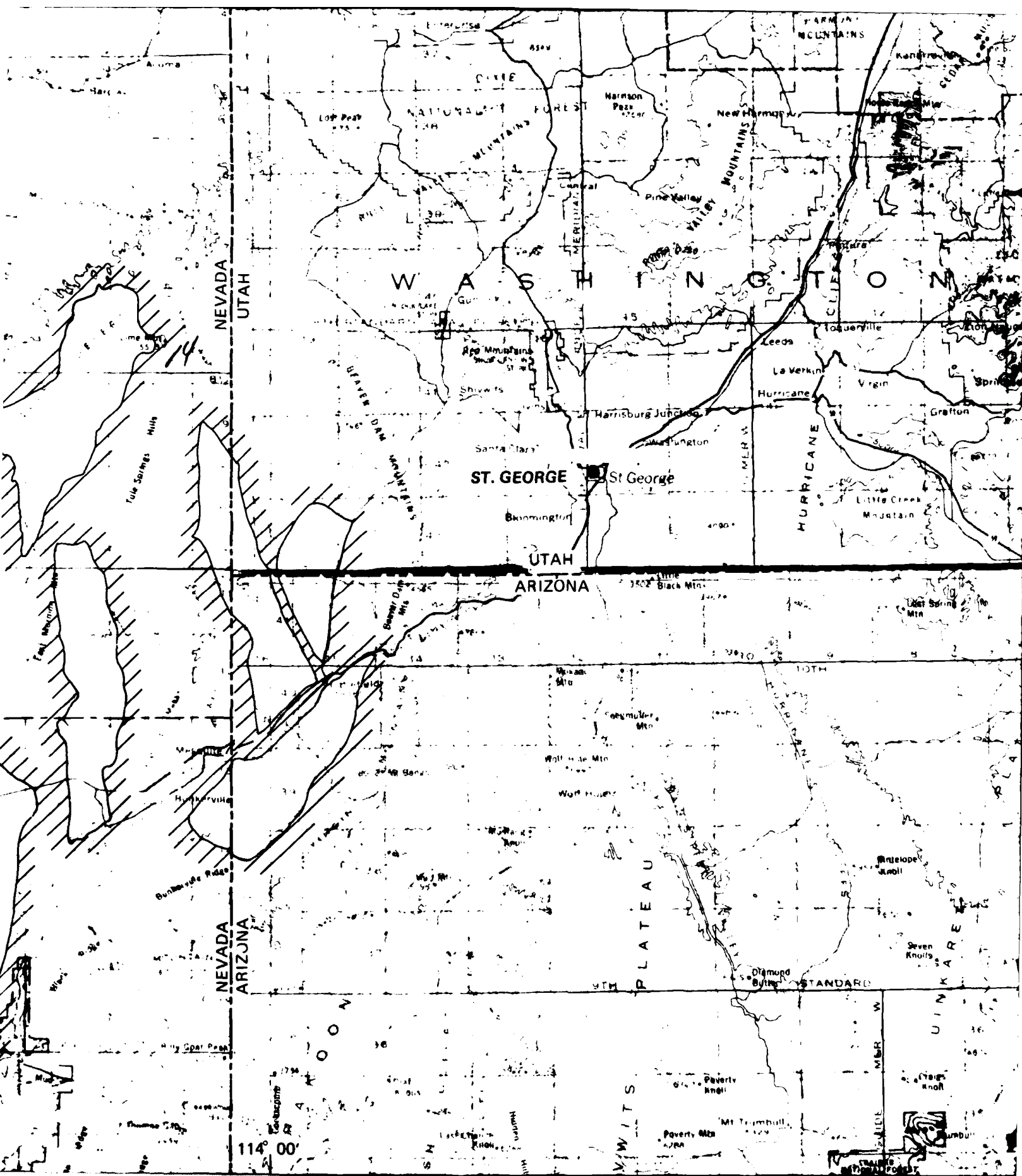


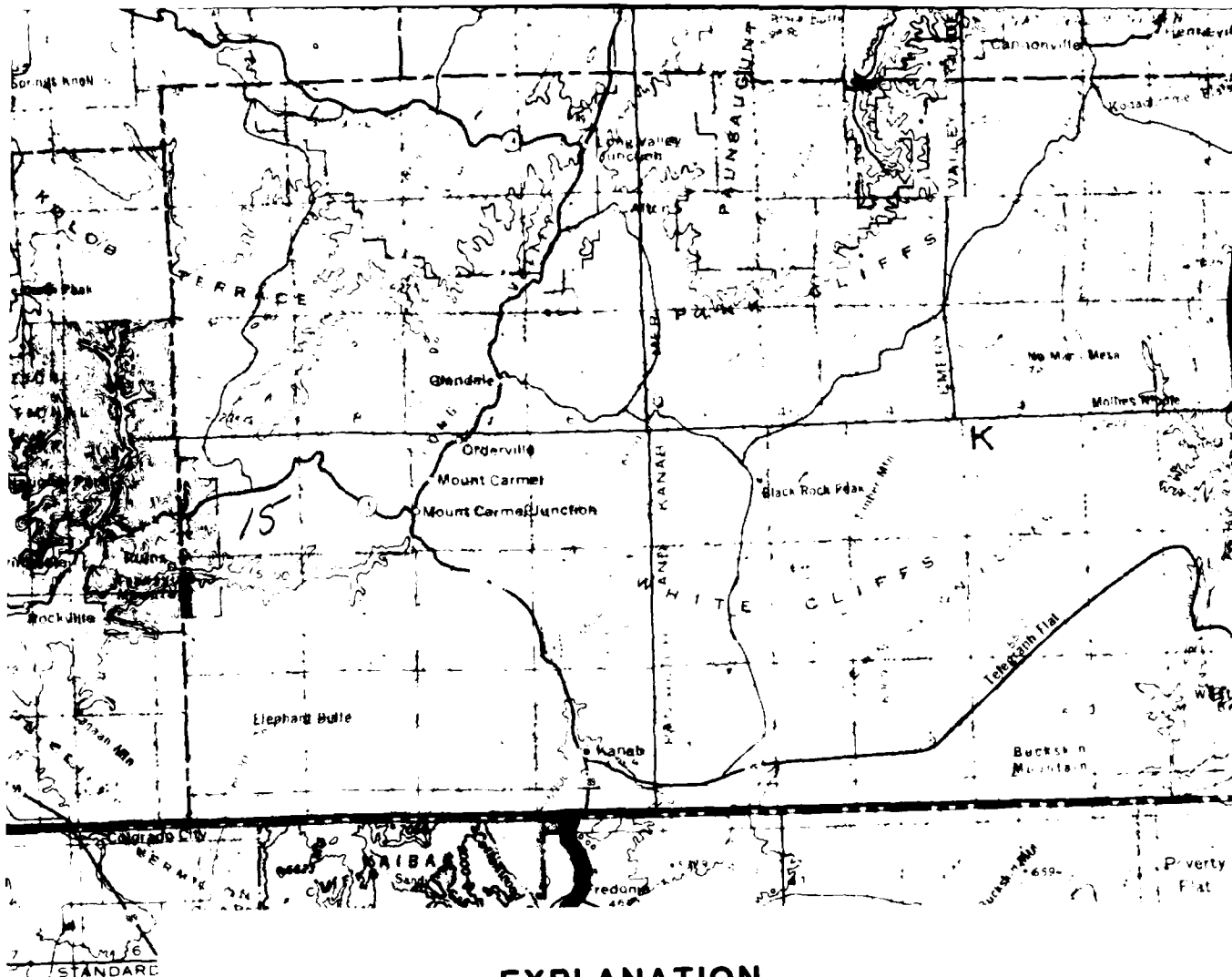












EXPLANATION



SUITABLE AREA FOR HORIZONTAL SHELTER BASED ON VERIFICATION STUDIES
FY 78, FY 79 AND FY 80

Yellow
Me



SUITABLE AREA FOR HORIZONTAL SHELTER BASED ON SCREENING STUDIES.
LOCALLY MODIFIED BY PRIOR VERIFICATION STUDIES

1 25 OCT 1979

2 27 FEB 1980

3 20 JUN 1980

4 26 NOV 1980

5 _____

6 _____

7 _____

GEOTECHNICALLY SUITABLE AREAS NEVADA-UTAH

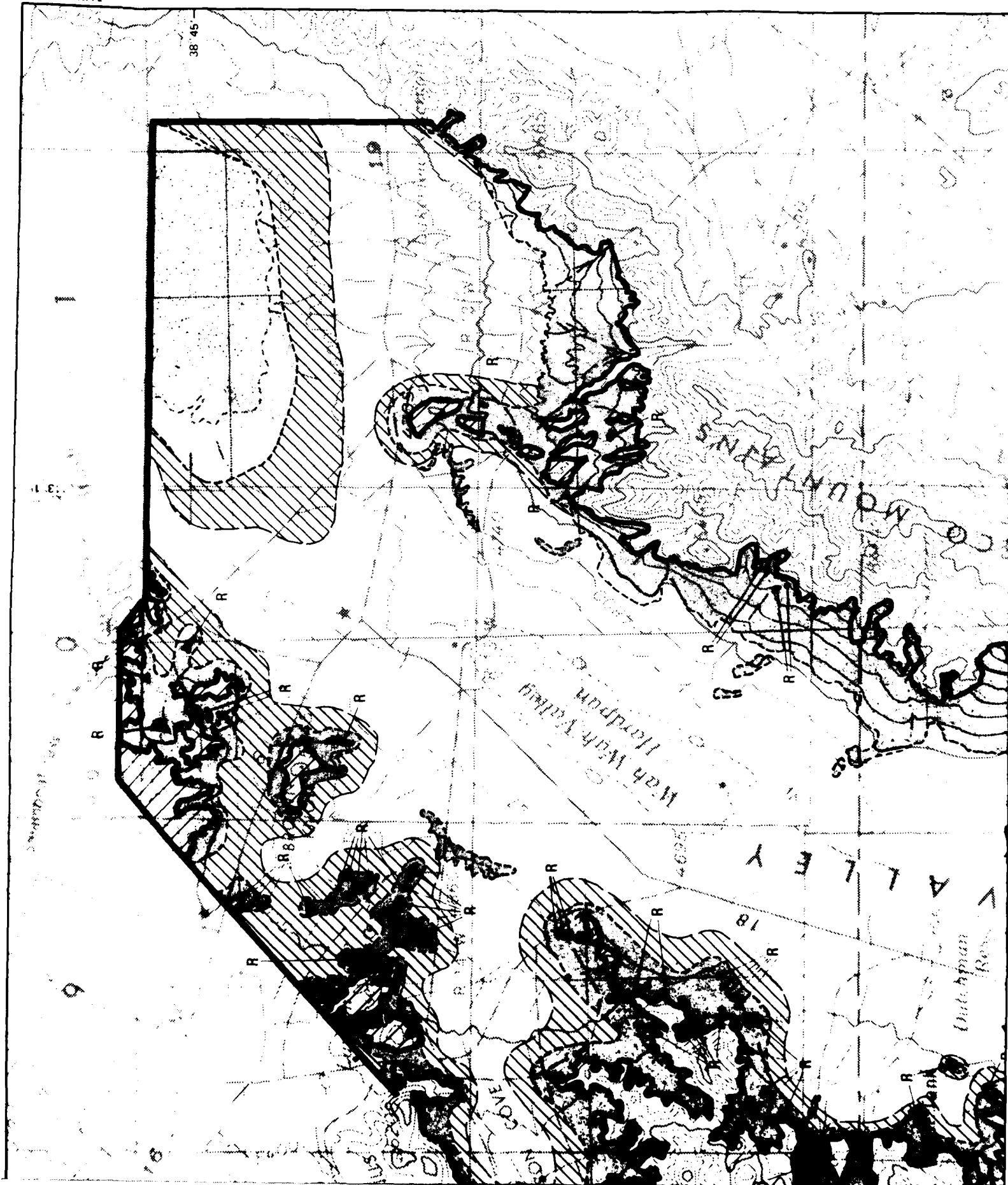
MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - BMO

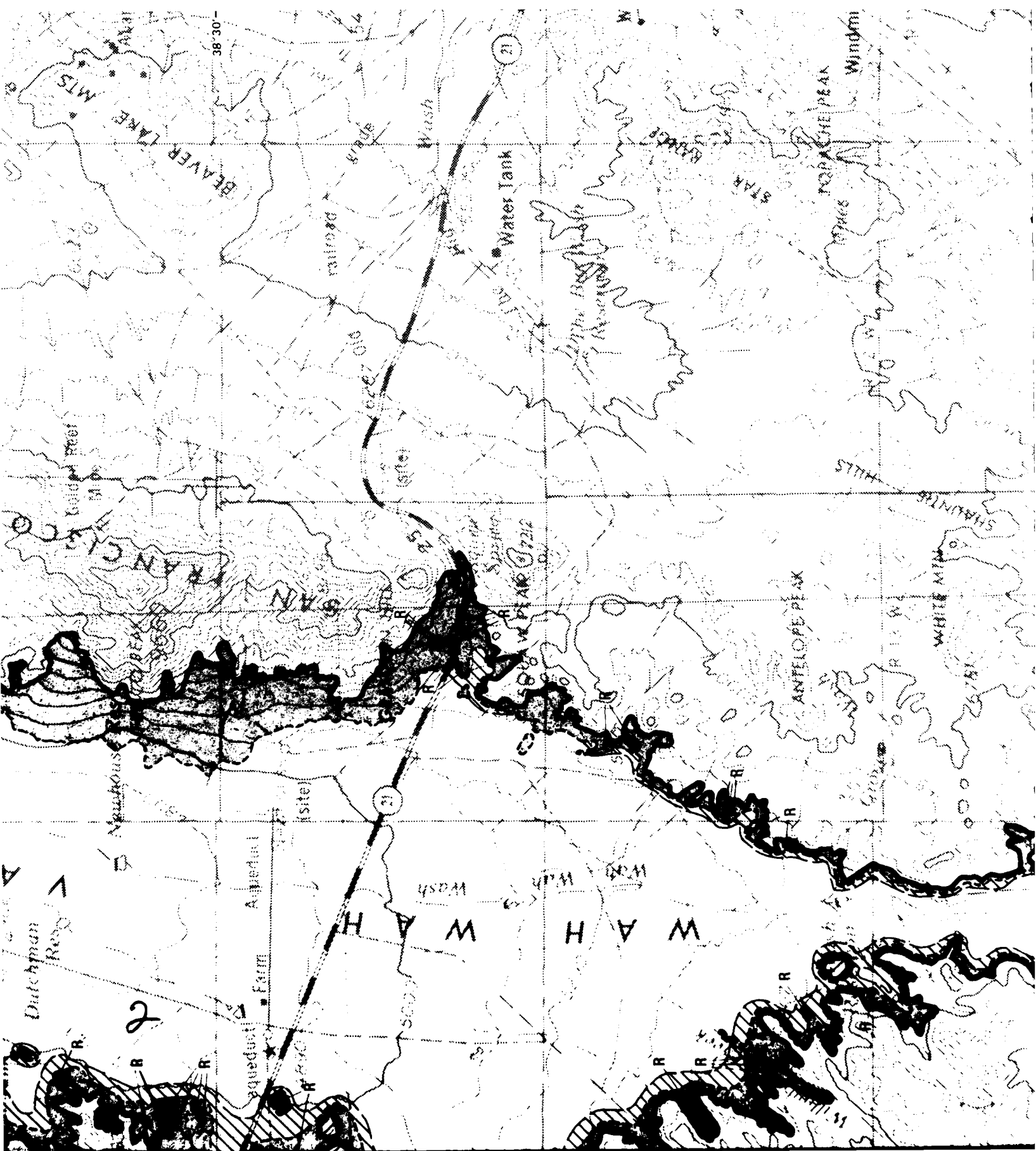
DRAWING

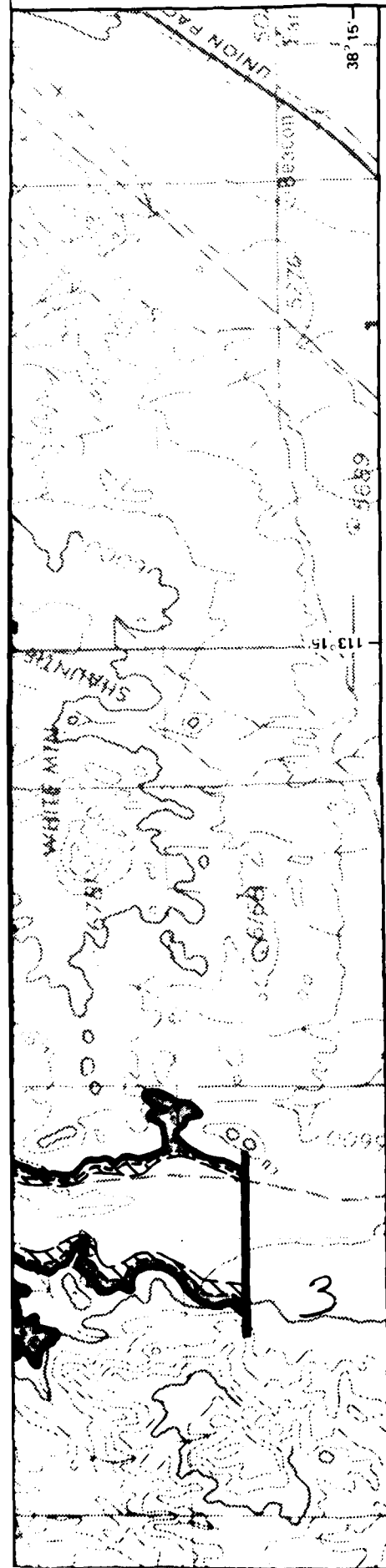
1-1

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Vertical Shelter: Relatively low compressional wave velocities in the upper 120 feet (36 m) indicate that large diameter auger drills could be used for vertical shelter excavation and that the walls of the holes will probably require stabilization with slurry or other materials.







EXPLANATION

-  Area suitable for horizontal and vertical shelter basing modes. Depth to rock and water greater than 150 feet (46m).
-  Area suitable for horizontal shelter but, not suitable for vertical shelter. Depth to rock greater than 50 feet (15m) and less than 150 feet (46m).
-  Area unsuitable for both horizontal and vertical shelter basing modes as determined from application of depth to rock and water, topographic terrain, and cultural exclusions.
-  Areas of isolated exposed rock.
- R** Areas of isolated exposed rock too small for shading.
-  Contact between rock and basin-fill.
-  Valley borders.



NORTH

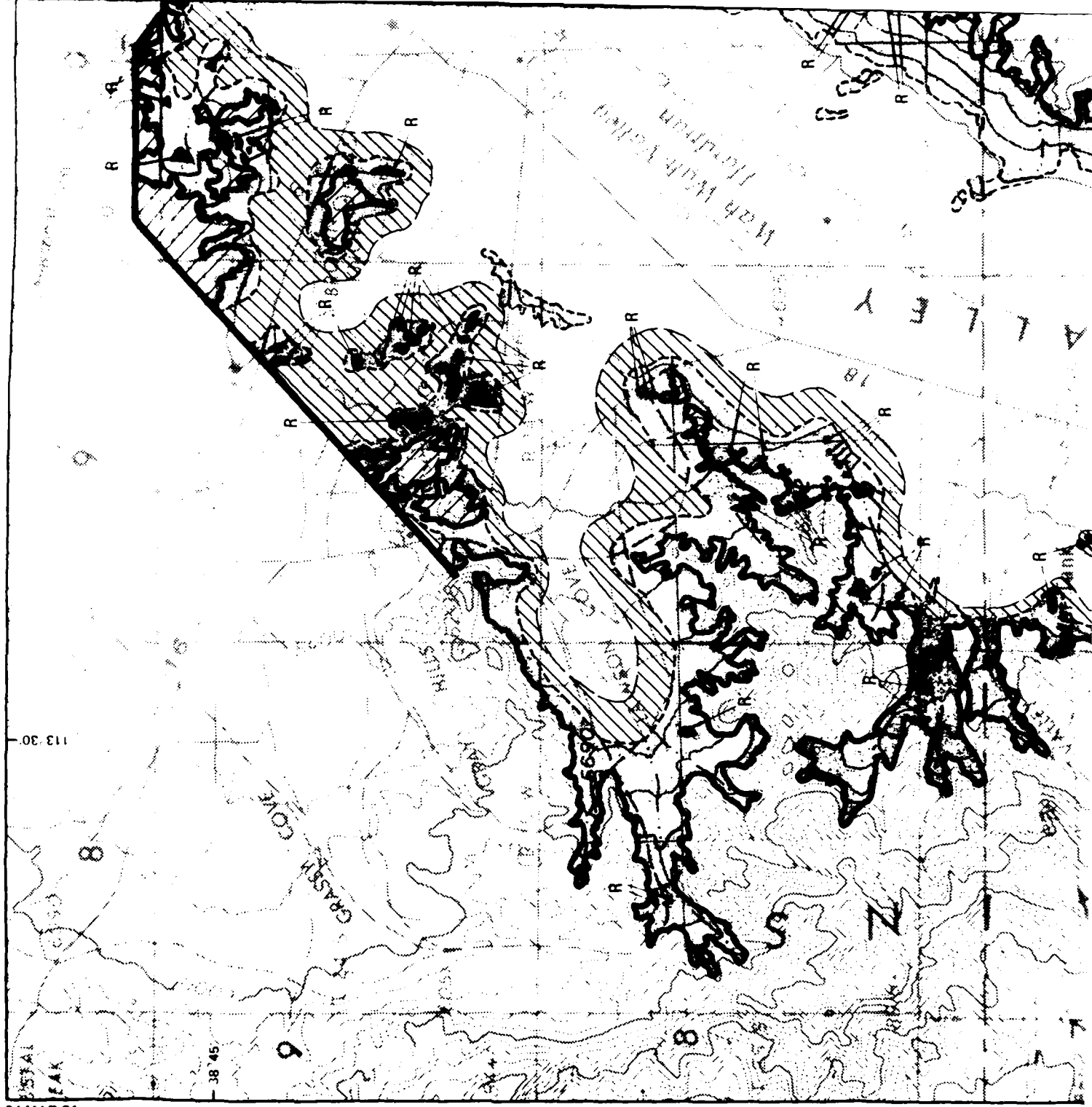
SCALE 1:125,000

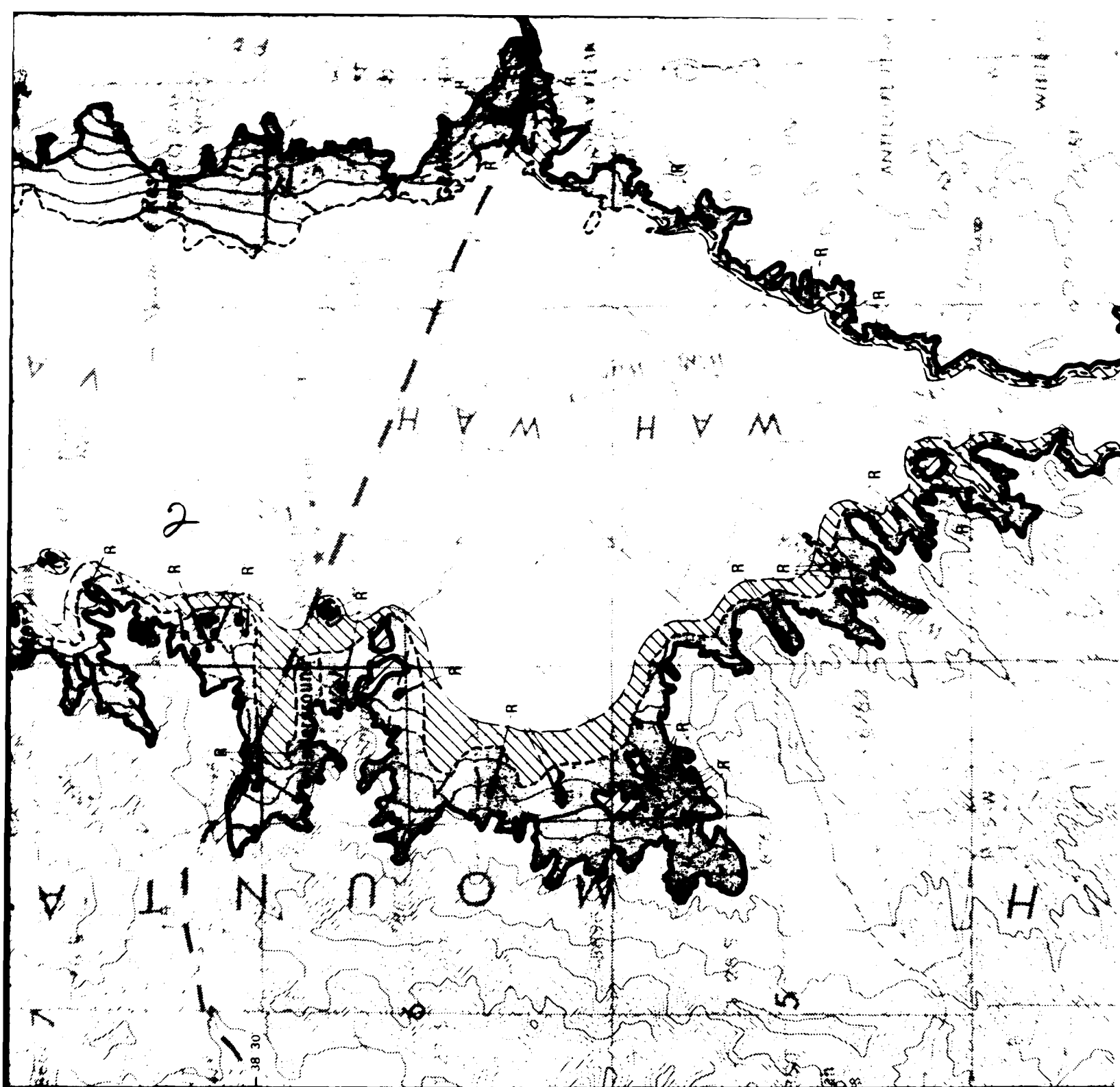


STATUTE MILES

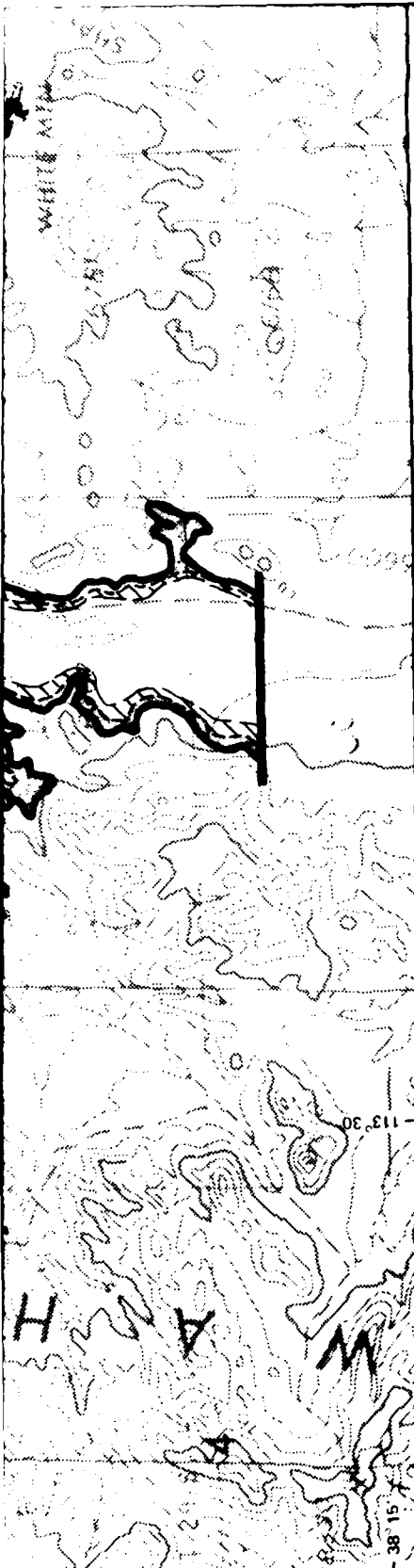


KILOMETERS











5



EXPLANATION

- 
 Area suitable for horizontal and vertical shelter basing modes. Depth to rock and water greater than 150 feet (46m).
- 
 Area suitable for horizontal shelter but, not suitable for vertical shelter. Depth to rock greater than 50 feet (15m) and less than 150 feet (46m).
- 
 Area unsuitable for both horizontal and vertical shelter basing modes as determined from depth to rock and water, topographic terrain, and cultural exclusions.
- 
 Areas of isolated exposed rock.
- R**
 Areas of isolated exposed rock too small for shading.
- 
 Contact between rock and basin-fill.
- 
 Valley borders.

| | |
|---|----------------|
| SUITABLE AREA FOR HORIZONTAL AND VERTICAL SHELTERS WAH WAH VALLEY, UTAH | |
| MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - BMO | DRAWING 2-1 |
| FUGRO NATIONAL, INC. | |

6

3.0 GEOTECHNICAL SUMMARY

3.1 GEOGRAPHIC SETTING

Wah Wah Valley is located in western Beaver and Millard counties, Utah (Figure 3-1). The valley is bounded on the west by the Wah Wah Mountains and on the east by the San Francisco Mountains. On the north and south, it is separated by low, narrow drainage divides from Sevier Lake Valley and Escalante Desert, respectively. State Highway 21 traverses the south-central part of the valley.

The valley is primarily undeveloped desert rangeland, with a few corrals, fences, and water tanks. Several abandoned mining sites and ranches are located within the valley. Milford, the nearest town, is 25 miles (40 km) to the east.

3.2 GEOLOGIC SETTING

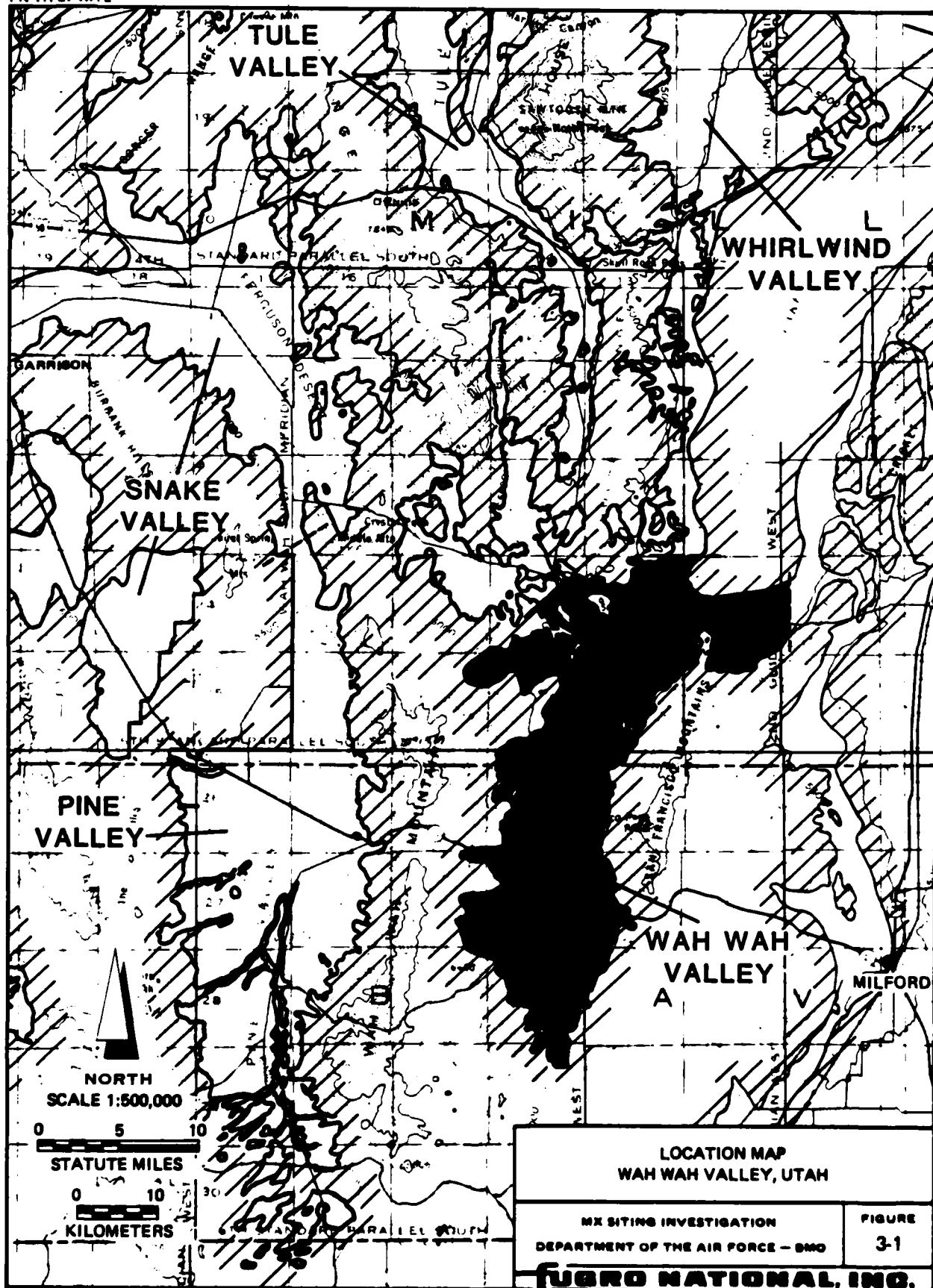
3.2.1 Rock Types

Wah Wah Valley is a north-south trending alluvial basin bordered by mountains on the west and east. These mountain ranges are composed primarily of a thick sequence of Paleozoic limestone and dolomite, with lesser amounts of Precambrian and Cambrian quartzites and phyllites. Tertiary volcanic rocks, consisting of dacite and pyroclastic rocks with minor basalt, are present in all the mountains bordering the valley (Stephens, 1974; and Hintze, 1963).

3.2.2 Structure

The geologic structure of Wah Wah Valley is typical of the Great Basin tectonic province and is a result of late Tertiary/

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Quaternary block faulting due to tensional stresses directed east-west or northwest-southeast. Fault structures in the Great Basin are generally tilted blocks or horst-graben structures in which the valleys occupy the down-tilted or the dropped blocks, and the mountains represent the upturned or lifted blocks. Most tectonic features, including the major faults bounding these blocks, generally trend north-south and are usually located near the margins of the valleys, although a few faults have been found near the valley axes. In some cases, however, faults are oriented in other directions.

The alluvial basin fill in Wah Wah Valley occupies the low part of a down-to-the-east tilted block, and the Wah Wah Mountains to the west represent the uptilted portion. The major basin-bounding fault system in Wah Wah Valley is on the eastern side at the base of the San Francisco Mountains. The surface manifestation of this structure is a 20-mile (32-km) long zone of subparallel scarps in alluvium. The maximum observed scarp height of 41 feet (12.5 m) occurs north of Newhouse Ranch (Drawing 3-2). The last movement on this fault system probably occurred in late Pleistocene time because the fault cuts intermediate-age alluvial fans (A5i) but not younger-age alluvial fans (A5y) and because the fault is covered to the north by unfaulted lake shorelines of latest Pleistocene age (about 10,000 to 15,000 years old).

Several smaller, localized fault zones are located in other areas of the valley (Drawing 3-2). All of these tectonic

features trend northerly and appear to be normal faults typical of the Basin and Range tectonic province.

A local zone of late Quaternary faults on the western side of Wah Wah Valley at Wah Wah Springs is composed of several short, subparallel, northwest-trending scarps in alluvium near the rock-alluvium contact. A height of 20 feet (6 m) was measured on one of these scarps. Springs coincident with this fault zone suggest that it may form a ground-water barrier.

Several small faults in bedrock or at bedrock-alluvium contacts have been identified around the valley. Most of these faults have northerly trends paralleling the regional structural grain. Their strong surface expression indicates they may be young, however, their age is uncertain because they are not overlain by young geologic units which could be used to date their last movement.

3.2.3 Surficial Geologic Units

Geologic data stops and engineering field activities were used to verify the aerial photographic interpretation of surficial geologic units. The data stop and field activity locations are shown in Drawing 3-1.

Lacustrine deposits from Pleistocene Lake Bonneville occupy the center of Wah Wah Valley and are the predominant surficial geologic units within Wah Wah Valley (Drawing 3-2). The highest shoreline of Lake Bonneville is well preserved and forms a contact between the alluvial fans on the valley margins and the lacustrine sediments in the center of the valley.

Surficial geologic units mapped within Wah Wah Valley (Drawing 3-2) consist of the following:

- o Older Alluvial Fan Deposits (A5o) - These Pleistocene sediments form the least extensive unit in the valley, occupying less than one percent of the total area. Only one area of old alluvial fan deposits was mapped. This area is located on the western side of the valley. These deposits are composed of sandy gravel and are uncemented with a Stage I caliche development in the near-surface soils.
- o Intermediate Alluvial Fan Deposits (A5i) - These fans, also of Pleistocene age, occupy 25 to 30 percent of the total valley area. The unit forms a discontinuous band immediately adjacent to the mountain fronts surrounding the valley except at its northern margin. These fans are composed of gravelly sands and sandy gravels near the mountains, grading into silty sands toward the valley center. Cementation ranges from absent to moderate. Caliche development is usually Stage I but can vary from absent to Stage II.
- o Younger Alluvial Fan Deposits (A5y) - These Holocene sediments occupy 30 to 35 percent of the total valley area. They occur adjacent to the mountain fronts, interspersed with A5i deposits, and near the valley center in contact with the lacustrine deposits. The unit is mainly composed of silty sands with a few deposits of gravelly soils. Cementation is absent, but some fans are moderately indurated. Caliche development is usually Stage I but varies from absent to Stage II.
- o Fluvial and Associated Flood-plain Deposits (A1) - These sediments are also of Holocene age and cover less than one percent of the valley area. They are primarily present in small channels that empty onto alluvial fans and are composed of silty sands and sandy silts. Both cementation and caliche are absent.
- o Lacustrine Deposits (A4, A4o) - A4 represents Holocene playas and A4o designates Tertiary-Quaternary lacustrine sediments. Together these units occupy 35 to 45 percent of the total area and cover the central and northern parts of the valley. Many soil types are represented in these deposits, consisting of sandy gravels in old lake bars, silty sands and gravelly sands in old lake-bottom sediments, and silts and clays in the active and inactive playa areas. Cementation is absent, induration is moderate, and caliche development ranges from absent to Stage I.

3.3 SURFACE SOILS

Surficial soils of Wah Wah Valley are predominantly coarse-grained. They range from gravels with some fines to sands with some fines. Fine-grained soils (silts and clays) have a limited areal distribution confined generally to the active playa in the northern portion of the valley along the edge of Sevier Lake. Soils from the predominant surficial geologic units can be combined into the following three categories based on their physical and engineering characteristics:

1. Sandy gravels and gravelly sands (geologic units A4os, A5ys, A5ys/A4os, and A5is);
2. Silty sands and clayey sands (geologic units A4os, A5ys, A5ys/A4os, and A5is); and
3. Silts and clays (geologic units A4f, A5ys, A5ys/A4os, and A5is).

3.3.1 Characteristics

A summary of the characteristics of surficial soils, based on field and laboratory test results, is presented in Table 3-1. In addition to the physical properties, the table includes road design data, consisting of laboratory compaction and CBR test results; thickness of low-strength surficial soils; and a qualitative assessment of their suitability for road use. Gradation ranges for the three categories of surficial soils are shown in Figure 3-2. The surficial soils in the top 2 feet (0.6 m) have sporadic, weak calcium-carbonate cementation.

Sandy gravels, silty gravels, gravelly sands, and sands cover approximately 40 to 50 percent of the valley. Gravelly soils commonly occur in the younger and intermediate age fans along

| SOIL DESCRIPTION | | Sandy Gravels, Silty Gravels, Gravelly Sands, and Sands | Silty Sands and Clayey Sa |
|---|--------------------------|--|--------------------------------|
| USCS SYMBOLS | | GM, SW, SP, SM | SM, SC |
| PREDOMINANT SURFICIAL GEOLOGIC UNITS | | A4os, A5ys, A5ys/A4os, A5is | A4os, A5ys, A5ys/A4os, A |
| ESTIMATED AREAL EXTENT % | | 40 - 50 | 40 - 50 |
| PHYSICAL PROPERTIES | | | |
| COBBLES 3 - 12 inches (8 - 30 cm) | % | 0 - 20 | 0 - 5 |
| GRAVEL | % | 1 - 77 [15] | 0 - 27 |
| SAND | % | 8 - 91 [15] | 38 - 81 |
| SILT AND CLAY | % | 3 - 27 [15] | 17 - 46 |
| LIQUID LIMIT | | NDA | 25 - 35 |
| PLASTICITY INDEX | | NDA | NP - 12 |
| ROAD DESIGN DATA | | | |
| MAXIMUM DRY DENSITY | pcf (kg/m ³) | 131.0 - 133.6 (2099 - 2140) [3] | 118.5 - 127.8 (1898 - 2047) |
| OPTIMUM MOISTURE CONTENT | % | 8.5 - 9.1 [3] | 9.7 - 14.0 |
| CBR AT 90% RELATIVE COMPACTION | % | 7 - 33 [3] | 4 - 34 |
| SUITABILITY AS ROAD SUBGRADE ⁽¹⁾ | | good to very good | fair to very good |
| SUITABILITY AS ROAD SUBBASE OR BASE ⁽¹⁾ | | fair to good | poor to fair |
| THICKNESS OF LOW STRENGTH SURFICIAL SOIL ⁽²⁾ | RANGE ft (m) | 0.5 - 8.1 (0.2 - 2.5) [18] | 0.5 - 10.1 (0.2 - 3.1) |
| | AVERAGE ft (m) | 2.0 (0.6) [18] | 3.4 (1.0) |

(1) Suitability is a subjective rating explained in Section A5.0 of the Appendix.

(2) Low strength surficial soil is defined as soil which will perform poorly as a road subgrade at its present consistency; see Table 3.2 for details.

NOTES: • [] - Number
• NDA - No data
not perf

| | | |
|----------------------------------|---|--|
| ity Sands and Clayey Sands | Sandy Silts, Silts, Sandy Clays, and Clays | |
| M, SC | ML, CL, MH, CH | |
| 4os, A5ys, A5ys/A4os, A5is | A4f, A5ys, A5ys/A4os, A5is | |
| 0 - 50 | 10 - 20 | |
| | | |
| - 5 | 0 | |
| 1 - 27 [33] | 0 - 6 [14] | |
| 18 - 81 [33] | 0 - 48 [14] | |
| 7 - 46 [33] | 50 - 100 [14] | |
| 25 - 35 [4] | 23 - 57 [12] | |
| NP - 12 [7] | NP - 31 [13] | |
| | | |
| 18.5 - 127.8 (898 - 2047) [8] | 102.3 - 121.4 (1639 - 1945) [5] | |
| 0.7 - 14.0 [8] | 12.7 - 22.0 [5] | |
| 1 - 34 [8] | 4 - 17 [5] | |
| fair to very good | poor to fair | |
| poor to fair | not suitable | |
| 0.5 - 10.1 (0.2 - 3.1) [42] | 1.0 - 12.0 (0.3 - 3.7) [10] | |
| 4 (1.0) [42] | 6.0 (1.8) [10] | |

• [] - Number of tests performed.

• NDA - No data available (insufficient data or tests not performed)

2

CHARACTERISTICS OF SURFICIAL SOILS
WAH WAH VALLEY, UTAH

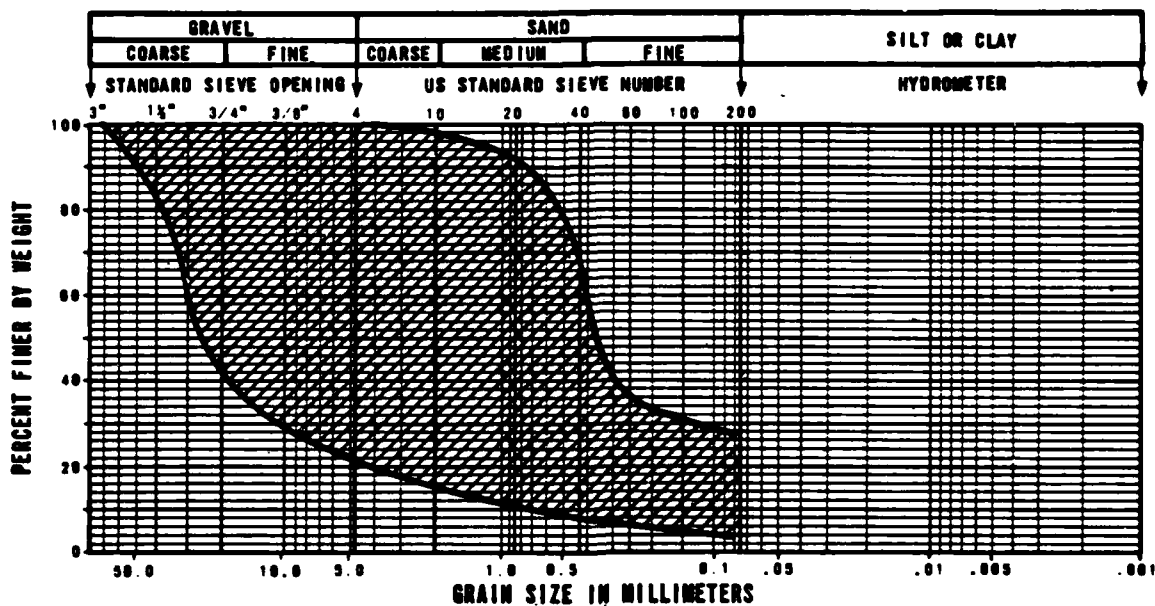
MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - BMO

TABLE
3-1

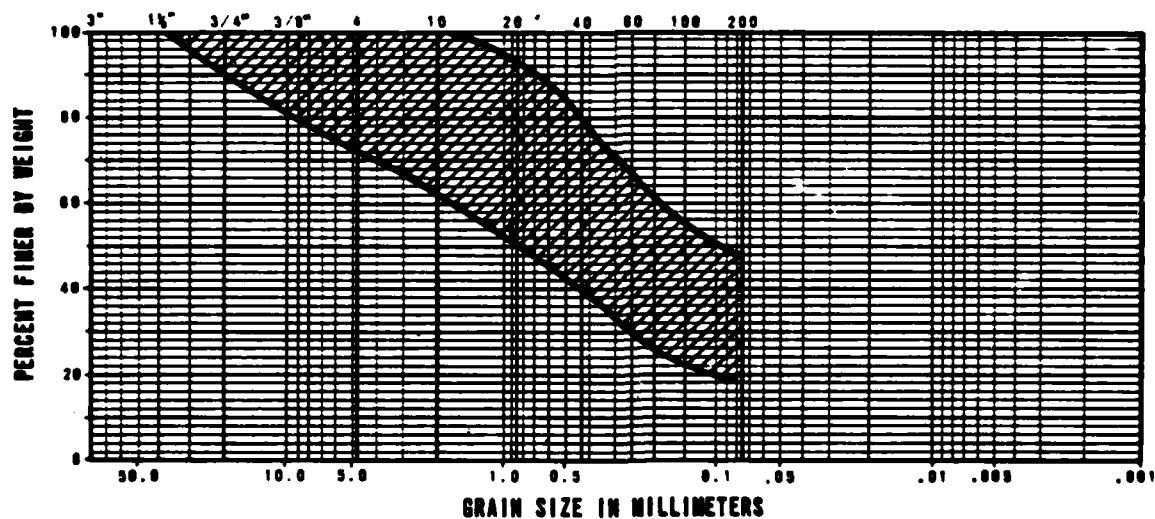
FUGRO NATIONAL, INC.

AFV-18

FN-TR-27-WA-I



SOIL DESCRIPTION: Sandy Gravels, Silty Gravels, Gravelly Sands and Sands
from 0 to 2 feet (0 to 0.6m)



SOIL DESCRIPTION: Silty Sands and Clayey Sands
from 0 to 2 feet (0 to 0.6m)

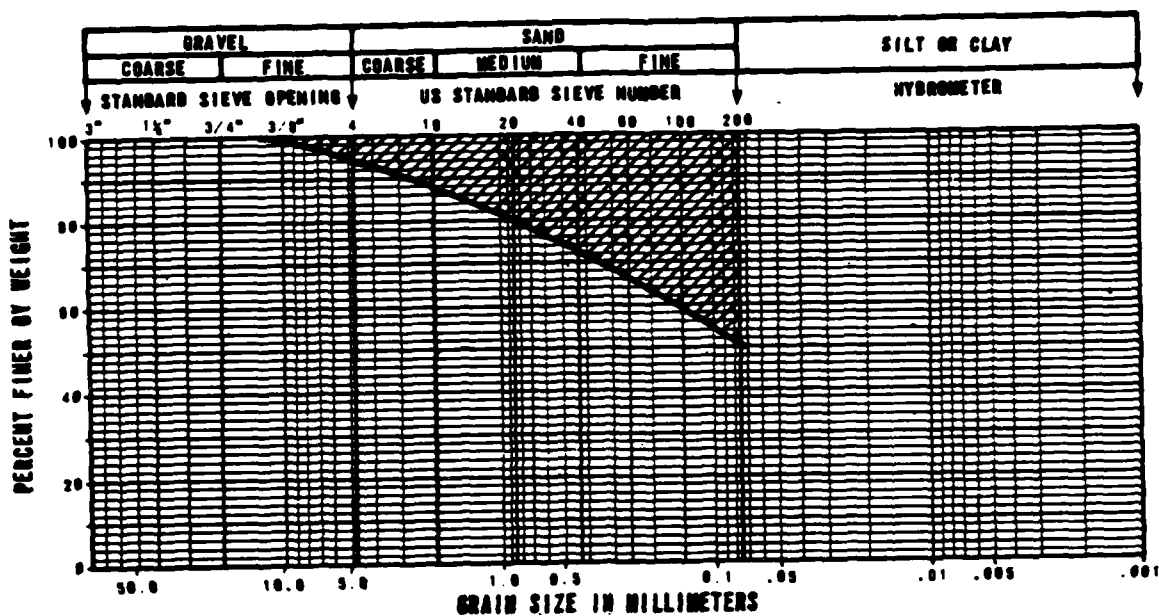
**RANGE OF GRADATION OF SURFICIAL SOILS
WAH WAH VALLEY, UTAH**

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - MNO

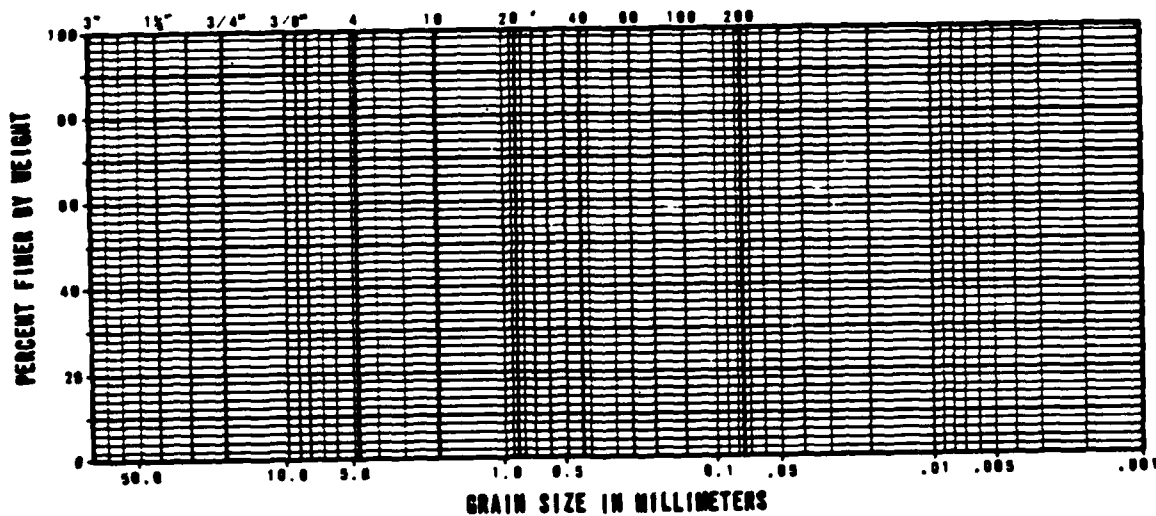
FIGURE
3-2
1 OF 2

FURRO NATIONAL INC.

FN-TR-27-WA-I



SOIL DESCRIPTION: Sandy Silts, Silts, Sandy Clays and Clays
from 0 to 2 feet (0 to 0.6m)



RANGE OF GRADATION OF SURFICIAL SOILS
WAH WAH VALLEY, UTAH

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - MDO

FIGURE
3-2
2 OF 2

FUGRO NATIONAL INC.

24 MAR 81

USAF-82

the valley flanks and in the younger alluvial fans associated with small tributary stream channels. The sands generally extend to the mountain fronts. The gravel content increases near the mountain fronts and locally grades into gravels. Gravelly sands and sandy gravels have a wide range of particle sizes and contain traces to some amounts of fines. Cobbles and boulders to 12 inches (30 cm) and even larger in size are occasionally encountered at or near the ground surface in these gravelly deposits. The percentage of cobbles and boulders is higher in the southern portion of the valley.

Silty sands and clayey sands also cover approximately 40 to 50 percent of the area. They are widely distributed, being the major component in all areas except alluvial fans very near the mountain fronts, alluvial fan deposits associated with small stream channels, and the lacustrine and active playa deposits in the northern part of the valley. The sands are coarse to fine and are poorly graded. They contain little to some amounts of fines and their plasticity ranges from nonplastic to slightly plastic. The fines content is highest near the playa and decreases toward the basin margin. Gravel content increases toward the mountain fronts.

Silts and clays cover approximately 10 to 20 percent of the valley. They consist of sandy silts, silts, sandy clays, and clays. They occur predominantly in the northern portion of the valley. These soils contain none to some amounts of sand. Their plasticity ranges from nonplastic to highly plastic.

3.3.2 Low-Strength Surficial Soil

Based on the Cone Penetrometer Test (CPT) results and soil classification, the thickness of low-strength surficial soil at each CPT location was estimated and is presented in Table 3-2.

Summaries of the range and mean thickness of the low-strength surficial soil for the three categories are included in Table 3-1. Sandy gravels, silty gravels, gravelly sands, and sands with low strength were observed to depths ranging from 0.5 to 8.1 feet (0.2 to 2.5 m) with an average of 2.0 feet (0.6 m). Silty and clayey sands with low strengths were found to depths ranging from 0.5 to 10.1 feet (0.2 to 3.1 m) with an average of 3.4 feet (1.0 m). The variation in the extent of low-strength granular soils is due to fluctuations in the in-situ density and calcium-carbonate cementation. Silts and clays exhibit low strength to depths ranging from 1.0 to 12.0 feet (0.3 to 3.7 m) with an average of 6.0 feet (1.8 m). The variation in the extent of low-strength, fine-grained soils is due to variations in the in-situ density, the amount of fine sand present, and calcium carbonate-cementation.

3.4. SUBSURFACE SOILS

Subsurface soils are predominantly coarse-grained (granular) except in the playa area in the northern part of the valley where fine-grained soils predominate. The coarse-grained soils consist of sandy gravels, clayey gravels, gravelly sands, sands, silty sands, and clayey sands. Subsurface soils within the playa area of the valley are predominantly fine-grained. These

| CONE PENETROMETER TEST NUMBER ⁽¹⁾ | THICKNESS OF LOW STRENGTH SURFICIAL SOIL, ⁽²⁾ | | SOIL TYPE ⁽³⁾ |
|--|---|--------|--------------------------|
| | FEET | METERS | |
| C-1 | 3.7 | 1.1 | SP-SM |
| C-2 | 6.6 | 2.0 | SM |
| C-3 | 3.0 | 0.9 | SM/GP-GC |
| C-4 | 1.9 | 0.6 | SM |
| C-5 | 0.9 | 0.3 | SM |
| C-6 | 1.2 | 0.4 | SM |
| C-7 | 1.0 | 0.3 | ML |
| C-8 | 1.5 | 0.5 | SM |
| C-9 | 7.4 | 2.3 | CL-ML/ML |
| C-10 | 6.3 | 1.9 | ML |
| C-11 | 4.5 | 1.4 | SC |
| C-12 | 10.0 | 3.0 | SM/SM-SC |
| C-13 | 2.4 | 0.7 | SM |
| C-14 | 4.3 | 1.3 | SM |
| C-15 | 1.5 | 0.5 | SM |
| C-16 | 0.5 | 0.2 | SM |
| C-17 | 4.9 | 1.5 | SM |
| C-18 | 1.2 | 0.4 | SM |
| C-19 | 1.1 | 0.3 | SM |
| C-20 | 2.5 | 0.8 | SM |
| C-21 | 6.7 | 2.0 | ML/SP-SM |
| C-22 | 3.6 | 1.1 | SM |
| C-23 | 9.5 | 2.9 | SM |
| C-24 | 1.1 | 0.3 | SM |
| C-25 | 0.8 | 0.2 | SW-SM |
| C-26 | 4.5 | 1.4 | SM |
| C-27 | 2.3 | 0.7 | SM |
| C-28 | 10.1 | 3.1 | SM |

| CONE PENETROMETER TEST NUMBER ⁽¹⁾ | THICKNESS OF LOW STRENGTH SURFICIAL SOIL, ⁽²⁾ | |
|--|---|--------|
| | FEET | METERS |
| C-29 | 4.0 | 1.2 |
| C-30 | 1.0 | 0.3 |
| C-31 | 2.4 | 0.7 |
| C-32 | 4.1 | 1.2 |
| C-33 | 1.8 | 0.5 |
| C-34 | 4.0 | 1.2 |
| C-35 | 6.3 | 1.9 |
| C-36 | 5.1 | 1.6 |
| C-37 | 0.9 | 0.3 |
| C-38 | 12.0 | 3.7 |
| C-39 | 0.5 | 0.2 |
| C-40 | 0.9 | 0.3 |
| C-41 | 1.0 | 0.3 |
| C-42 | 9.5 | 2.9 |
| C-43 | 2.9 | 0.9 |
| C-44 | 1.4 | 0.4 |
| C-45 | 0.8 | 0.2 |
| C-46 | 2.0 | 0.6 |
| C-47 | 4.1 | 1.2 |
| C-48 | 3.9 | 1.2 |
| C-49 | 7.1 | 2.2 |
| C-50 | 1.9 | 0.6 |
| C-51 | 2.0 | 0.6 |
| C-52 | 1.1 | 0.3 |
| C-53 | 2.6 | 0.8 |
| C-54 | 1.5 | 0.5 |
| C-55 | 3.9 | 1.2 |
| C-56 | 2.1 | 0.6 |

(1) For Cone Penetrometer Test locations see Drawing 3-1 Activity Location Map.

(2) Thickness corresponds to depth below ground surface. Low strength surficial soil is defined as soil which will perform poorly as a road subgrade at its present consistency. Low strength is based on Cone Penetrometer Test results using the following criteria:

Coarse grained soils: $q_c < 120$ tsf (117 kg/cm²)

Fine grained soils: $q_c < 80$ tsf (78 kg/cm²)

where q_c is cone resistance.

(3) Soil type is based on Unified Soil Classification System; see Section A5.0 in the Appendix for explanation

NOTES: • For fine grain strength surficial of the soil at

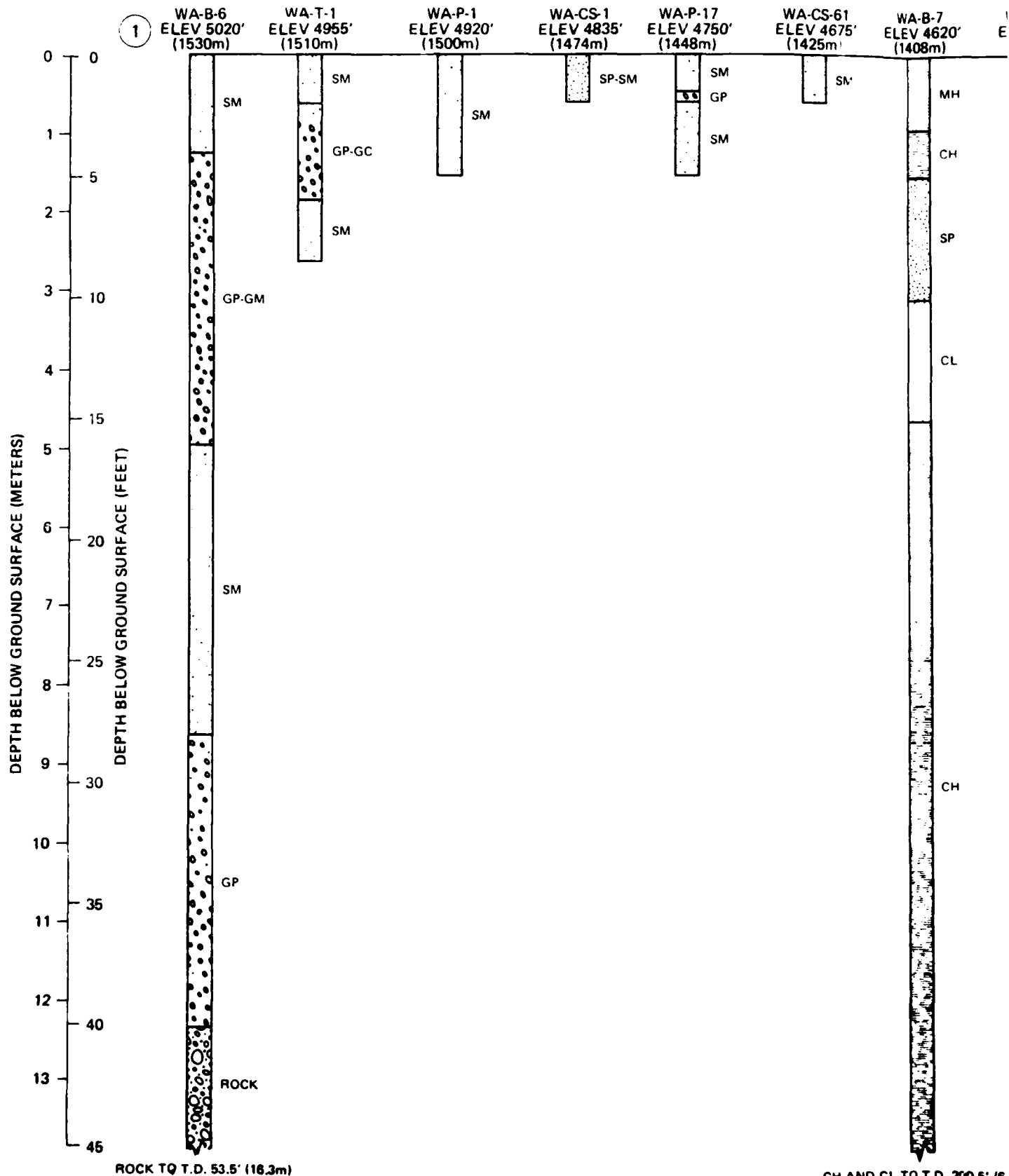
• SM/GM - indica

• NDA - No data

fine-grained soils consist of sandy silts, clayey silts, silts, sandy clays, and clays with plasticity ranging from nonplastic to highly plastic. At the playa margin, these fine-grained soils interfinger with the coarse-grained soils. Fine-grained soils are estimated to compose 25 to 35 percent of the subsurface deposits within the suitable area boundaries. This percentage of subsurface, fine-grained soils is higher than is found in most MX valleys because Wah Wah Valley has significantly more lacustrine deposits. The composition of subsurface soils with depth, as determined from borings, trenches, test pits, and surficial soil samples, is illustrated in the soil profiles presented in Figures 3-3 through 3-6.

Results of seismic and electrical surveys are summarized in Table 3-3. The characteristics of subsurface soils, determined from field and laboratory tests, are presented in Table 3-4. Ranges of gradation of the subsurface soils are shown in Figure 3-7. Coarse-grained subsurface soils are poorly to well-graded, contain coarse to fine sands and gravels, and are dense to very dense below 10 to 15 feet (3.6 to 4.6 m). Variable cementation occurs intermittently, but well-developed, continuous cementation was not encountered. These soils exhibit low compressibilities and moderate to high shear strengths.

Fine-grained soils (silts and clays) range in consistency from stiff to hard and exhibit low to moderate compressibilities and shear strengths. Soil plasticity ranges from nonplastic to highly plastic depending in part on the amount of fine sand

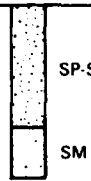


WA-CS-63
ELEV 4680'
(1426m)



SM

WA-P-18
ELEV 4720'
(1439m)



SP-SM

SM

WA-CS-65
ELEV 4730'
(1442m)



SM

WA-P-19
ELEV 4720'
(1439m)



GP-GM

CL

WA-CS-67
ELEV 4730'
(1442m)



SM

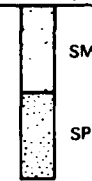
WA-CS-71
ELEV 4720'
(1439m)



SM

ML

WA-P-20
ELEV 4720'
(1439m)



SM

SP

WA-CS-69
ELEV 4760'
(1451m)



SM

CH

WA-T-20
ELEV 4840'
(1475m)



SM

SP

SM

GC

CL

1'

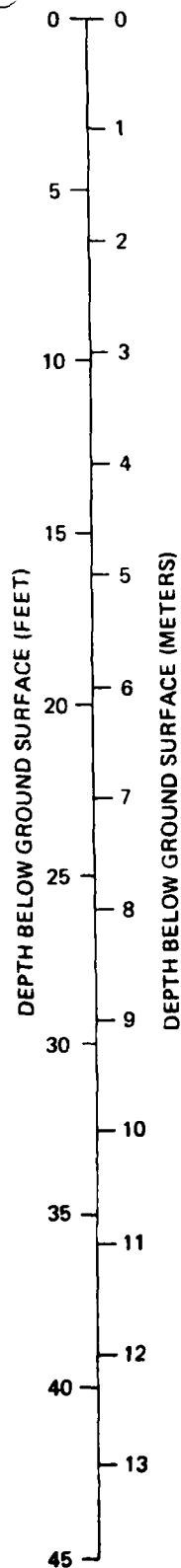
DEPTH BELOW GROUND SURFACE (FEET)

0
5
10
15
20
25
30
35
40
45

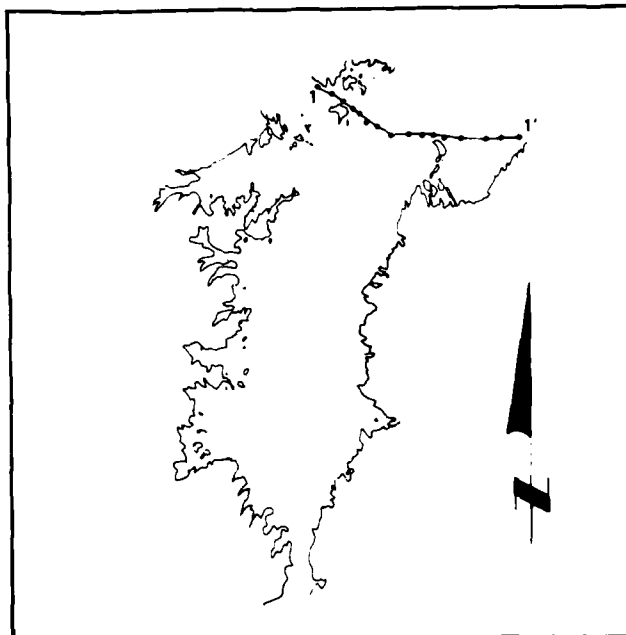
2

WA-T-20
ELEV 4840'
(1475m)

1'



LOCATION MAP



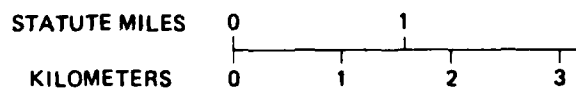
EXPLANATION

B - Boring
T - Trench
P - Test Pit
CS - Surficial soil sample at Cone Penetrometer Test location.

NOTES:

1. Ground surface elevations shown at activity locations are approximate.
2. T. D. = Total Depth.
3. Soil types shown adjacent to soil column are based on the Unified Soil Classification System (USCS) and are explained in the Appendix.

HORIZONTAL SCALE

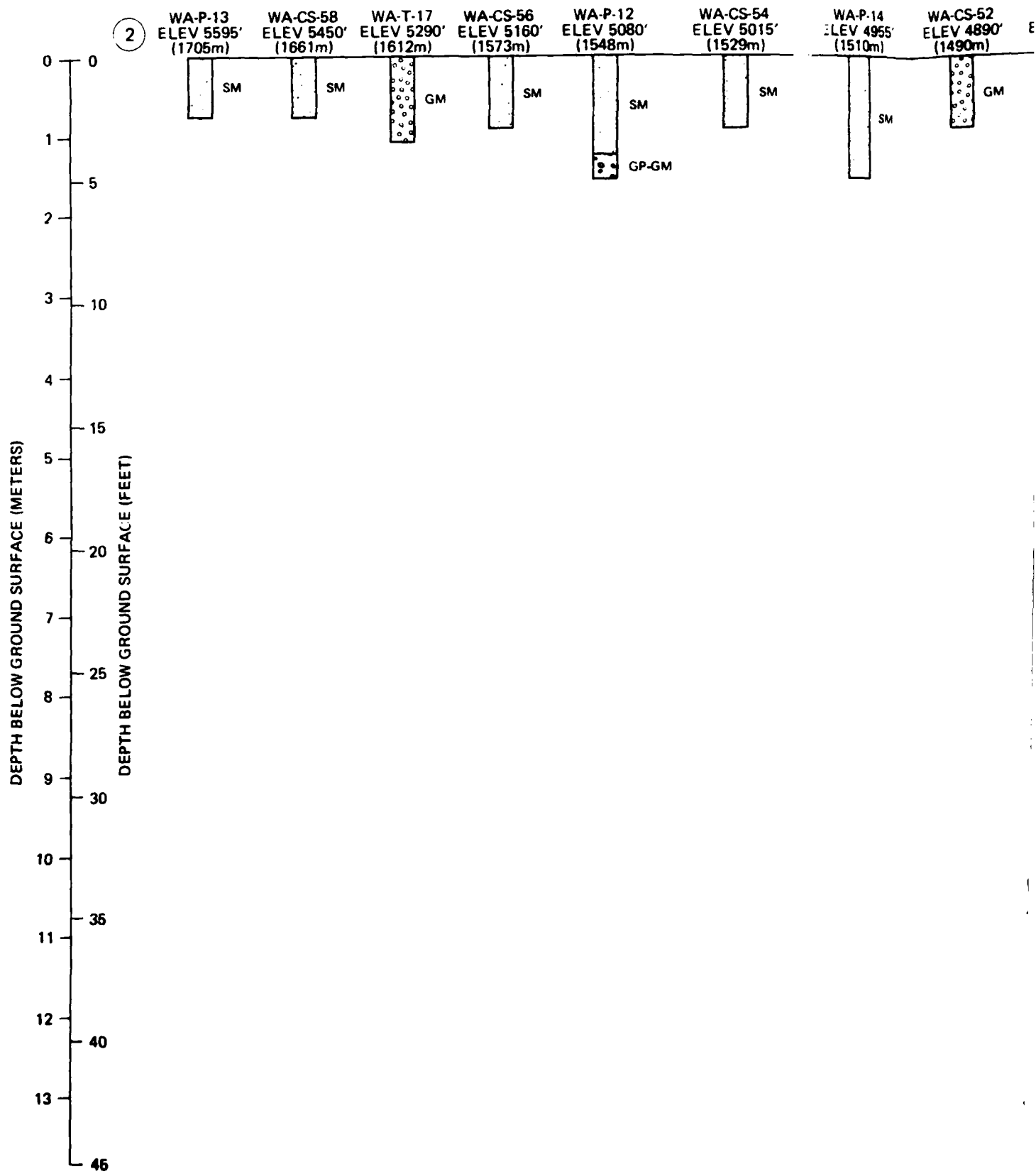


SOIL PROFILE 1-1' WAH WAH VALLEY, UTAH

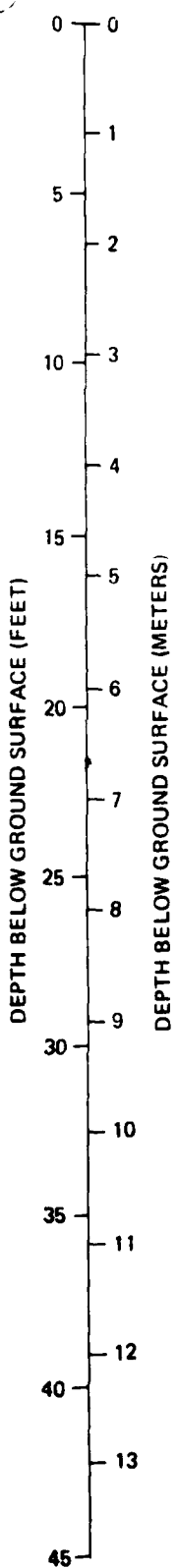
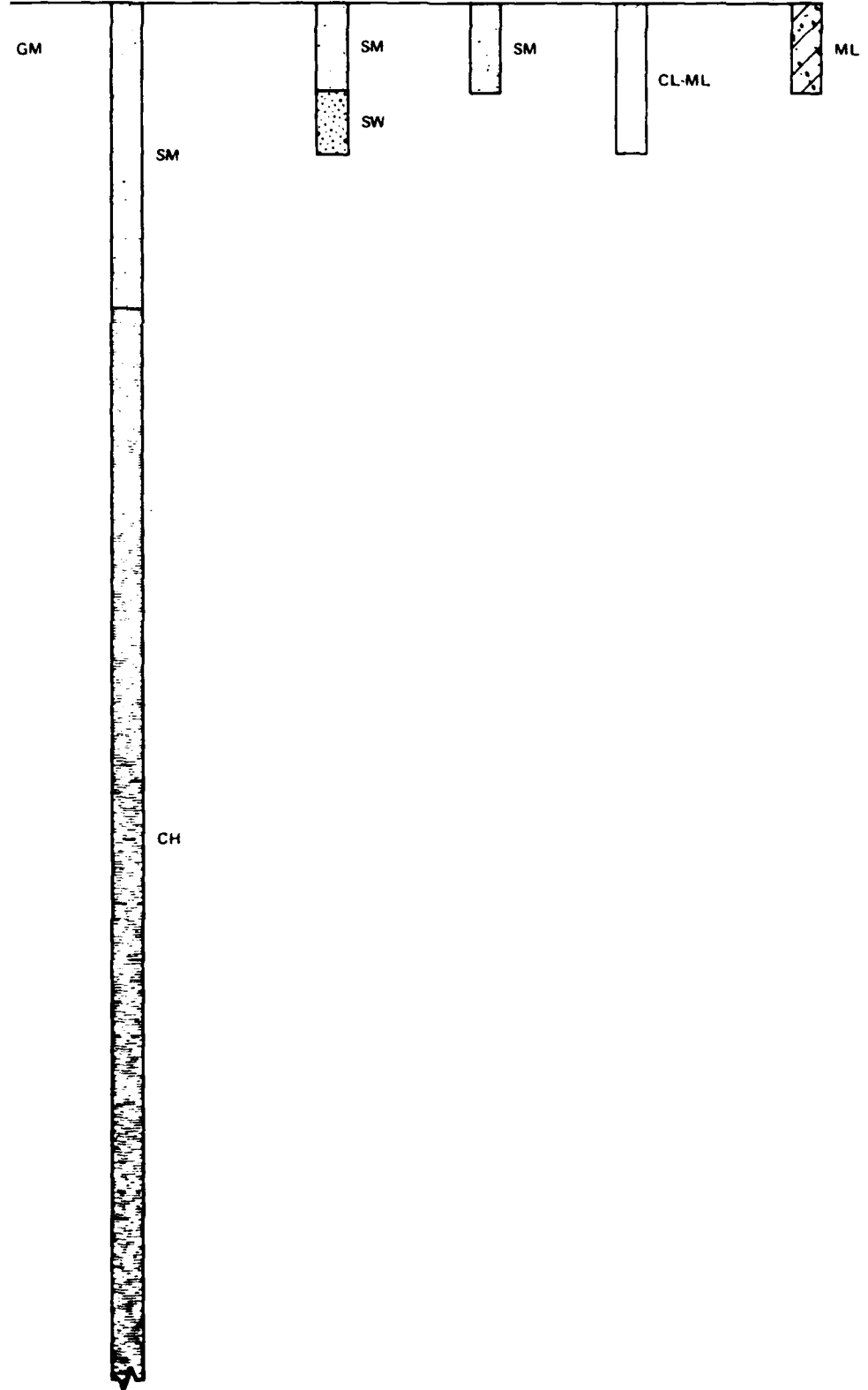
MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - BMO

FIGURE
3-3

FUGRO NATIONAL, INC.



52 390' n) WA-B-1 ELEV 4810' (1466m) WA-P-15 ELEV 4735' (1443m) WA-CS-49 ELEV 4700' (1433m) WA-P-16 ELEV 4655' (1419m) WA-CS-47 ELEV 4640' (1414m) 2'



B - Boring
T - Trench
P - Test Pit
CS - Surficial soil sample

NOTES:
1. Ground surface elevation
2. T. D. = Total Depth
3. Soil types shown in profile
Classification System

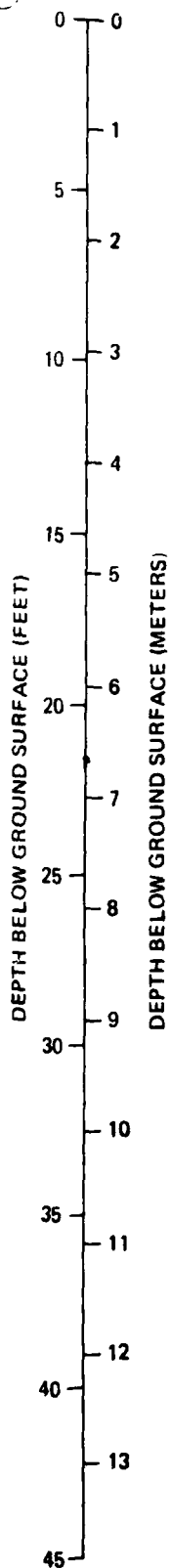
STATUTE MILE
KILOMETERS

GM, GC AND SP SM TO T.D. 160.0' (48.8m)

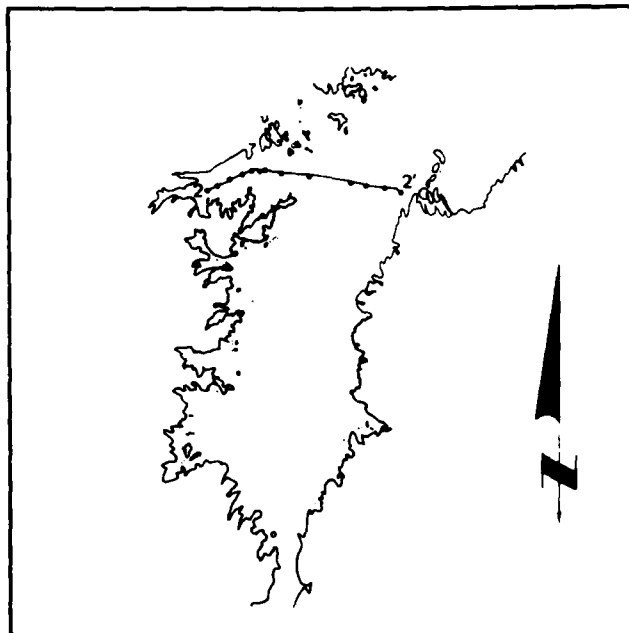
VA-CS-47
EV 4640'
(1414m)

2'

ML



LOCATION MAP



EXPLANATION

B - Boring
T - Trench
P - Test Pit
CS - Surficial soil sample at Cone Penetrometer Test location.

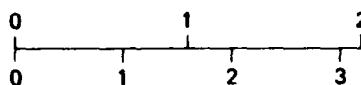
NOTES:

1. Ground surface elevations shown at activity locations are approximate.
2. T. D. = Total Depth.
3. Soil types shown adjacent to soil column are based on the Unified Soil Classification System (USCS) and are explained in the Appendix.

HORIZONTAL SCALE

STATUTE MILES

KILOMETERS



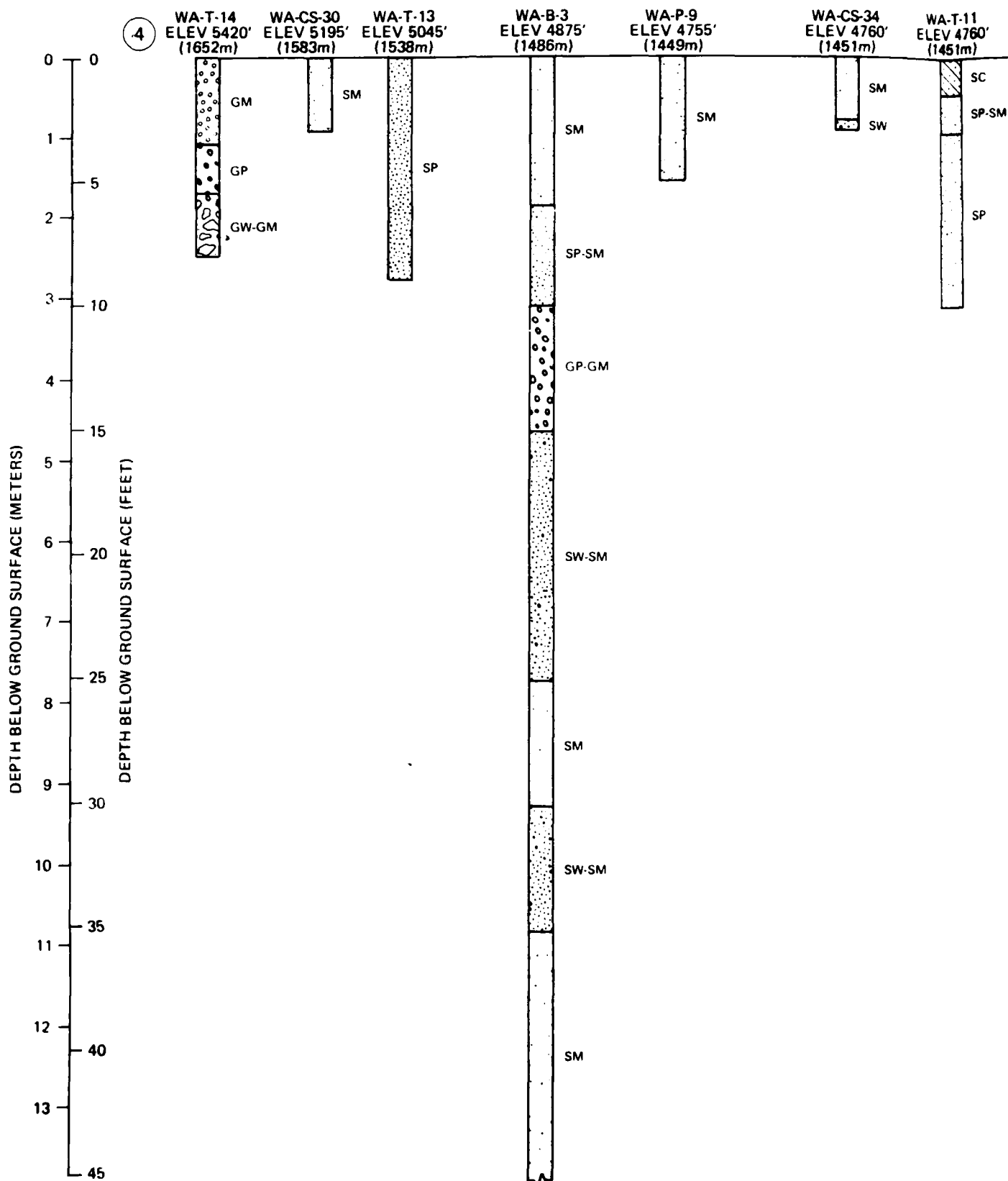
SOIL PROFILE 2-2'
WAH WAH VALLEY, UTAH

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - BMO

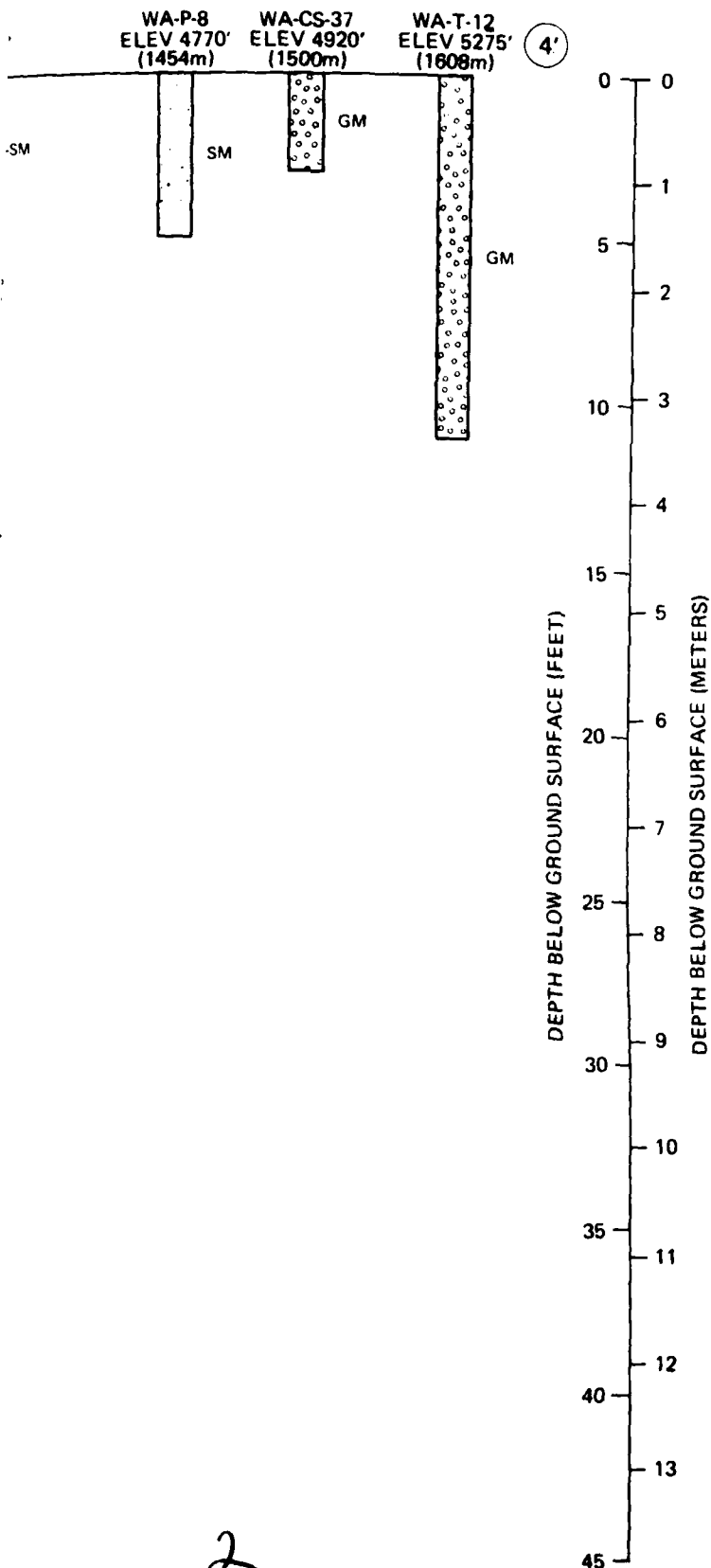
FIGURE
3-4

FUGRO NATIONAL, INC.

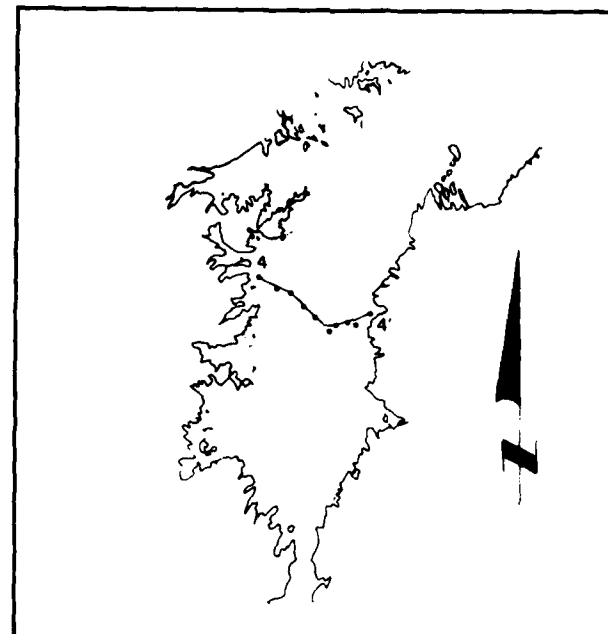
3



GP-GM, SW-SM, ML AND SM TO T.D. 160.0' (48.8m)



LOCATION MAP

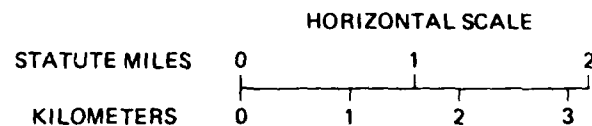


EXPLANATION

- B - Boring
T - Trench
P - Test Pit
CS - Surficial soil sample at Cone Penetrometer Test location.

NOTES:

1. Ground surface elevations shown at activity locations are approximate.
2. T. D. = Total Depth.
3. Soil types shown adjacent to soil column are based on the Unified Classification System (USCS) and are explained in the Appendix.

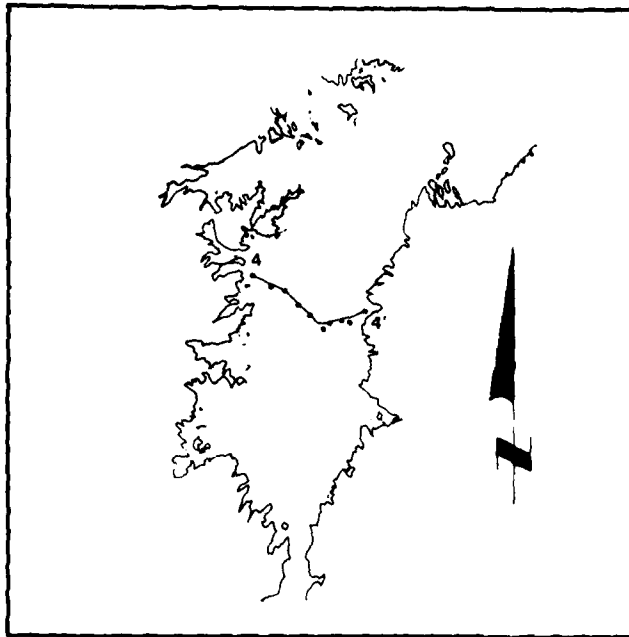


SOIL PROFILE 4-4'
WAH WAH VALLEY, UTAH

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - BMO

FUGRO NATIONAL

LOCATION MAP



EXPLANATION

- B - Boring
 T - Trench
 P - Test Pit
 CS - Surficial soil sample at Cone Penetrometer Test location.

NOTES:

1. Ground surface elevations shown at activity locations are approximate.
2. T. D. = Total Depth.
3. Soil types shown adjacent to soil column are based on the Unified Soil Classification System (USCS) and are explained in the Appendix.

HORIZONTAL SCALE


 SOIL PROFILE 4-4'
 WAH WAH VALLEY, UTAH

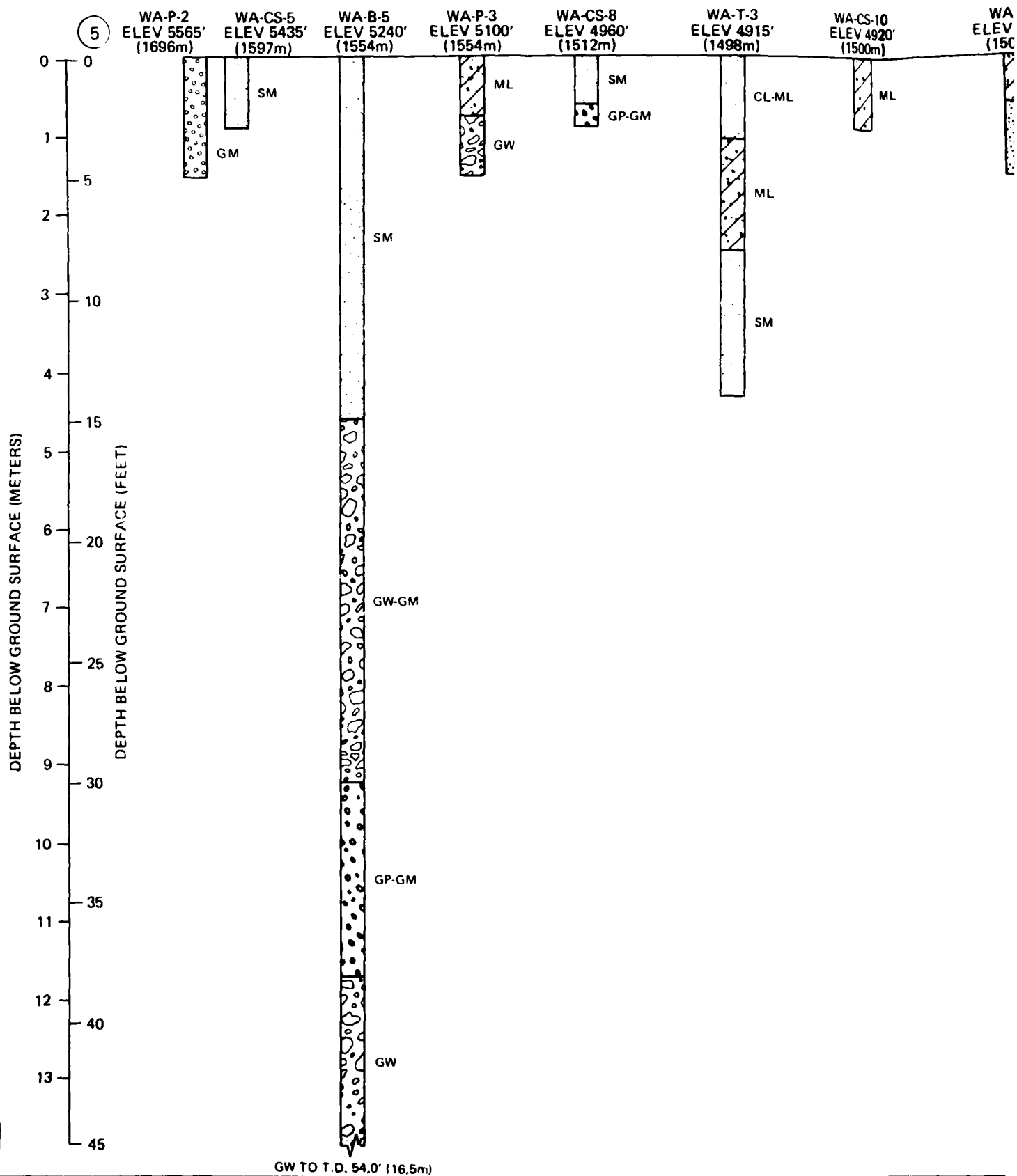
MX SITING INVESTIGATION
 DEPARTMENT OF THE AIR FORCE - BMO

FIGURE
 3-5

TUBRO NATIONAL, INC.

DEPTH BELOW GROUND SURFACE (METERS)

3



WA-P-7
EV 4950'
1509m)

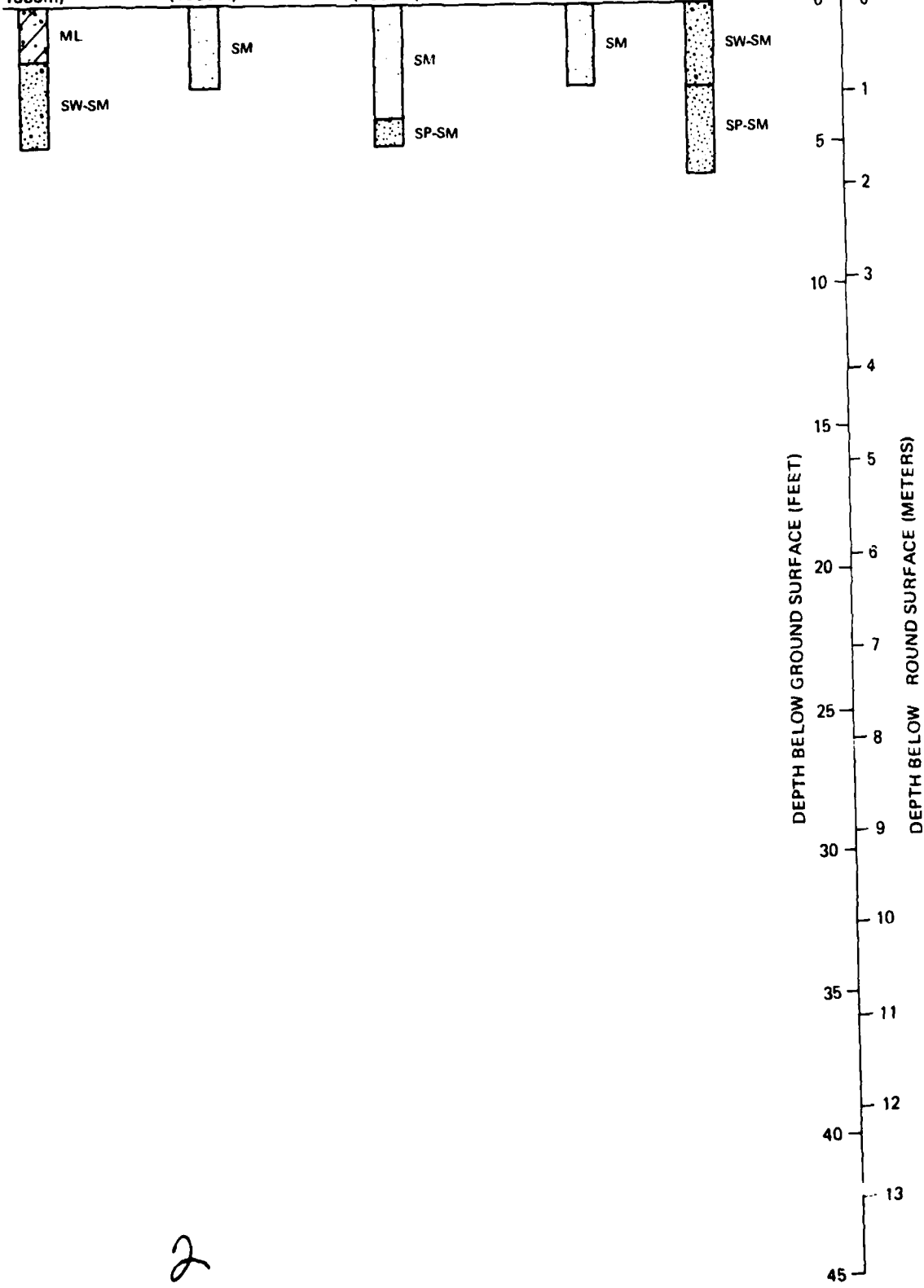
WA-CS-28
ELEV 5110'
(1558m)

WA-P-6
ELEV 5270'
(1606m)

WA-CS-26
ELEV 5560'
(1695m)

WA-T-10
ELEV 5720'
(1743m)

5'



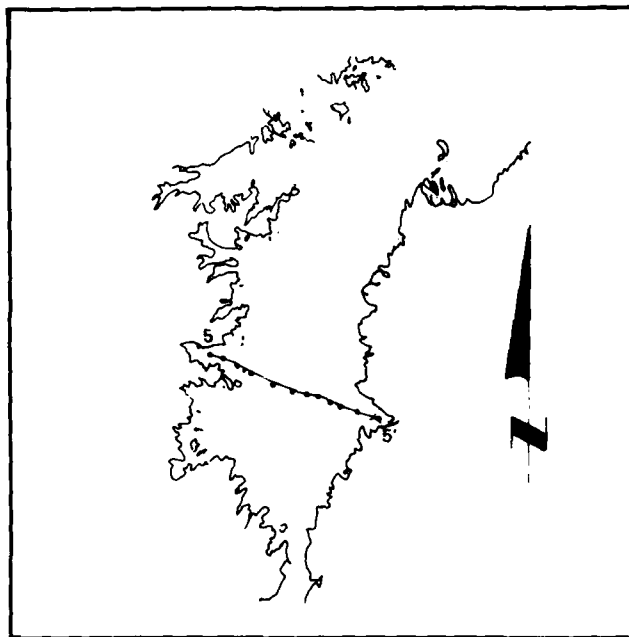
B - Boring
T - Trench
P - Test Pit
CS - Surficial soil sample

NOTES:
1. Ground surface elevation
2. T. D. = Total Depth
3. Soil types shown as per
Classification System

STATUTE MILES
KILOMETERS

2

LOCATION MAP



EXPLANATION

B - Boring
 T - Trench
 P - Test Pit
 CS - Surficial soil sample at Cone Penetrometer Test location.

NOTES:

1. Ground surface elevations shown at activity locations are approximate.
2. T. D. = Total Depth.
3. Soil types shown adjacent to soil column are based on the Unified Soil Classification System (USCS) and are explained in the Appendix.

HORIZONTAL SCALE



SOIL PROFILE 5-5'
 WAH WAH VALLEY, UTAH

MX SITING INVESTIGATION
 DEPARTMENT OF THE AIR FORCE - BMO

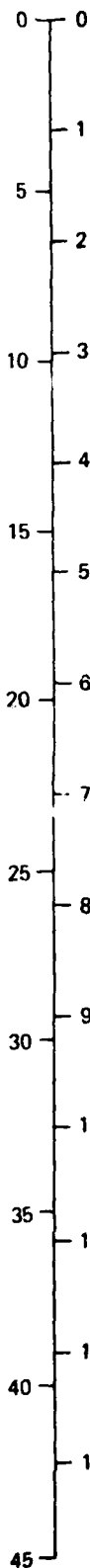
FIGURE
 3-6

FUGRO NATIONAL, INC.

3

DEPTH BELOW GROUND SURFACE (FEET)

DEPTH BELOW GROUND SURFACE (METERS)



0
 20'
 5'

SW-SM

SP-SM

FN-TR-27-WA-I

| ACTIVITY NO | S-1 | R-1 | S-2 | R-2 | S-3 | R-3 | S-4 | R-4 | S-5 | R-5 | S-6 | R-6 | S-7 | R-7 | S-8 | R-8 | S-9 | R-9 |
|-------------------|----------------|-------|----------------|-------|----------------|-------|----------------|-------|----------------|-------|----------------|-------|----------------|-------|---------------|-------|----------------|-------|
| DEPTH (m) (ft) | fps (mps) | ohm-m | fps (mps) | ohm-m | fps (mps) | ohm-m | fps (mps) | ohm-m | fps (mps) | ohm-m | fps (mps) | ohm-m | fps (mps) | ohm-m | fps (mps) | ohm-m | fps (mps) | ohm-m |
| 0 | 1300 (396) | 16 | 1420 (433) | 110 | 1320 (402) | 30 | 1550 (472) | 60 | 1690 (515) | 115 | 1780 (543) | 230 | 1430 (436) | 70 | 1380 (421) | 30 | 1440 (439) | 30 |
| 10 | 2400 (732) | | | | | | | | | | | | | | | | | |
| 5 | | 85 | | | 4250 (1295) | | 2350 (716) | 40 | 3600 (1097) | 20 | 3550 (1082) | | 2500 (762) | 25 | 2000 (610) | | | |
| 20 | | | 3400 (1036) | | | | | 50 | 8550 (2606) | | | 100 | | | | 50 | 2750 (838) | 8 |
| 30 | | | | 13 | | | | | | | | 40 | | | | | | 3 |
| 40 | 4850 (1478) | 170 | | | | 55 | | | | 12 | | | | | | 80 | 4750 (1448) | |
| 15 | | | | 160 | | 340 | | | | 45 | 4550 (1387) | | | | | | | |
| 60 | | | | | | | | | | | | 65 | | | 2550 (777) | | | |
| 20 | | 250 | | | | | | 30 | | | | | | 730 | | | | |
| 70 | | | | | | | | | | | | | 3800 (1158) | | | | | |
| 25 | | | 9650 (2941) | | | 950 | 6400 (1950) | | | | | | | | | | | |
| 80 | | | | | | | | | | | | 340 | | | | | 6700 (2042) | |
| 90 | | | | | | | | | | | | | | | | | | |
| 30 | | | | 640 | 6800 (2072) | | | | | 15 | | | | | | | | |
| 100 | | | | | | | | | | | | | | | | | | |
| 110 | | | | | | | | | | | | | | | | | | |
| 35 | | | | | | | | | | | | | | | | 360 | | |
| 120 | | | | | | | | | | | | | | | | | | |
| 40 | | | | | | | | | | | | | | | | | | |
| 130 | | | | | | | | | | | | | | | | | | |
| 140 | | | | | | | | | | | | | | | | | | |
| 45 | | | | | | | | | | | | | | | | | | |
| 150 | | | | | | | | | | | | | | | | | | |
| * ft (m) | 101 (31) | | | | | | 78 (24) | | | | 145 (44) | | 160 (49) | | | | 106 (32) | |

Deeper Results
Velocity/Resistivity @ Depth

- Approximate depth above which there is no indication of material with a velocity as great as 7000 fps (2134 mps). See Appendix A for an explanation of how this exclusion depth is calculated when the observed velocities are all less than 7000 fps (2134 mps).

6050 @ 154
(1844) (47)

| 14 | S-15 | R-15 | S-16 | R-16 | S-17 | R-17 | S-18 | R-18 | S-19 | R-19 | S-20 | R-20 | S-21 | R-21 | DEPTH (ft) m |
|-----|----------------|-------|----------------|-------|----------------|-------|----------------|-------|----------------|-------|----------------|-------|----------------|-------|-----------------|
| m-m | fps (mps) | ohm-m | fps (mps) | ohm-m | fps (mps) | ohm-m | fps (mps) | ohm-m | fps (mps) | ohm-m | fps (mps) | ohm-m | fps (mps) | ohm-m | 0 |
| 30 | 1540 (469) | 16 | 1390 (424) | 25 | 1340 (408) | 60 | 1370 (418) | 5 | 1440 (439) | 95 | 1660 (506) | 50 | 1610 (491) | 100 | 10 |
| | 2600 (792) | 140 | | | | 30 | | 25 | 4000 (1219) | 25 | 2900 (884) | 25 | 3100 (945) | 30 | 5 |
| 100 | | | 3750 (1143) | 100 | 2350 (716) | | 2050 (625) | 100 | | 12 | | | | 13 | 20 |
| | | | 7200 (2195) | | | 160 | 3450 (1052) | 340 | | 200 | 210 | 75 | 3750 (1143) | 240 | 30 |
| | 3350 (1021) | 160 | | | 6700 (2042) | | | | | | 8500 (2591) | | | | 15 |
| 170 | | | | 2390 | | | | | | | | 30 | | | 20 |
| | 194 (59) | | | | 101 (31) | | 173 (53) | | 134 (41) | | | | 167 (51) | | 25 |
| | | | | | | | | | | | | | | | 30 |
| | | | | | | | | | | | | | | | 35 |
| | | | | | | | | | | | | | | | 40 |
| | | | | | | | | | | | | | | | 45 |
| | | | | | | | | | | | | | | | 50 |
| | | | | | | | | | | | | | | | 55 |
| | | | | | | | | | | | | | | | 60 |
| | | | | | | | | | | | | | | | 65 |
| | | | | | | | | | | | | | | | 70 |
| | | | | | | | | | | | | | | | 75 |
| | | | | | | | | | | | | | | | 80 |
| | | | | | | | | | | | | | | | 85 |
| | | | | | | | | | | | | | | | 90 |
| | | | | | | | | | | | | | | | 95 |
| | | | | | | | | | | | | | | | 100 |
| | | | | | | | | | | | | | | | 105 |
| | | | | | | | | | | | | | | | 110 |
| | | | | | | | | | | | | | | | 115 |
| | | | | | | | | | | | | | | | 120 |
| | | | | | | | | | | | | | | | 125 |
| | | | | | | | | | | | | | | | 130 |
| | | | | | | | | | | | | | | | 135 |
| | | | | | | | | | | | | | | | 140 |
| | | | | | | | | | | | | | | | 145 |
| | | | | | | | | | | | | | | | 150 |

SEISMIC REFRACTION AND
ELECTRICAL RESISTIVITY RESULTS
WAH WAH VALLEY, UTAH

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE

000

TABLE
3-3

FUGRO NATIONAL, INC.

AFV-16

| DEPTH RANGE | 2' - 20' (0.6 - 6.0m) | |
|---|---|--|
| SOIL DESCRIPTION | Coarse-grained soils | Fine-grained soils |
| | Sandy Gravels, Clayey Gravels, Gravelly Sands, Sands, and Silty Sands | Sandy Silts, Clayey Silts, Sandy Clays, and Clay |
| USCS SYMBOLS | GW, GP, GC, SW, SP, SM | ML, CL, MH, CH |
| ESTIMATED EXTENT IN SUBSURFACE % | 70 - 80 | 20 - 30 |
| PHYSICAL PROPERTIES | | |
| DRY DENSITY pcf (kg/m ³) | 81.4 - 126.5 (1304 - 2026) [16] | 68.3 - 109.1 (1094 - 1748) |
| MOISTURE CONTENT % | 1.5 - 3.1 [17] | 7.5 - 29.2 |
| DEGREE OF CEMENTATION | moderate to strong | moderate |
| COBBLES 3 - 12 inches (8 - 30 cm) % | 0 - 15 | 0 |
| GRAVEL % | 0 - 65 [39] | 0 - 9 |
| SAND % | 18 - 94 [39] | 0 - 47 |
| SILT AND CLAY % | 2 - 46 [39] | 51 - 100 |
| LIQUID LIMIT | 23 - 49 [2] | 21 - 67 |
| PLASTICITY INDEX | NP - 19 [3] | 3 - 44 |
| COMPRESSIONAL WAVE VELOCITY fps (mps) | 1300 - 4600 (396 - 1402) [42] | 1320 - 1370 (402 - 418) |
| SHEAR STRENGTH DATA | | |
| UNCONFINED COMPRESSION S_u - ksf (kN/m ²) | NDA | 0.7 (34) |
| TRIAXIAL COMPRESSION c - ksf (kN/m ²), ϕ° | NDA | NDA |
| DIRECT SHEAR c - ksf (kN/m ²), ϕ° | $C = 0.0 - 1.0$, $\phi = 32 - > 45^\circ$ (0 - 48) [3] | $C = 0.5$, $\phi = 32$ (24) |

NOTES:

- Characteristics of soils between 2 and 20 feet (0.6 and 6.0 meters) are based on results of tests on samples from 7 borings, 13 trenches, and 5 test pits, and results of 21 seismic refraction surveys.
- Characteristics of soils below 20 feet (6.0 meters) are based on results of tests on samples from 7 borings and results of 21 seismic refraction surveys.

- [] - Number
- NDA - No data available
- - High angle

| 20' - 160' (6.0 - 49.0m) | | |
|--|---|---|
| ne-grained soils | Coarse-grained soils | Fine-grained soils |
| its, Clayey Silts, Silts, ays, and Clays | Sandy Gravels, Gravelly Sands, Sands, Silty Sands, and Clayey Sands | Sandy Silts, Sandy Clays, and Clays |
| MH, CH | GW, GP, GC, SW, SP, SM, SC | ML, CL, CH |
| | 65 - 75 | 25 - 35 |
| | | |
| 9.1 (48) [9] | 93.6 - 130.3 (1499 - 2087) [37] | 84.8 - 117.5 (1358 - 1882) [50] |
| [9] | 3.4 - 28.4 [38] | 2.9 - 34.5 [50] |
| | moderate | moderate |
| | 0 - 5 | 0 - 5 |
| [16] | 1 - 64 [17] | 0 - 2 [14] |
| [16] | 34 - 85 [17] | 0 - 44 [14] |
| [16] | 1 - 37 [17] | 54 - 100 [14] |
| [12] | 25 - 48 [2] | 56 - 67 [11] |
| [12] | NP - 29 [3] | 29 - 46 [11] |
| 70 8) [2] | 2000 - 6800 (610 - 2072) [34] | NDA |
| | | |
| [1] | NDA | 10.5 (503) [1] |
| | C = 1.2, $\phi = 30$ (57) [1] | C = 2.0 - 4.6, $\phi = 12 - 42$ (96 - 220) [3] |
| z = 32 [1] | C = 0.0 - 2.5, $\phi = 35 - > 45^*$ (0 - 120) [2] | C = 4.0, $\phi = 34$ (192) [1] |

- Number of tests performed.

No data available (insufficient data or tests not performed.)

High angle due to large gravels and/or cementation.

2

CHARACTERISTICS OF SUBSURFACE SOILS
WAH WAH VALLEY, UTAH

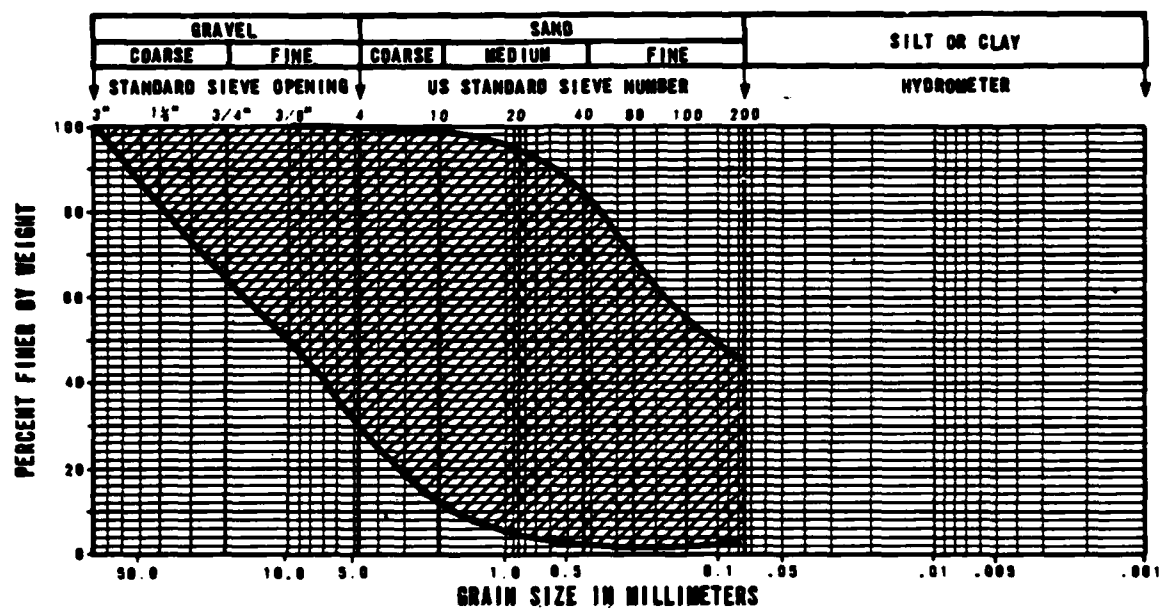
MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - DMO

TABLE
3-4

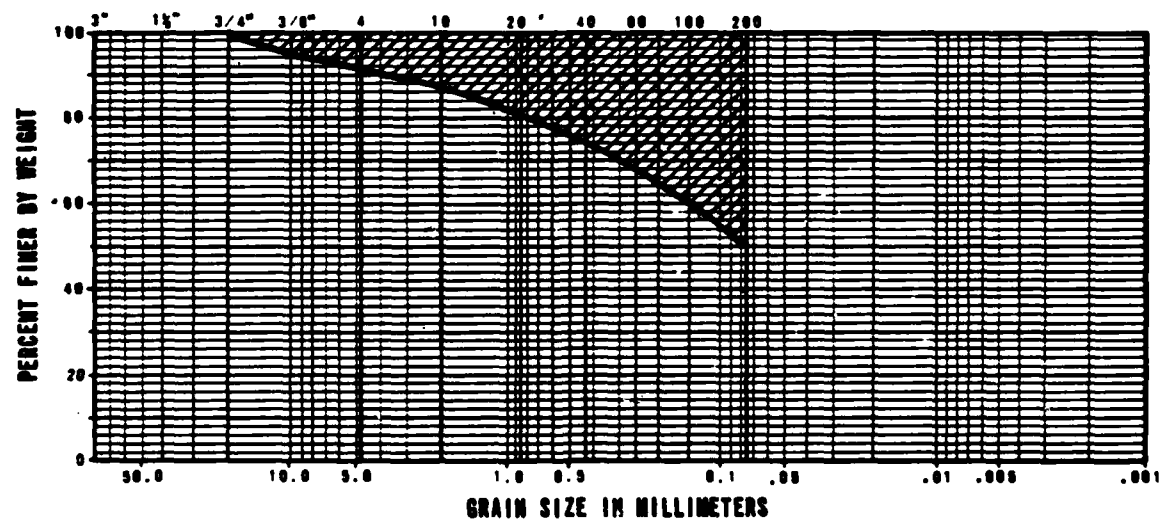
TURRO NATIONAL, INC.

AFV-20

FN-TR-27-WA-I



SOIL DESCRIPTION: Coarse - Grained Soils
from 2 to 20 feet (0.6 to 6.0m)



SOIL DESCRIPTION: Fine - Grained Soils
from 2 to 20 feet (0.6 to 6.0m)

**RANGE OF GRADATION OF SUBSURFACE SOILS
WAH WAH VALLEY, UTAH**

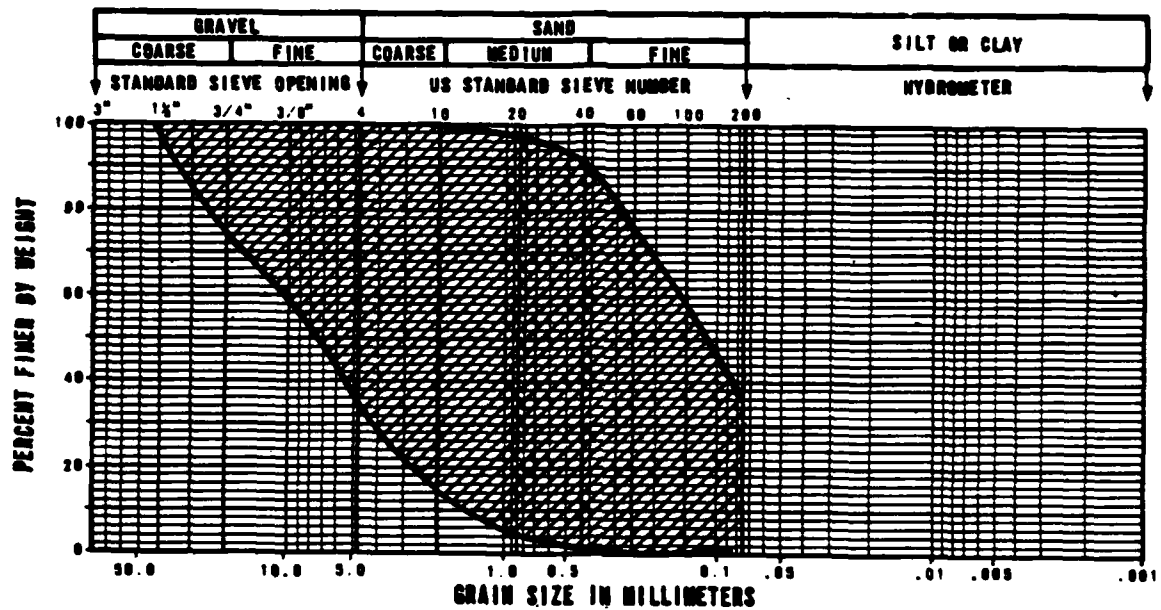
MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - DMO

FIGURE
3-7
1 OF 2

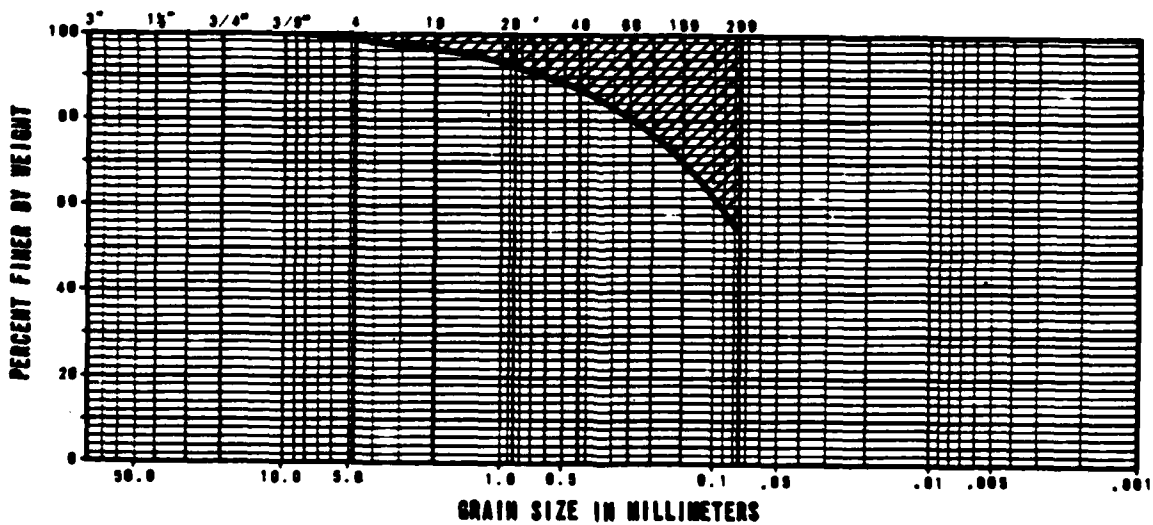
FUGRO NATIONAL INC.

24 MAR 81

USAF-82



SOIL DESCRIPTION: Coarse - Grained Soils
from 20 to 160 feet (6.0 to 49.0m)



SOIL DESCRIPTION: Fine - Grained Soils
from 20 to 160 feet (6.0 to 49.0m)

**RANGE OF GRADATION OF SUBSURFACE SOILS
WAH WAH VALLEY, UTAH**

**MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - HHS**

**FIGURE
3-7
2 OF 2**

USARO NATIONAL INC.

present. Calcium-carbonate cementation is usually from weak to moderate, depending on the age of the deposit.

The soils in the construction zone (120 feet [37 m]) have a wide range of seismic compressional wave velocities (1300 to 6800 fps [396 to 2072 mps]) depending on their composition, consistency, cementation, and moisture content. Compressional wave velocities for deeper materials are listed in Table 3-3. The soil types represented by these velocities are unknown.

Electrical conductivity measured for the soils in the upper 50 feet (15 m) ranged from 0.0006 to 0.0294 mhos per meter (average 0.0126 mhos per meter). At two of the 21 measurement locations, the measured conductivities were less than the minimum value of 0.004 mhos per meter specified in the Fine Screening criteria.

Results of chemical tests indicate that potential for sulfate attack of soils on concrete will range from "negligible" to "severe." The "severe" rating is associated with soils in the vicinity of the Wah Wah Valley Hardpan (see Drawing 2-1) at the northern end of the valley.

3.5 DEPTH TO ROCK

Subsurface data concerning depth to rock in the valley were obtained from several borings, seismic refraction lines, and published well data (Drawing 3-3). Three water wells near the southern end of the valley (W-3, W-4, W-5, Table II-2-1) penetrated rock at depths ranging from 715 feet to 1406 feet (218 m to 429 m). Two shallow FNI borings (B-5 and B-6), located near

the rock line, penetrated rock at depths of less than 50 feet (15 m).

Drawing 3-3 shows the interpreted 50- and 150-foot- (15- and 46-m-) depth-to-rock contours in Wah Wah Valley.

The rock-alluvium contact on the western side of the valley is highly irregular, and many small outcrops of volcanic rock were mapped as far as one-half mile (0.8 km) into the valley. Rock shallower than 50 feet (15 m) was interpreted to occur in a strip varying from one-tenth of a mile (0.2 km) to two miles (3.2 km) in width along the valley's entire western margin.

The eastern side of the valley is characterized by a fairly regular mountain front interrupted by a few narrow reentrant canyons. These canyons contain alluvial fan sediments interpreted to be thin veneers over bedrock. Along most of the eastern valley margin, the area where rock is interpreted to be less than 50 feet (15 m) deep forms a strip generally less than one-quarter mile (0.4 km) wide.

3.6 DEPTH TO WATER

Drawing 3-4 shows the locations of all data points used to define ground-water conditions in Wah Wah Valley. The sources of this information, in addition to FNI activities, are the Utah State Engineer's Office (1979) and Stephens (1974).

A broad alluvial high in the northern part of the valley acts as a topographic drainage divide between Sevier Lake and Wah Wah

Valley. North of the divide, around Sevier Lake (at the northeastern edge of the mapped area), four FNI observations wells define 50- and 150-foot- (15- and 46-m-) depth-to-water contours. Surface water is often present in Sevier Lake. South of the drainage divide, within the Wah Wah Valley basin, depth to water is greater than 200 feet (61 m) near the playa (W-1, Table II-2-1) and greater than 500 feet (152 m) at the southern end of the valley. Fault-controlled springs (Section 3.2.1) are present along the valley margins, indicating that localized shallow water may exist in some of the canyons.

3.7 TERRAIN

3.7.1 Terrain Exclusions

Terrain conditions are shown in Drawing 3-5. Areas designated as terrain exclusions are considered to be unsuitable based on a combination of field- and office-derived data which were evaluated under the criteria in Appendix Table A2-1. Field derived exclusions include: 1) areas having very steep slopes, such as the sides of major drainages, and 2) areas in which incisions deeper than 10 feet (3 m) are spaced closer than 1000 feet (305 m) apart. Office-derived exclusions consist primarily of identifying areas on topographic maps that have slopes greater than 10 percent. In some instances, where road access is inadequate for field work, office analysis of aerial photographs is also used to define and exclude areas of rugged or adverse terrain. However, preference was given to determining such exclusions in the field.

Even though areas where slopes exceed five percent are considered to be suitable, they are shown on Drawing 3-5, because they require special consideration in planning construction and operations.

Several parts of Wah Wah Valley are excluded based on the terrain criteria. On the eastern and northeastern sides of the valley, areas with slopes exceeding 10 percent form a band adjacent to the mountains that ranges up to 2 miles (3.2 km) in width. The mountains on the western side of the valley are bordered for most of their length by narrow (less than one-quarter mile [0.4 km] wide) strips of land with slopes greater than 10 percent.

3.7.2 Incision Depth and Number of Drainages Per Mile

Data on drainage incision depths and number of drainages encountered per mile were collected for Wah Wah Valley. Information on incision depths was obtained from field observations; the number of drainages per mile was determined from both field observations and interpretation of aerial photographs.

Applicable data were analyzed for the prevalent surficial geologic units with the results shown in Table 3-5. Average values of the two terrain characteristics are reported for each prevalent surficial unit with further breakdowns providing data on: 1) portions of the unit on the eastern side of the valley axial drainage versus those on the western side, and 2) portions of the unit whose surface slopes are between five and 10 percent versus those whose slope is less than five percent.

| SURFICIAL GEOLOGIC UNIT | AVERAGE NUMBER OF DRAINAGES PER MILE | | | |
|----------------------------|--------------------------------------|--------|------------------------|-----------|
| | WESTERN SIDE OF VALLEY | | EASTERN SIDE OF VALLEY | |
| | SURFACE SLOPE, % | | SURFACE SLOPE, % | |
| | 0-5 | 5-10 | 0-5 | 5-10 |
| A5i ^g s | — 7.5 (3.7) | — — | — 6.3 (2.9) | — — |
| A5ys | 6.3 (4.2) | — | 5.8 (3.2) | — |
| A4os | 8.4 (4.9) | — | 8.3 (5.3) | 6.5 (3.6) |
| A4f | — | — | 1.2 (2.2) | — |

NOTE: DRAINAGES WERE COUNTED ALONG A ONE-MILE LINE PERPENDICULAR TO THE DRAINAGE DIRECTION

| SURFICIAL GEOLOGIC UNIT | AVERAGE DEPTH OF INCISIONS | | | |
|----------------------------|---------------------------------------|---------------------------------------|---|-------------------------------------|
| | WESTERN SIDE OF VALLEY | | EASTERN SIDE OF VALLEY | |
| | SURFACE SLOPE, % | | SURFACE SLOPE, % | |
| | 0-5 | 5-10 | 0-5 | 5-10 |
| A5i ^g s | — 4.4 ft (2.2 ft) 1.3 m (0.8 m) | — 6.5 ft (3.6 ft) 2.0 m (1.1 m) | 8.0 ft * 2.4 m 4.2 ft (2.9 ft) 1.3 m (0.9 m) | — 1.5 ft * 1.4 m |
| A5ys | 3.4 ft (2.1 ft) 1.0 m (0.6 m) | — | 3.6 ft (2.5 ft) 1.1 m (0.8 m) | 5.0 ft * 1.5 m |
| A4os | 3.9 ft (2.7 ft) 1.2 m (0.8 m) | — | 6.7 ft (4.0 ft) 2.0 m (1.2 m) | 14.3 ft (38.0 ft) 4.4 m (11.6 m) |
| A4f | — | — | — | — |

- LIMITED DATA (6 ≤ n < 10) VALUE IS MEDIAN, NO STANDARD DEVIATION
- NO DATA OR INSUFFICIENT DATA (n < 6)
- () STANDARD DEVIATION
- A5i INTERMEDIATE-AGE ALLUVIAL FANS
- A5y YOUNG-AGE ALLUVIAL FANS
- A4o OLDER LACUSTRINE DEPOSITS
- A4 ACTIVE PLAYAS
- g GRAVELS
- s SANDS
- f FINES: CLAYS, SILTS

DRAINAGES PER MILE AND DEPTH OF INCISIONS
IN PREVALENT SURFICIAL GEOLOGIC UNITS
WAH WAH VALLEY, UTAH

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - BMO

TABLE
3-5

FUGRO NATIONAL, INC.

AD-A113 392

FUGRO NATIONAL INC LONG BEACH CA
VERIFICATION STUDY - WAM WAM VALLEY, UTAH. VOLUME I. SYNTHESIS. (U)
MAR 81 F04704-80-C-0006
FN-TR-27-WA-VOL-1

F/G 13/2

UNCLASSIFIED

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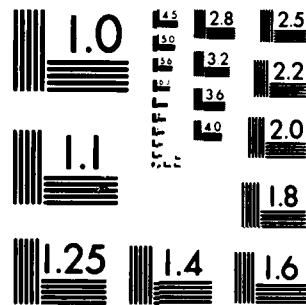
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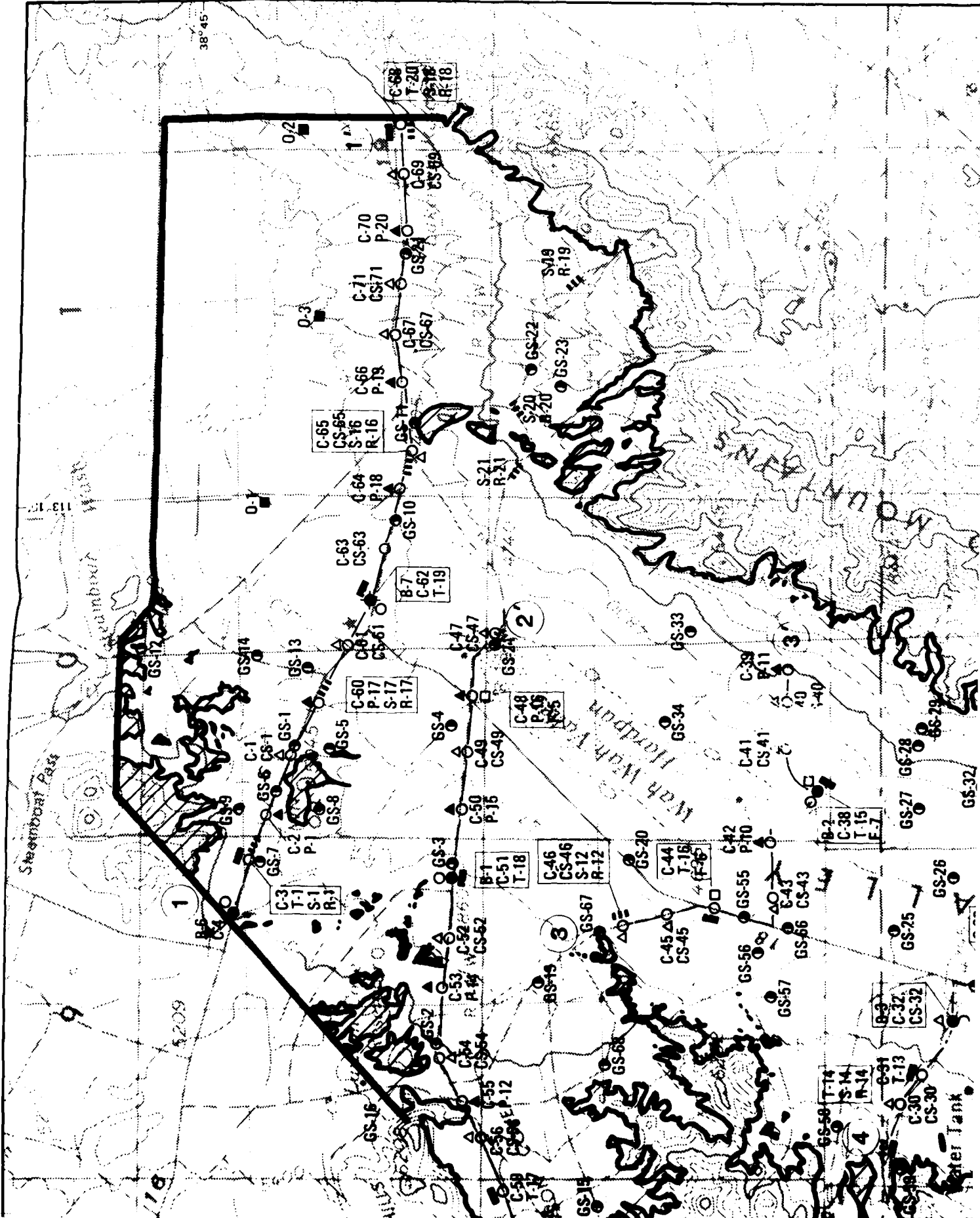


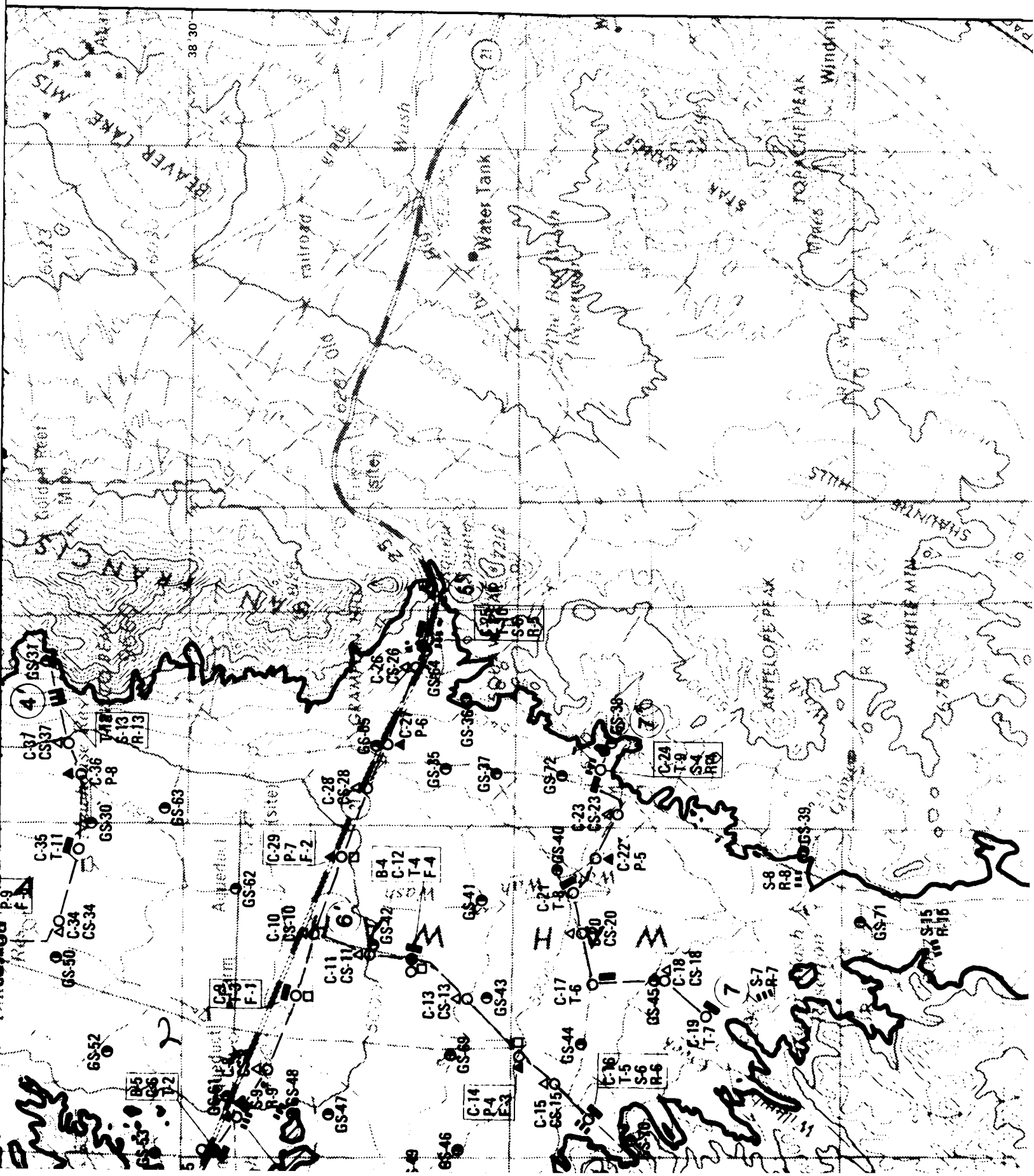
MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

The small areal extent of some of the surficial units resulted in only limited or insufficient data for analysis. The available data show that the drainages occurring in the lacustrine deposits (A4c) and younger-age alluvial fans (A5y) are deeper on the eastern side of Wah Wah Valley, while those occurring in the intermediate-age alluvial fans (A5i) are deeper on the west. Incision depths vary within a unit depending upon its grain size and degree of slope. All prevalent surficial units have a slightly greater number of drainages per mile on the western side of the valley.

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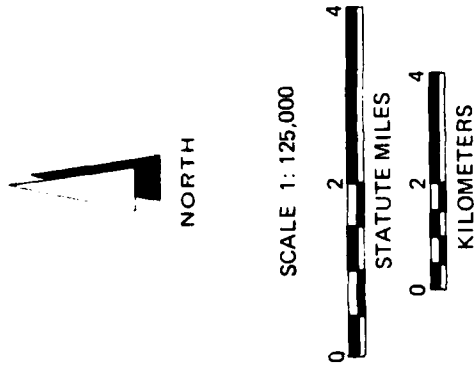


3

EXPLANATION

- GS-1 GEOLOGIC STATION
- B-1 BORING
- ◆ B-7 BORING AND OBSERVATIONAL WELL
- C-1 CONE PENETROMETER TEST (CPT)
- △ CS-1 SURFICIAL SOIL SAMPLE
- T-1 TRENCH
- ▲ P-1 TEST PIT
- ⋯ S-1 SEISMIC REFRACTION LINE
R-1 ELECTRICAL RESISTIVITY SOUNDING
- O-1 OBSERVATIONAL WELL
- F-1 FIELD CALIFORNIA BEARING RATIO (CBR) TEST
- ①—①' ACTIVITY LINE
- Contact between rock and basin fill.
- Valley borders.
- ▨ Area of isolated exposed rock.

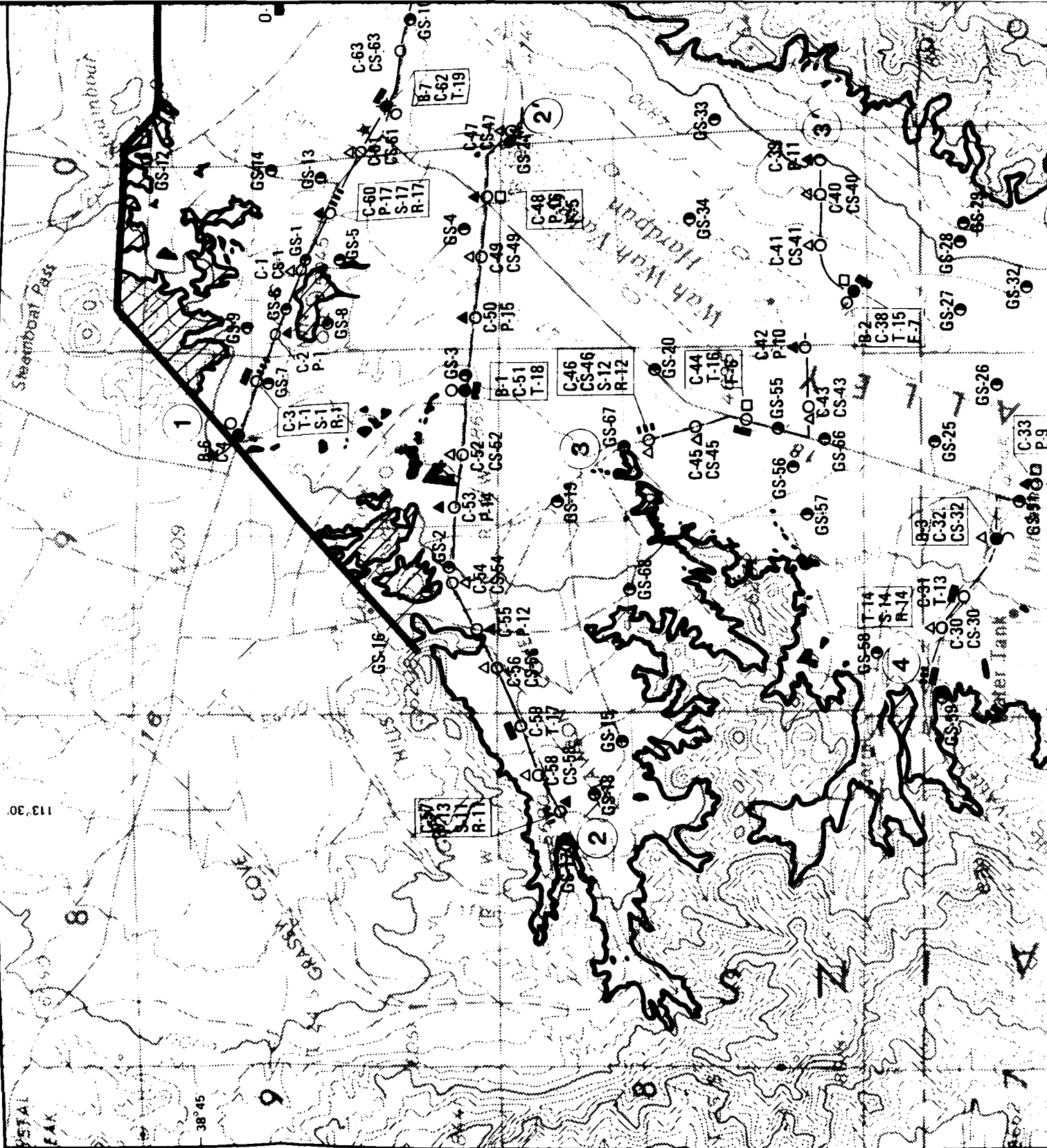
NOTE Where multiple activities were performed at the same location, the correct location is designated by either (1) the boring symbol or (2) CPT symbol, if no boring was drilled



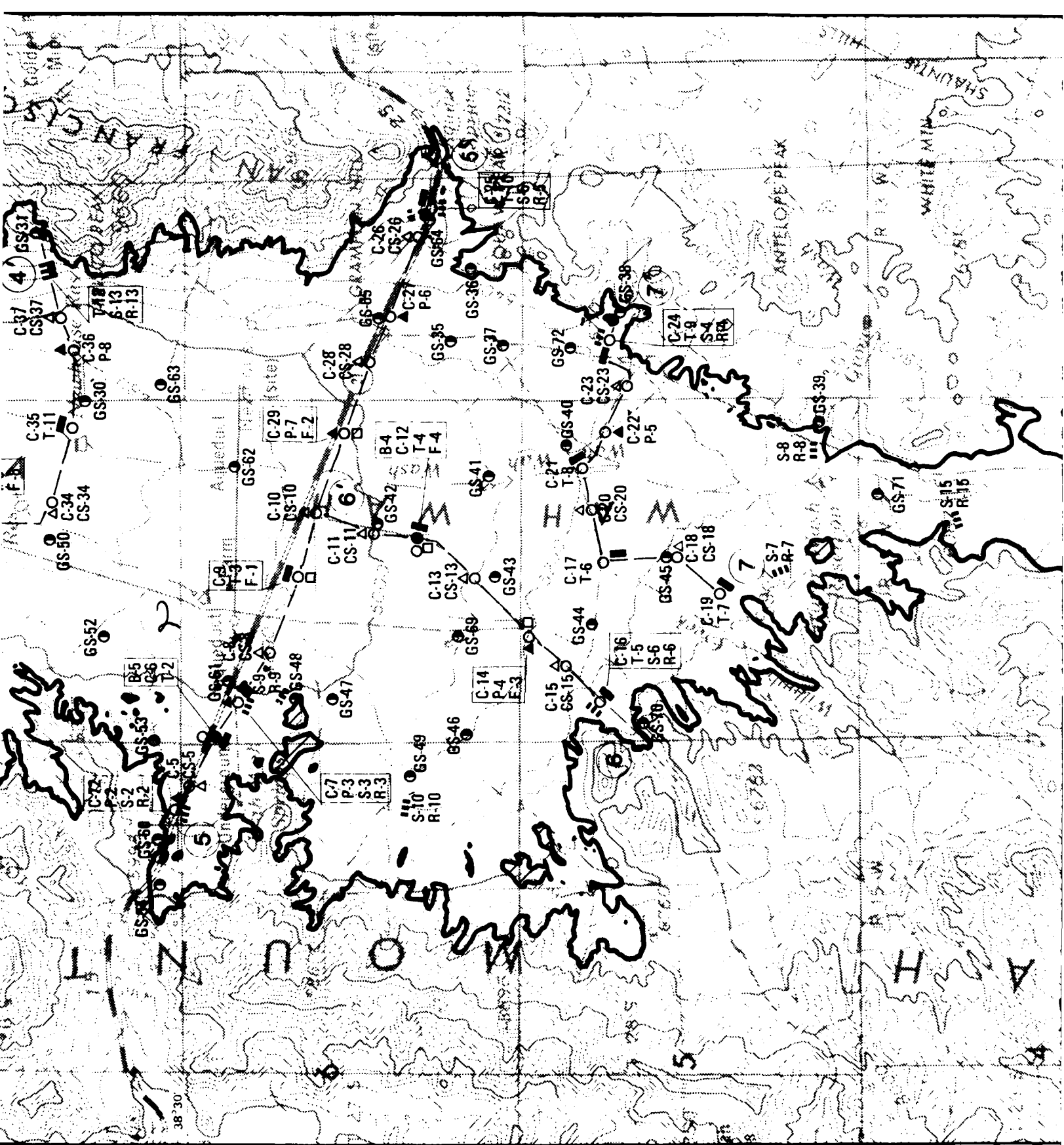
24 MAR 81

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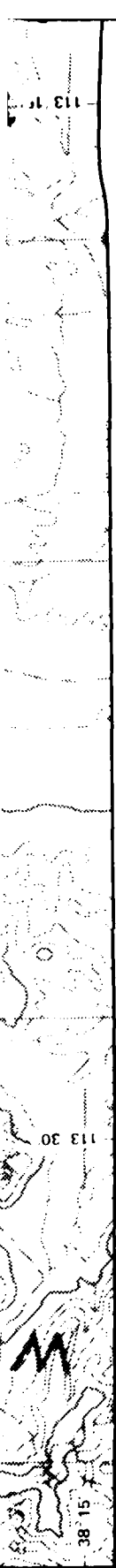
113°30'



4



5

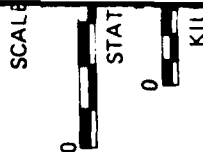


EXPLANATION

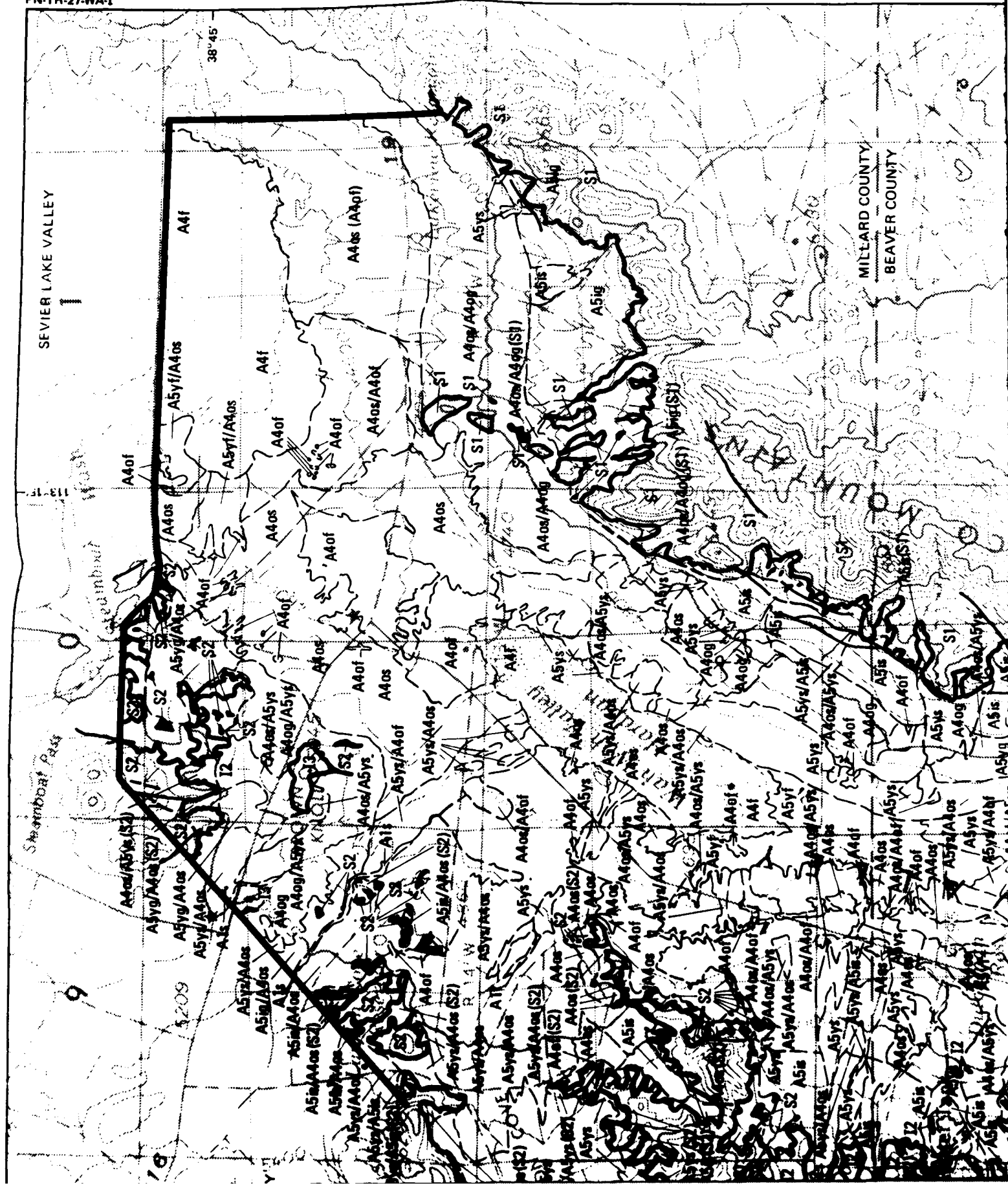
| | |
|------------|--|
| GS-1 | GEOLOGIC STATION |
| B-1 | BORING |
| B-7 | BORING AND OBSERVATIONAL WELL |
| C-1 | CONE PENETROMETER TEST (CPT) |
| CS-1 | SURFICIAL SOIL SAMPLE |
| T-1 | TRENCH |
| P-1 | TEST PIT |
| S-1 R-1 | SEISMIC REFRACTION LINE ELECTRICAL RESISTIVITY SOUNDING |
| O-1 | OBSERVATIONAL WELL |
| F-1 | FIELD CALIFORNIA BEARING RATIO (CBR) TEST |
| 1-1' | ACTIVITY LINE |
| | Contact between rock and basin fill. |
| | Valley borders. |
| | Area of isolated exposed rock. |

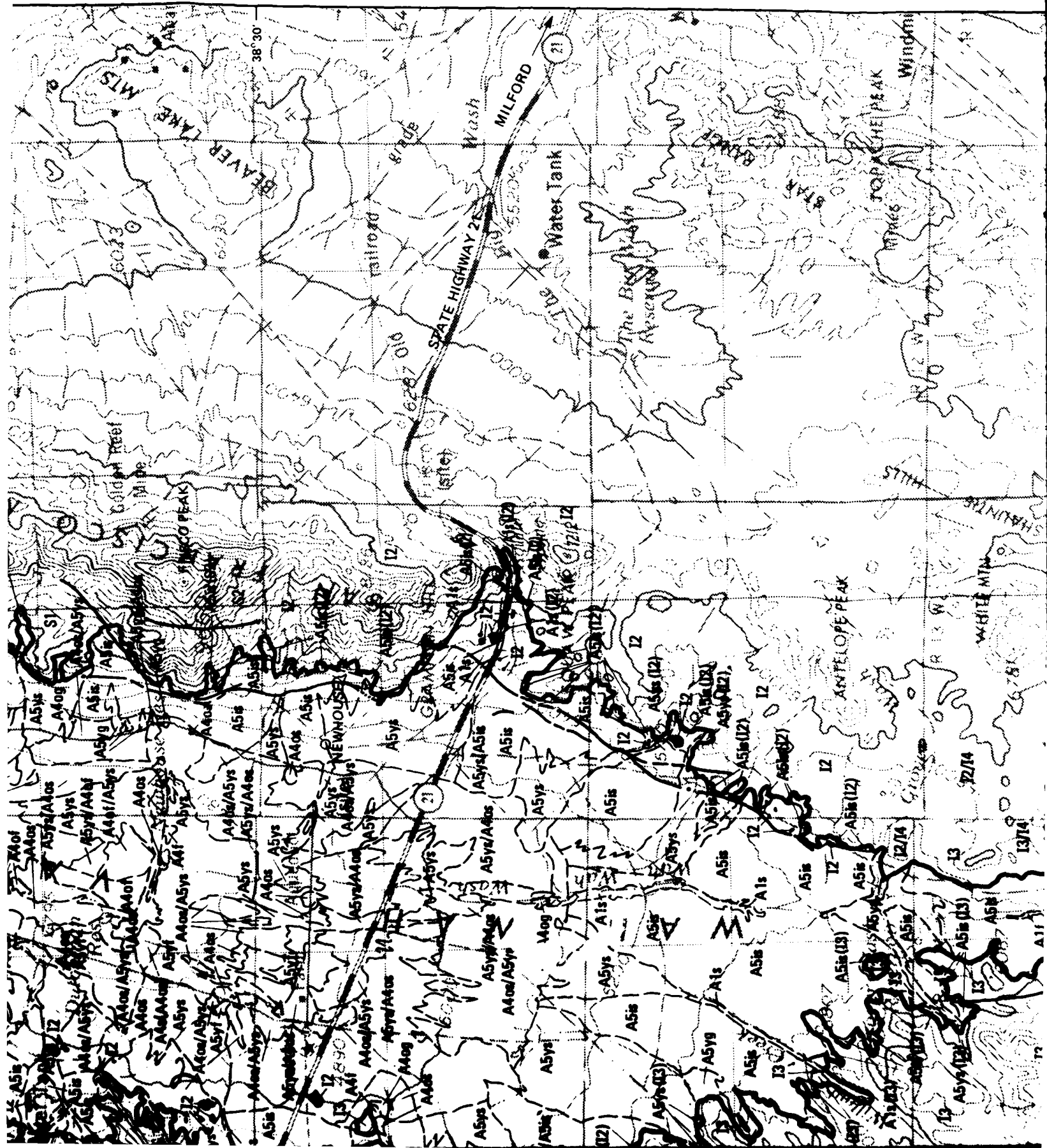
NOTE Where multiple activities were performed at the same location, the correct location is designated by either (1) the boring symbol or (2) CPT symbol, if no boring was drilled.

| | |
|--|----------------|
| ACTIVITY LOCATIONS WAH WAH VALLEY, UTAH | |
| MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - BMO | DRAWING 3-1 |
| FUGRO NATIONAL, INC. | |



4





A5 is (S2)

Igneous (I)

| |
|----|
| I2 |
| I3 |
| I4 |

Sedimentary (S)

| |
|----|
| S1 |
| S2 |
| S4 |

ROCK UNITS

Undifferentiated volcanic rocks consisting of rhyolite, latite, dacite and andesite.

Undifferentiated volcanic rocks consisting of basalts.

Undifferentiated volcanic rocks consisting of welded tuffs, ash flows, ignimbrites and tuffroclastics.



Sandstone.

Limestone and dolomite.

Gypsum.

SYMBOLS

Contact between rock and basin-fill.

Contact between surficial basin-fill or rock units.

Fault, trace of surface rupture, ball on downthrown side, dashed where approximately located in bedrock, dotted where inferred in alluvium.

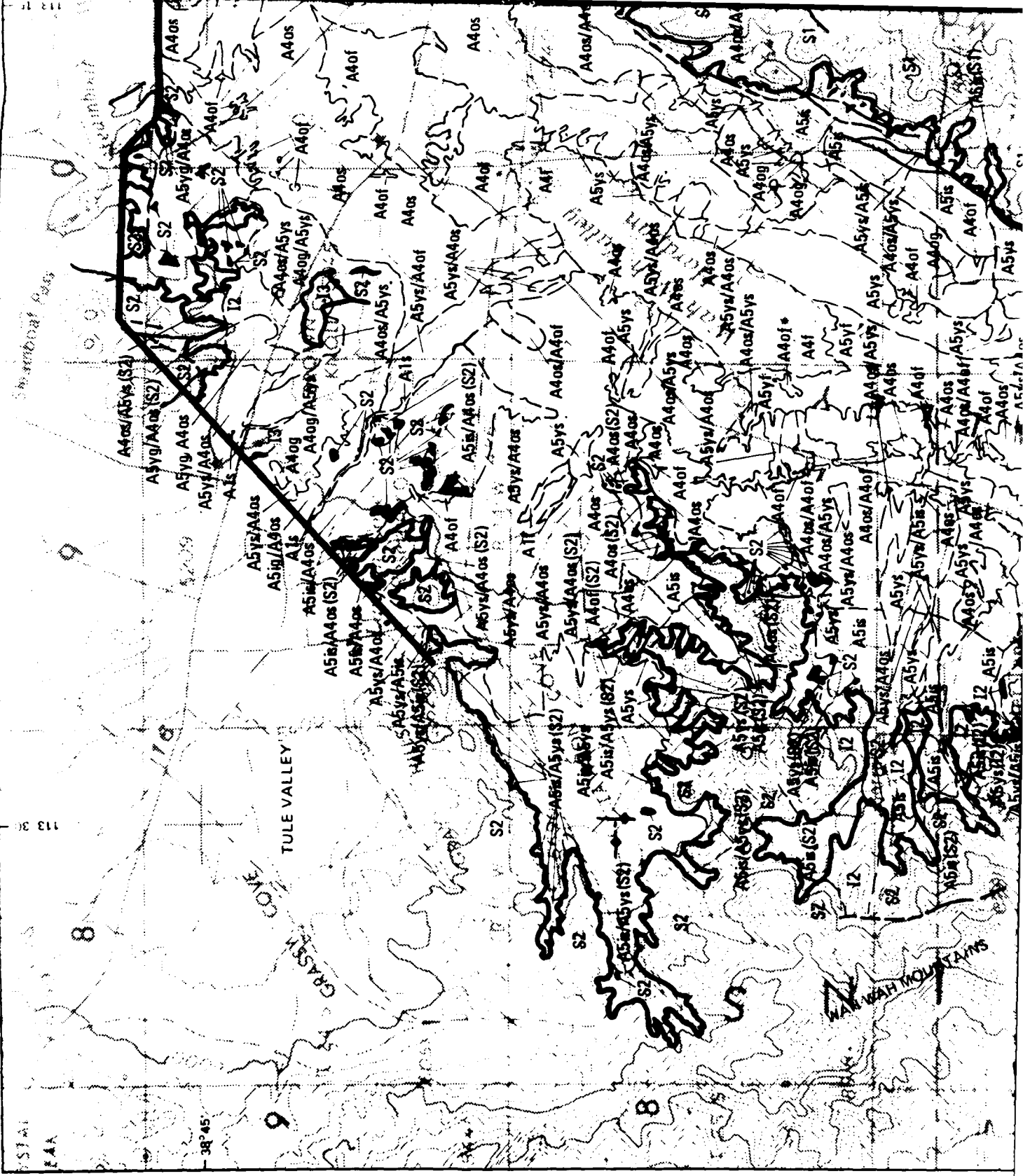
Tectonic lineament, probably a fault, generally expressed as a linear vegetational growth on aerial photographs.

Valley borders (north, south and west).

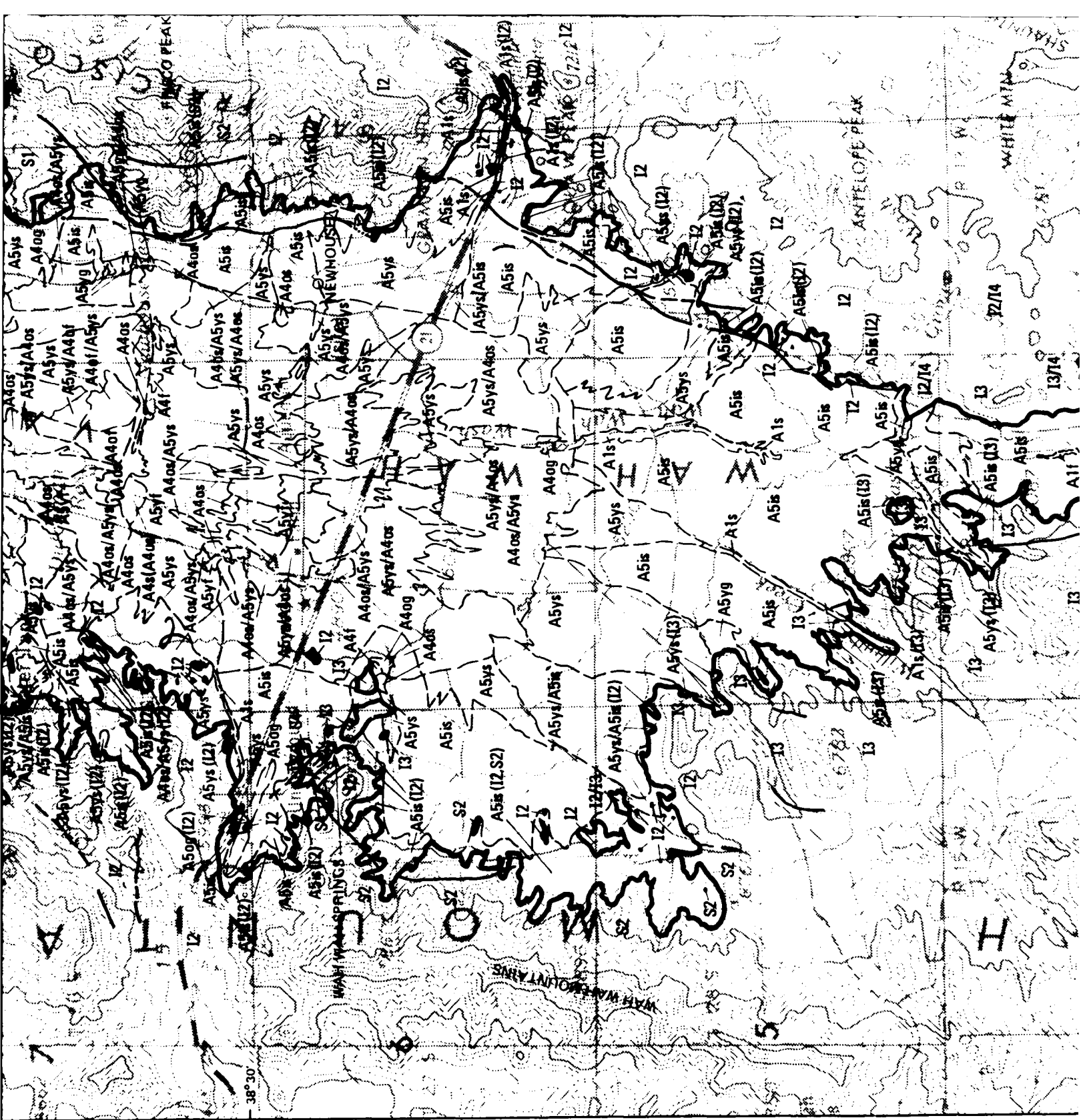
NOTES:

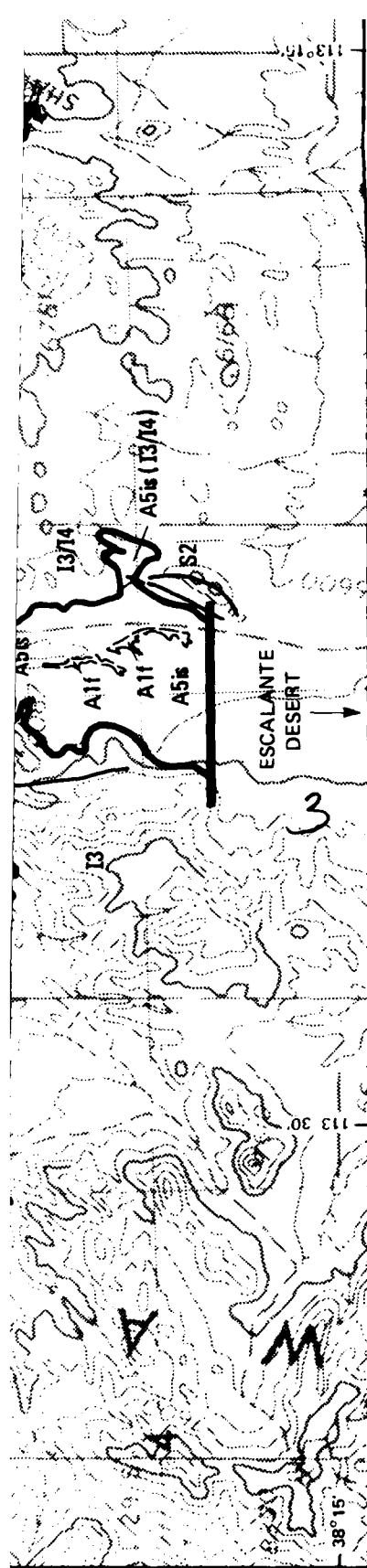
1. Surficial basin-fill units pertain only to the upper several feet of soil. Due to variability of surficial deposits and scale of map presentation, unit descriptions refer to the predominant soil types. Varying amounts of other soil types may be present within a geologic unit.
2. The distribution of geologic data stations is presented in Volume II Drawing II-1. A tabulation of all station data and generalized description of all geologic units is included in Volume II Section I.
3. Geology in areas of exposed rock from: Fugro National Inc. (1979, 1980) unpublished data. Thorman and Kerner (1979), and Stokes (1979).

18 MAR 81



5





EXPLANATION

SURFICIAL BASIN - FILL DEPOSITS

Young fluvial deposits in modern stream channels and on flood plains. A1f - sandy silts and clays
A1s - silty and gravelly sand.

Young lacustrine (lake) deposits occurring on active playas. A4f - silts and clays; A4s - silty sand.

Older lacustrine (lake) deposits. A4of - silts and clays associated with old playas; A4os - silty sand near shore beach sedimentation, A4og - sandy gravels in bars and shoreline features.

Young-age alluvial fans where deposition is now occurring. A5yf - sandy silts and clays; A5ys - silty sand; A5yg - sandy gravels.

Alluvial fans of intermediate-age. A5is - silty and gravelly sands; A5ig - sandy gravels.

Old-age alluvial fans having deep incisions and rounded erosional surfaces. A5og - sandy gravels.

Unit designation for areas where two types of deposits are inseparable at map scale. The predominant unit is indicated by the first letter.

A1f
A1s

A4f
A4s

A4of
A4os
A4og

A5yf
A5ys
A5yg

A5is
A5ig

A5og

A5is/A5ys

A5 is (S2)

Igneous (I)

| |
|----|
| I2 |
| I3 |
| I4 |

Sedimentary (S)

| |
|----|
| S1 |
| S2 |
| S4 |

ROCK UNITS

Undifferentiated volcanic rocks consisting of rhyolite, latite, dacite and andesite.

Undifferentiated volcanic rocks consisting of basalts.

Undifferentiated volcanic rocks consisting of welded tuffs, ash flows, ignimbrites and pyroclastics.

Sandstone.

Limestone and dolomite.

Gypsum.

SYMBOLS

Contact between rock and basin-fill.

Contact between surficial basin-fill or rock units.

Fault, trace of surface rupture, ball on downthrown side, dashed where approximately located in bed dotted where inferred in alluvium.

Tectonic lineament, probably a fault, generally expressed as a linear vegetational growth on aerial photo.

Valley borders (north, south and west).

NOTES:

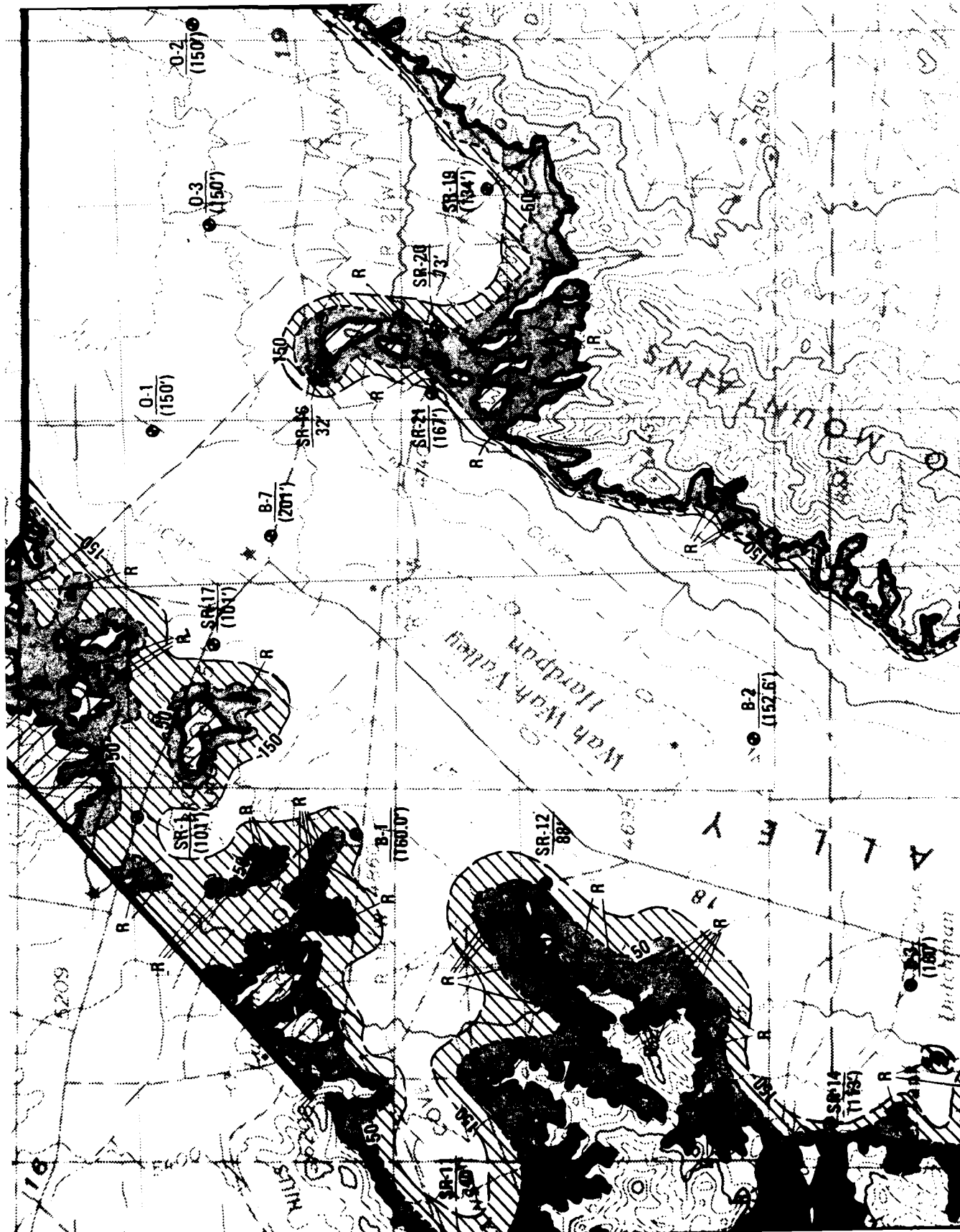
1. Surficial basin-fill units pertain only to the upper several feet of soil. Due to variability of surficial deposits and scale of map presentation, unit descriptions refer to the predominant soil types. Varying amount of other soil types may be present within a geologic unit.
2. The distribution of geologic data stations is presented in Volume II Drawing II-1. A tabulation of all station data and generalized description of all geologic units is included in Volume II Section I.
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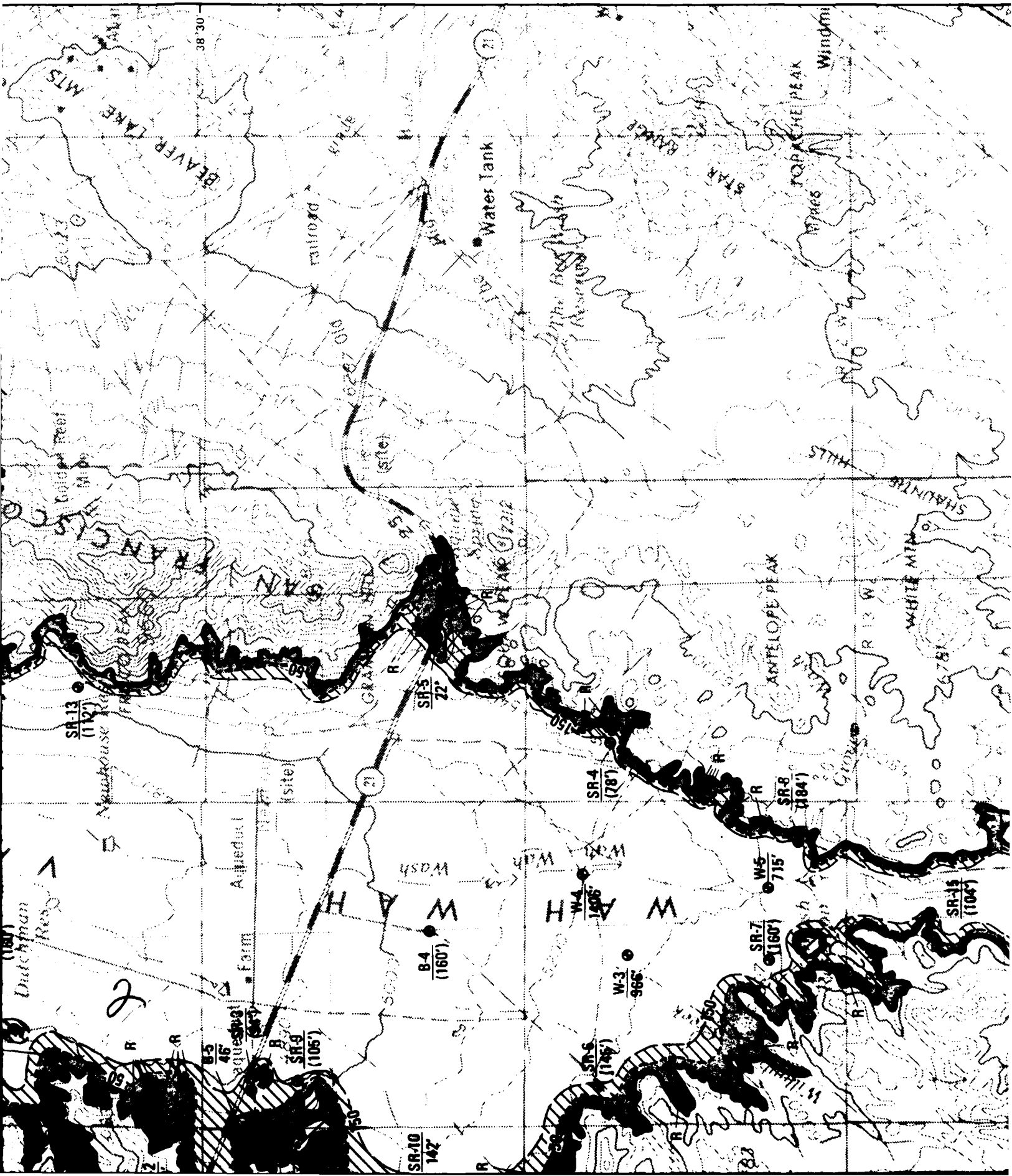
SURFICIAL GEOLOGICAL UNITS WAH WAH VALLEY, UTAH

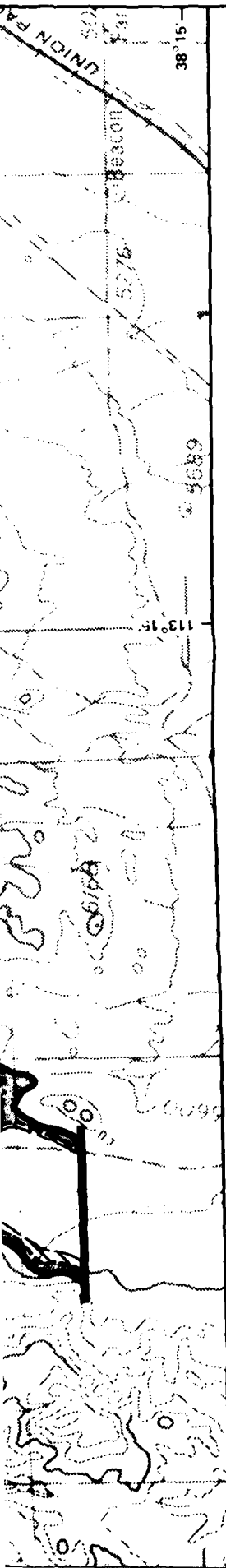
MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - BMO

DRAWING
3-2

FUGRO NATIONAL, INC.







3

EXPLANATION



Contour indicates rock at a depth of approximately 50 feet (15m) - shading indicates rock less than 50 feet (15m).



Contour indicates rock at a depth of approximately 150 feet (46m) - shading indicates rock between 50 feet (15m) and 150 feet (46m).



Contact between rock and basin-fill.



Valley borders.



Areas of isolated exposed rock.

R

Areas of isolated exposed rock too small for shading.

SR-9
● 123'

Data Source - Seismic refraction line and electrical resistivity sounding (SR); boring (B); published water well (W); and, observational test well (O); Volume II, Table 2-1.

Depth to rock or, when in parentheses, total depth at which rock not encountered.

NOTE The contours are based on geologic interpretations and the limited data points shown on the map. Some changes in contour locations can be expected as additional data are obtained.



NORTH

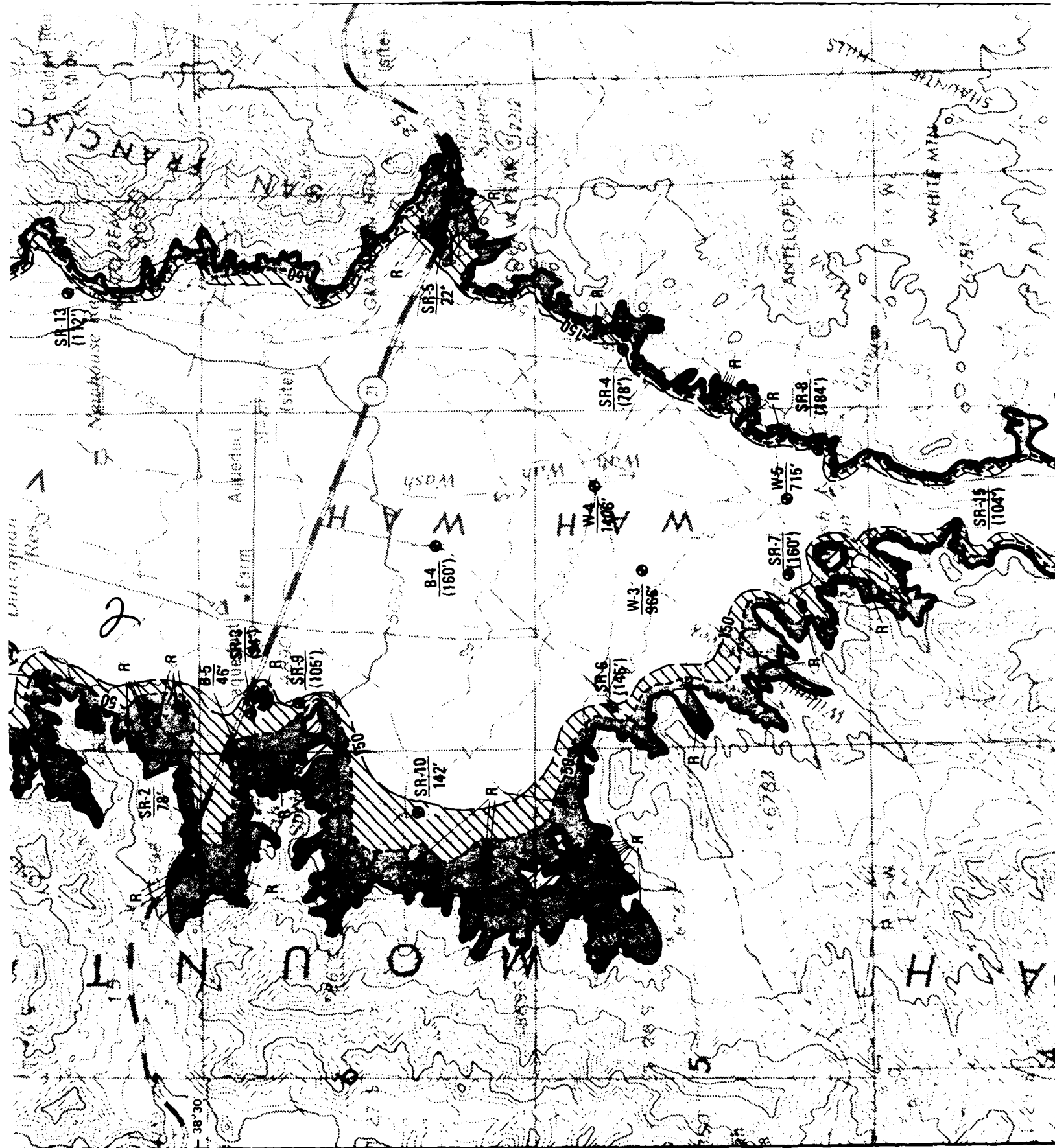
SCALE 1:125,000



STATUTE MILES











KILOMETERS



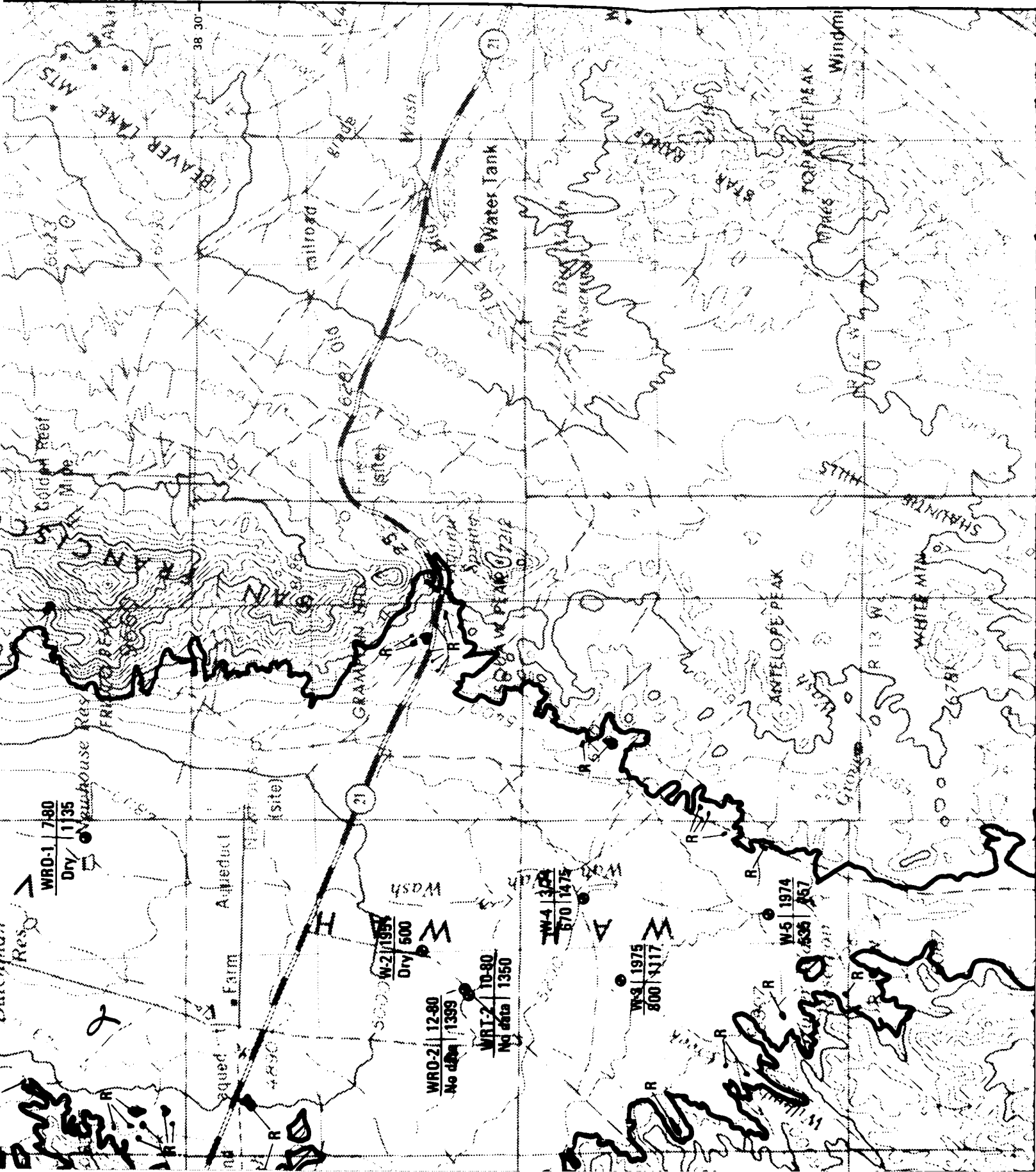


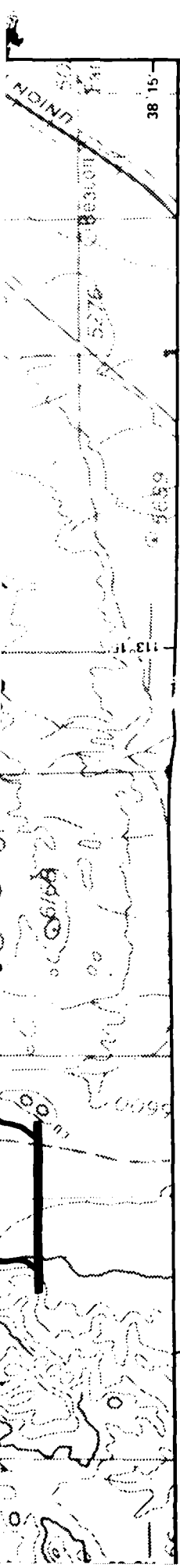
EXPLANATION

-  Contour indicates rock at a depth of approximately 50 feet (15m) - shading indicates rock less than 50 feet (15m).
-  Contour indicates rock at a depth of approximately 150 feet (46m) - shading indicates rock between 50 feet (15m) and 150 feet (46m).
-  Contact between rock and basin-fill.
-  Valley borders.
-  Areas of isolated exposed rock.
-  Areas of isolated exposed rock too small for shading.
-  Data Source - Seismic refraction line and electrical resistivity sounding (SR); boring (B); published water well (W); and, observational test well (O); Volume II, Table 2-1.
-  Depth to rock or, when in parentheses, total depth at which rock not encountered.

NOTE The contours are based on geologic interpretations and the limited data points shown on the map. Some changes in contour locations can be expected as additional data are obtained.

| | |
|--|----------------|
| DEPTH TO ROCK WAH WAH VALLEY, UTAH | |
| MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - BMO | DRAWING 3-3 |
| FUGRO NATIONAL, INC. | |





EXPLANATION



Contour indicates ground water at a depth of approximately 50 feet (15m) - shading indicates less than 50 feet (15m) to ground water.



Contour indicates ground water at a depth of approximately 150 feet (46m) - hachuring indicates between 50 feet (15m) and 150 feet (46m) to ground water.

Absence of contours indicates ground water occurs at depths greater than 150 feet. Fugro National, Inc. borings, and assorted wells indicate depths to ground water generally in excess of 400 feet throughout most of Wah Wah Valley (see Volume I, Section 3.0).

Contact between rock and basin-fill.



Valley borders.



Areas of isolated exposed rock.



R Areas of isolated exposed rock too small for shading.

Data Source - Water resources test well or observational well (WRT or WRO); published water well (W); boring and observational well (B(O)); or observational well (O); see Volume II, Table 2.1.

W-3 | 11-79
340 | 394

Month-Year of water level measurement, or year when month unknown.

Depth to water (feet).

Depth of well (feet).

Spring, indicating direction of flow.



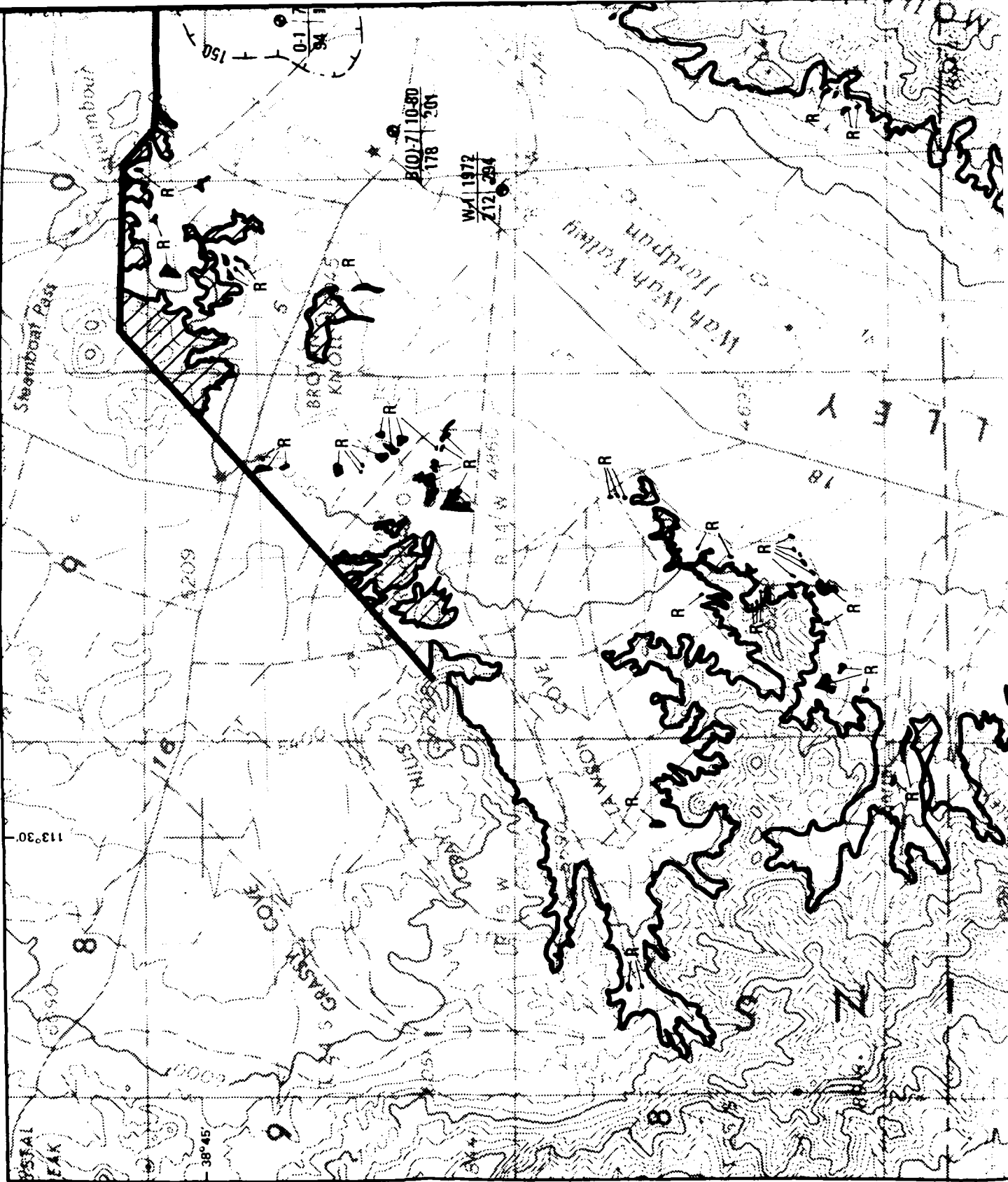
SCALE 1: 125,000



STATUTE MILES

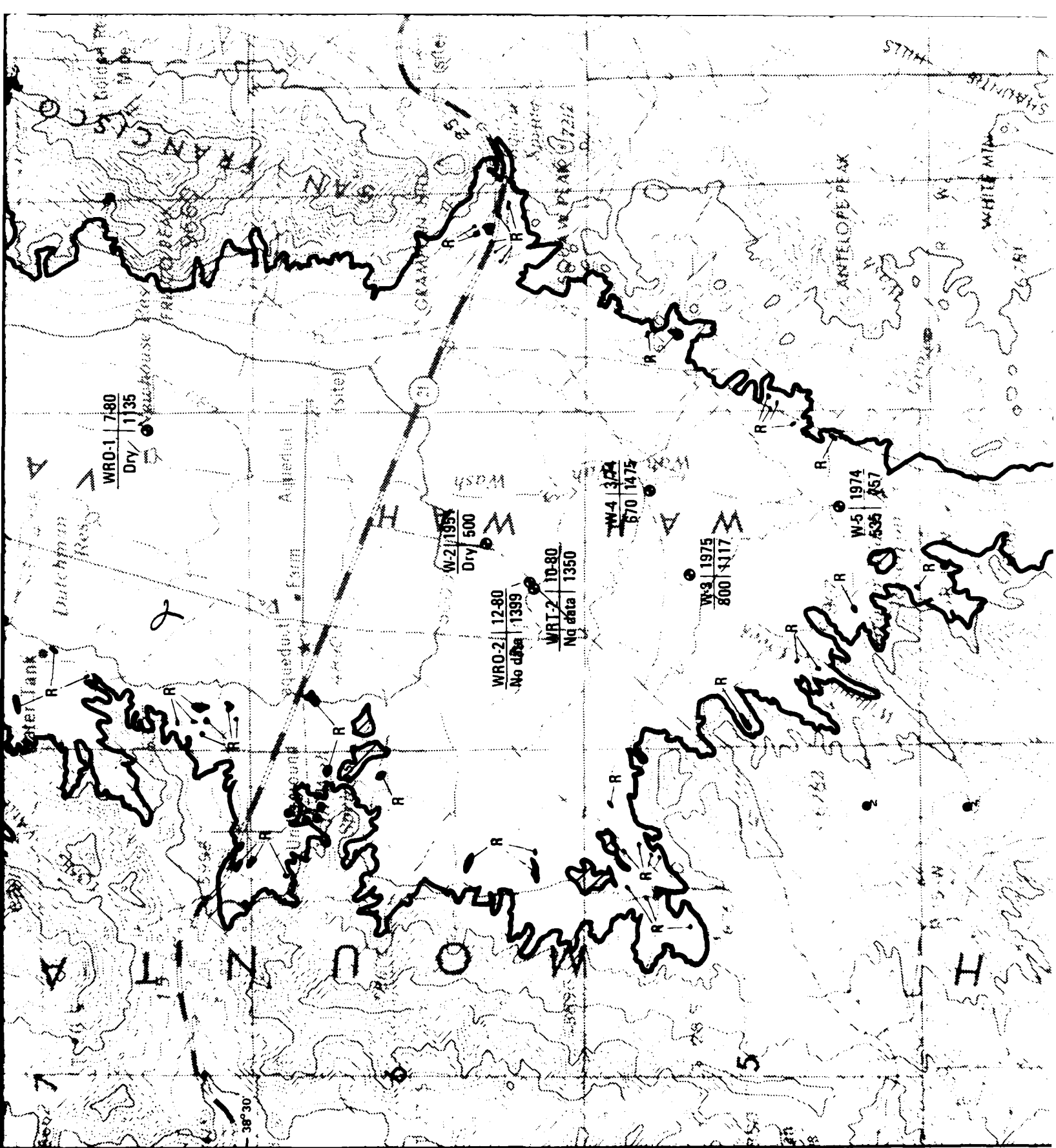


KILOMETERS



24 MAR 81

4



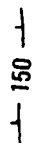
5



EXPLANATION



Contour indicates ground water at a depth of approximately 50 feet (15m) - shading indicates less than 50 feet (15m) to ground water.



Contour indicates ground water at a depth of approximately 150 feet (46m) - hachuring indicates between 50 feet (15m) and 150 feet (46m) to ground water.

Absence of contours indicates ground water occurs at depths greater than 150 feet. Fugro National, Inc. borings, and assorted wells indicate depths to ground water generally in excess of 400 feet throughout most of Wah Wah Valley (see Volume I, Section 3.0).



Contact between rock and basin-fill.



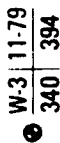
Valley borders.



Areas of isolated exposed rock.

R

Areas of isolated exposed rock too small for shading.



Data Source - Water resources test well or observational well (WRT or WRO), published water well (W), boring and observational well (B(O)); or observational well (O); see Volume II, Table 2-1.

Depth to water (feet).



Spring, indicating direction of flow.

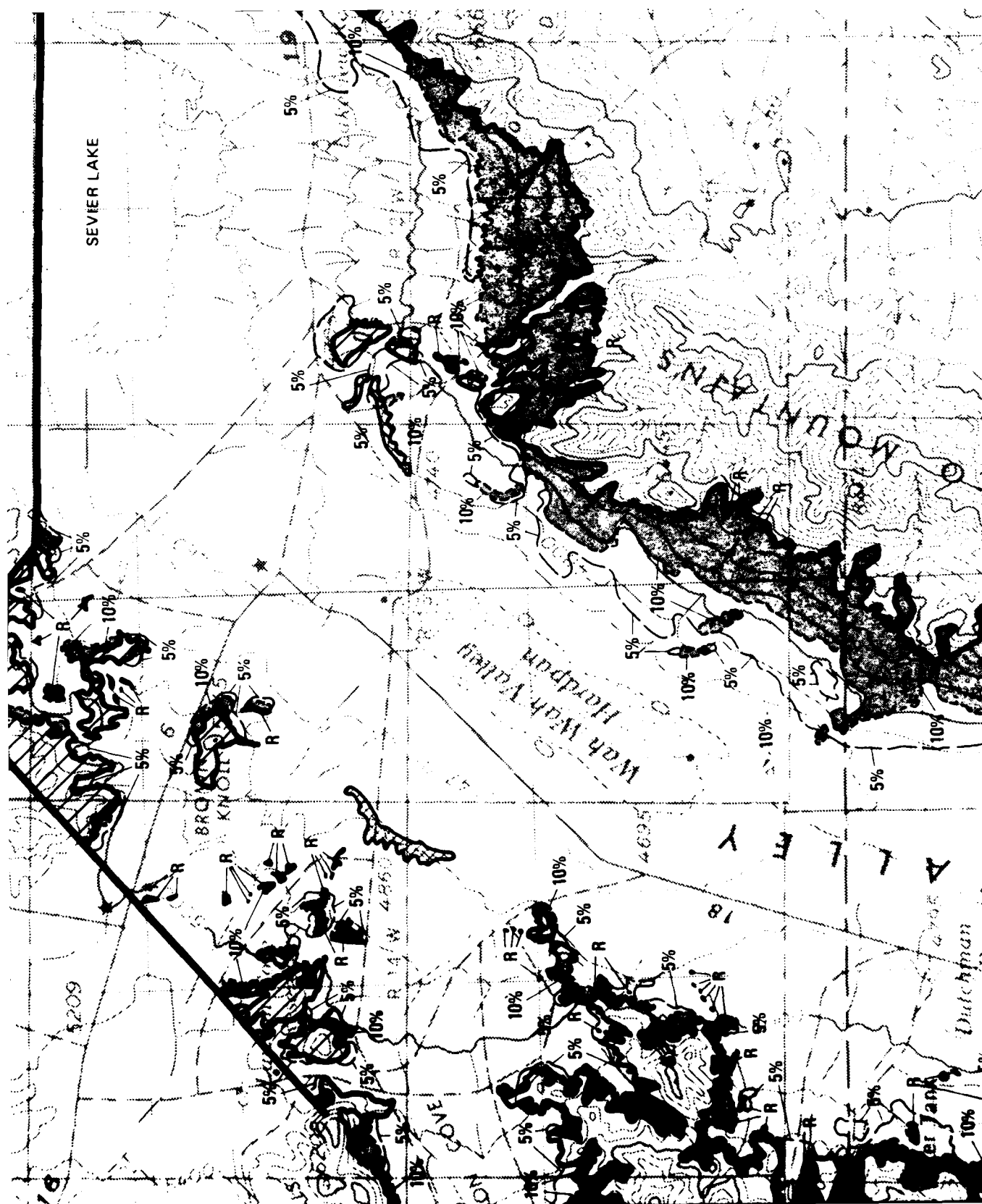
Depth of well (feet).

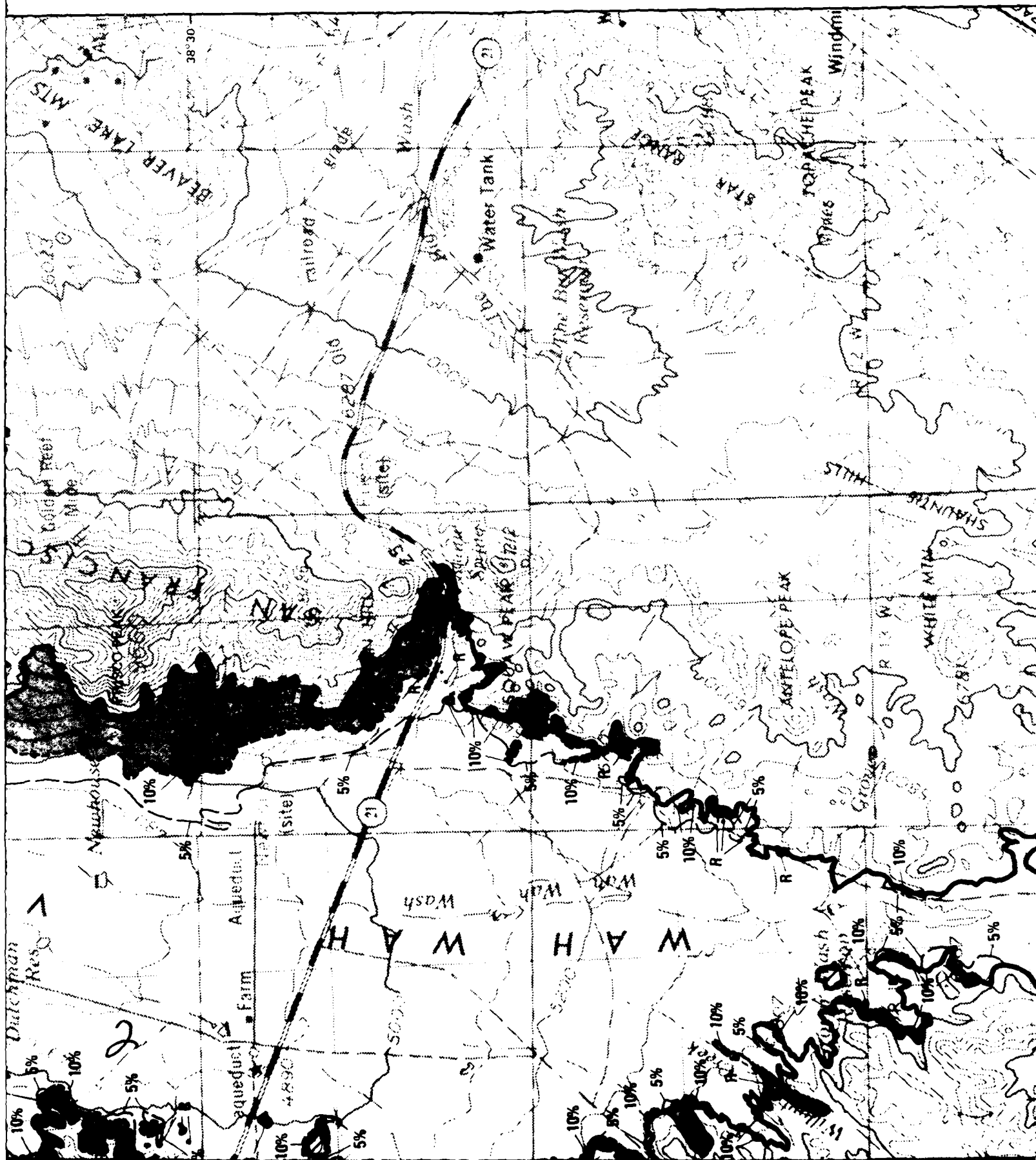
DEPTH TO WATER
WAH WAH VALLEY, UTAH

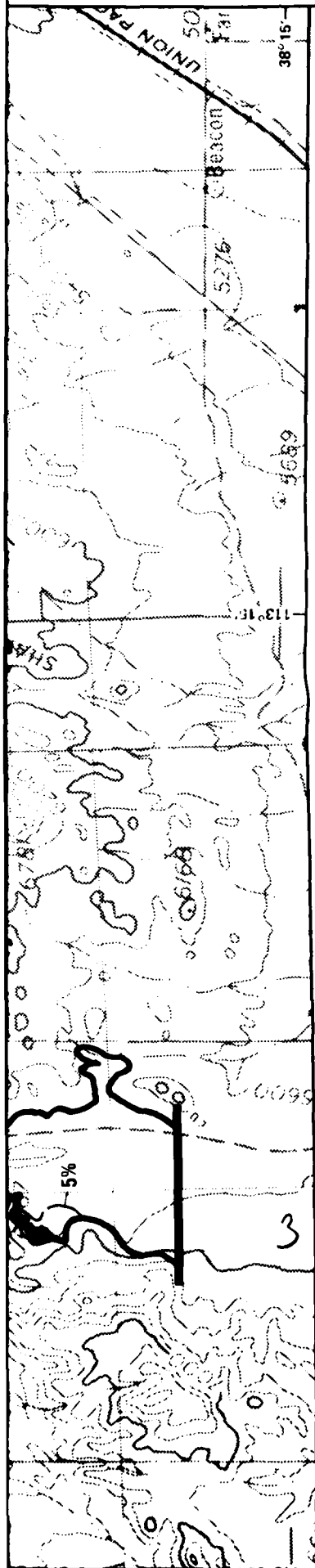
MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - BMO

DRAWING
3-4

FUGRO NATIONAL, INC.







EXPLANATION

— Contact between rock and basin fill.

- - - 5% Slope line.

- - - 10% Slope line.

— Valley borders.

Area excluded on basis of 10% slopes.

Terrain exclusion area.

Areas of isolated exposed rock.

R Areas of isolated exposed rock too small for shading.



NORTH

SCALE 1:125,000

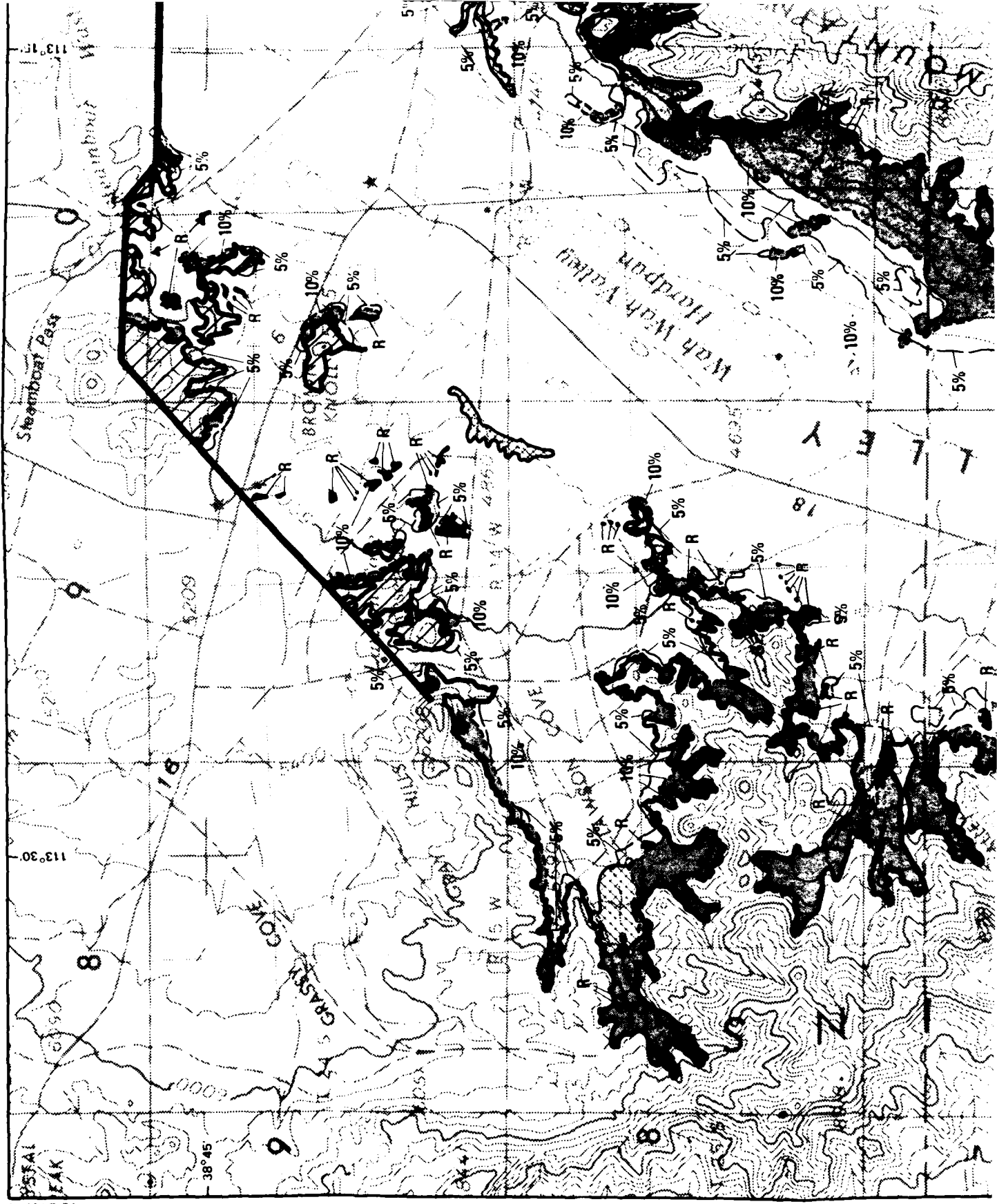


STATUTE MILES



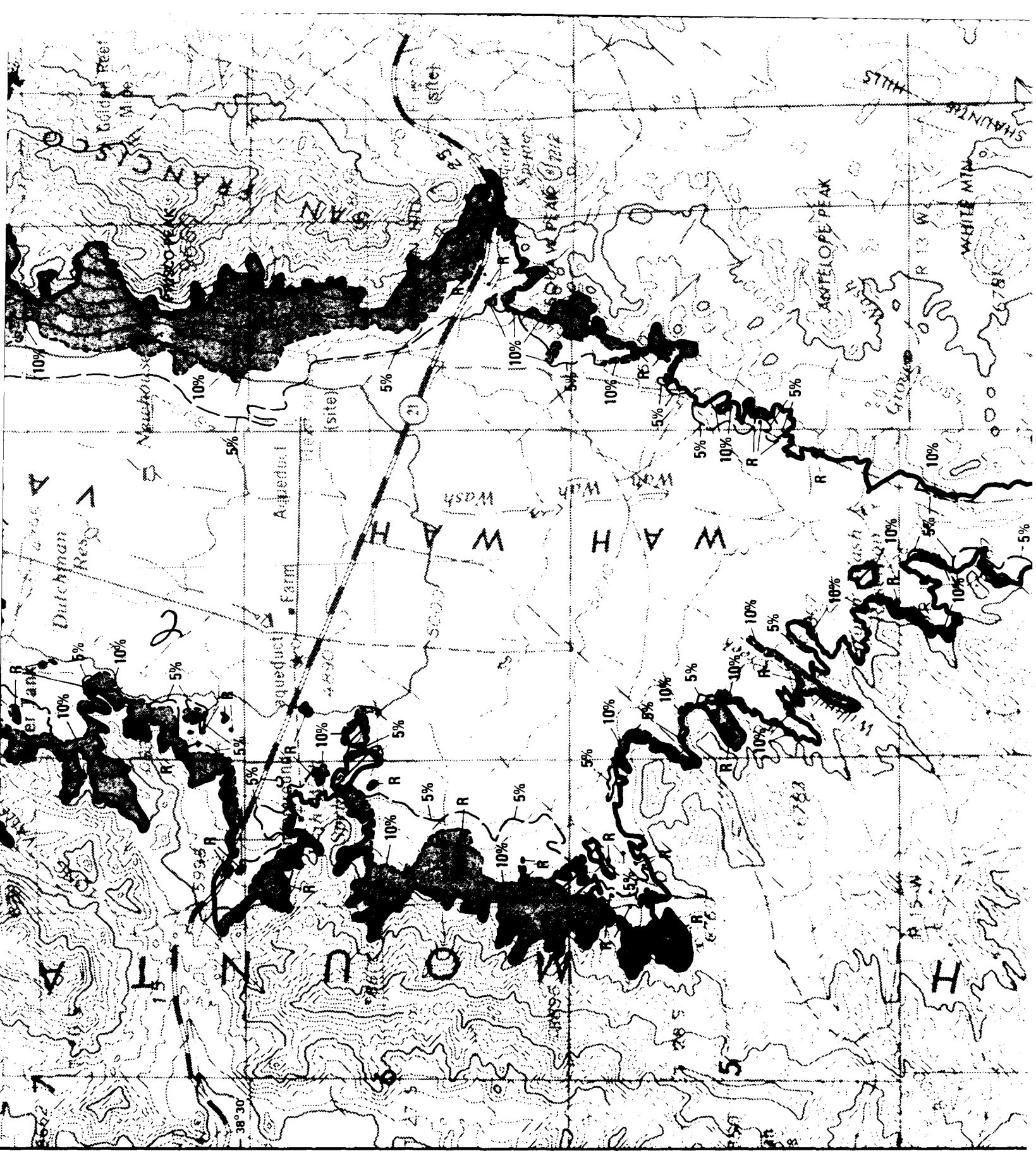
KILOMETERS

NOTE: Data used in constructing this map are from: (1) field observations, (2) 1:62,500 USGS topographic maps, and (3) 1:60,000 and 1:25,000 aerial photographs. Due to scale of presentation and variability of terrain conditions, this map is generalized.

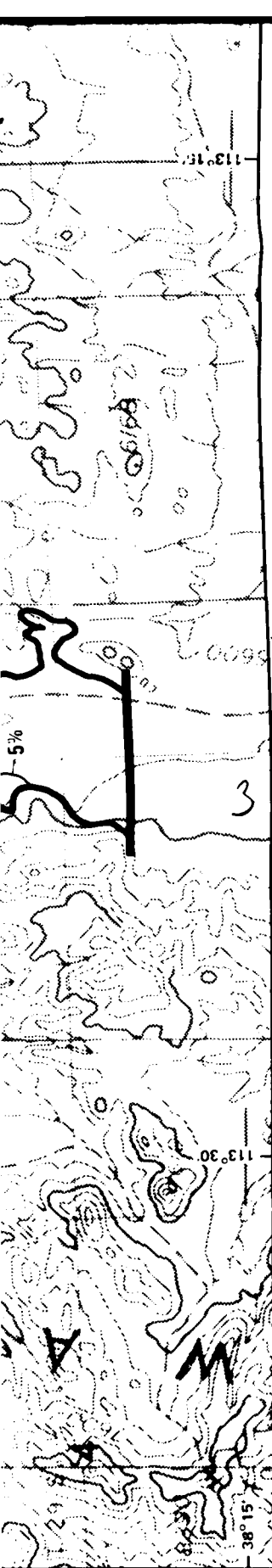


24 MAR 81

4



5



EXPLANATION

— Contact between rock and basin fill.

- - - 5% Slope line.

- - - 10% Slope line.

— Valley borders.

Area excluded on basis of 10% slopes.

Terrain exclusion area.

Areas of isolated exposed rock.

R Areas of isolated exposed rock too small for shading.

NOTE Data used in constructing this map are from: (1) field observations, (2) 1:62,500 USGS topographic maps, and (3) 1:60,000 and 1:25,000 aerial photographs. Due to scale of presentation and variability of terrain conditions, this map is generalized.

| | |
|--|----------------|
| TERRAIN WAH WAH VALLEY, UTAH | |
| MX SITING INVESTIGATION DEPARTMENT OF THE AIR FORCE - BMO | DRAWING 3-5 |
| FUGRO NATIONAL, INC. | |

A1.0 GLOSSARY OF TERMS

ACTIVE FAULT - A fault which has had surface displacement within Holocene time (about the last 11,000 years).

ACTIVITY NUMBER - A designation composed of the valley abbreviation followed by the activity type and a unique number; may also be used to designate a particular location in a valley.

ALLUVIAL FAN - A body of stream deposits whose surface approximates a segment of a cone that radiates downslope from the point where the stream leaves a mountainous area and experiences a marked change in gradient resulting in deposition of alluvium.

ALLUVIUM - A general term for a more-or-less stratified deposit of gravel, sand, silt, clay, or other debris, moved by streams from higher to lower ground.

AQUIFER - A permeable saturated zone below the earth's surface capable of conducting and yielding water as to a well.

ARRIVAL - An event; the appearance of seismic energy on a seismic record; a lineup of coherent energy signifying the arrival of a new wave train.

ATTERBERG LIMITS - A general term applied to the various tests used to determine the various states of consistency of fine-grained soils. The four states of consistency are solid, semisolid, plastic, and liquid.

Liquid limit (LL) - The water content corresponding to the arbitrary limit between the liquid and plastic states of consistency of a soil (ASTM D 423-66).

Plastic limit (PL) - The water content corresponding to an arbitrary limit between the plastic and the semisolid states of consistency of a soil (ASTM D 424-59).

Plasticity index (PI) - Numerical difference between the liquid limit and the plastic limit indicating the range of moisture content through which a soil-water mixture is plastic.

BASIN-FILL MATERIAL/BASIN-FILL DEPOSITS - Heterogeneous detrital material deposited in a sedimentary basin.

BASE LEVEL - The theoretical limit or lowest level toward which erosion constantly progresses; the level at which neither erosion or deposition takes place.

BEDROCK - A general term for the rock, usually solid, that underlies soil or other unconsolidated, surficial material. The term is also used here to include the rock composing the local mountain ranges.

BORING - A hole drilled in the ground for the purpose of subsurface exploration.

BOUGUER ANOMALY - The residual value obtained after latitude, elevation, and terrain corrections have been applied to gravity data.

BOULDER - A rock fragment, usually rounded by weathering and abrasion with an average diameter of 12 inches (305 mm) or more.

BULK SAMPLE - A disturbed soil sample (bag sample) obtained from cuttings brought to the ground surface by a drill rig auger or obtained from the walls of a trench excavation.

c - Cohesion (Shear strength of a soil not related to interparticle friction).

CALCAREOUS - Containing calcium carbonate; presence of calcium carbonate is commonly identified on the basis of reaction with dilute hydrochloric acid.

CALICHE - In general, secondary calcium-carbonate cementation of unconsolidated materials occurring in arid and semiarid areas.

CALIFORNIA BEARING RATIO (CBR) - The ratio (in percent) of the resistance to penetration developed by a subgrade soil to that developed by a specimen of standard crushed rock base material (ASTM D 1883-73). During the CBR test, the load is applied on the circular penetration piston (3 inches² base area [19 cm²]) which is penetrated into the soil sample at a constant penetration rate of 0.05 inch/minute (1.2 mm/min). The bearing ratio reported for the soil is normally the one at 0.1 inch (2.5 mm) penetration.

CLAST - An individual constituent, grain, or fragment of a sediment or rock, produced by the mechanical weathering (disintegration) of a larger rock mass.

CLAY - Fine-grained soil (passes No. 200 sieve [0.074 mm]) that can be made to exhibit plasticity within a range of water contents and that exhibits considerable strength when air-dried.

CLAY SIZE - That portion of the soil finer than 0.002 mm.

CLOSED BASIN - A catchment area draining to some depression or lake within its area from which water escapes only by evaporation or infiltration into the subsurface.

COARSE-GRAINED (or granular) - A term which applies to a soil of which more than one-half of the soil particles, by weight, are larger than 0.074 mm in diameter (No. 200 U.S. sieve size).

COARSER-GRAINED - A term applied to alluvial fan deposits which are predominantly composed of material (cobble) larger than 3 inches (76 mm) in diameter.

COBBLE - A rock fragment, larger than a pebble and smaller than a boulder, having a diameter between 3 and 10 inches (64 and 256 mm), being somewhat rounded or otherwise modified by abrasion in the course of transport.

COMPACTION TEST - A test to determine the relationship between the moisture content and density of a soil sample which is prepared in compacted layers at various water contents (ASTM D 1557-70).

COMPRESSIBILITY - Property of a soil pertaining to its susceptibility to decrease in volume when subjected to load.

COMPRESSIONAL WAVE - An elastic body wave in which particle motion is in the direction of propagation; the type of seismic wave assumed in conventional seismic exploration. Also called P-wave, dilatational wave, and longitudinal wave.

CONDUCTIVITY - The ability of a material to conduct electrical current. In isotropic material, conductivity is the reciprocal of resistivity. Units are mhos per meter.

CONE PENETROMETER TEST - A method of evaluating the in-situ engineering properties of soil by measuring the penetration resistance developed during the steady slow penetration of a cone (60° apex angle, 10-cm² projected area) into soil.

Cone resistance or end bearing resistance, q_c - The resistance to penetration developed by the cone, equal to the vertical force applied to the cone divided by its horizontally projected area.

Friction resistance, f_s - The resistance to penetration developed by the friction sleeve, equal to the vertical force applied to the sleeve divided by its surface area. This resistance consists of the sum of friction and adhesion.

Friction ratio, f_r - The ratio of friction resistance to cone resistance, f_s/q_c , expressed in percent.

CONSISTENCY - The relative ease with which a soil can be deformed.

CONSOLIDATION TEST - A type of test to determine the compressibility of a soil sample. The sample is enclosed in the consolidometer which is then placed in the loading device. The load is applied in increments at certain time intervals and the change in thickness is recorded.

CORE SAMPLE - A cylindrical sample obtained with a rotating core barrel with a cutting bit at its lower end. Core samples are obtained from indurated deposits and in rock.

DEGREE OF SATURATION - Ratio of volume of water in soil to total volume of voids.

DIRECT SHEAR TEST - A type of test to measure the shear strength of a soil sample where the sample is forced to fail on a predetermined plane.

DISSECTION/DISSECTED (alluvial fans) - The cutting of stream channels into the surface of an alluvial fan by the movement (or flow) of water.

DRY UNIT WEIGHT/DRY DENSITY - Weight per unit volume of the solid particles in a soil mass.

ELECTRICAL CONDUCTIVITY - Ability of a material to conduct electrical current.

ELECTRICAL RESISTIVITY - Property of a material which resists flow of electrical current.

EOLIAN - A term applied to materials which are deposited by wind.

EPHEMERAL (stream) - A stream or reach of a stream that flows briefly only in direct response to precipitation in the immediate locality and whose channel is at all times above the water table.

EXTERNAL DRAINAGE - Stream drainage system whose down-gradient flow is unrestricted by any topographic impediments.

EXTRUSIVE ROCK - Igneous rock that has been ejected onto the earth's surface (e.g., lava, basalt, rhyolite, andesite, detrital material, volcanic tuff, pumice).

FAULT - A plane or zone of fracture along which there has been displacement.

FAULT BLOCK MOUNTAINS - Mountains that are formed by normal faulting in which the surface crust is divided into partially to entirely fault-bounded blocks of different elevations.

- FINE-GRAINED** - A term which applies to a soil of which more than one-half of the soil particles, by weight, are smaller than 0.074 mm in diameter (passing the No. 200 U.S. size sieve).
- FINER-GRAINED** - A term applied to alluvial fan deposits which are composed predominantly of material less than 3 inches (76 mm).
- FLUVIAL DEPOSITS** - Material produced by river action; generally loose, moderately well-graded sands and gravel.
- FORMATION** - A mappable assemblage of rocks characterized by some degree of homogeneity or distinctiveness.
- FUGRO DRIVE SAMPLE** - A 2.50-inch- (6.4-cm) diameter soil sample obtained from a drill hole with a Fugro drive sampler. The Fugro drive sampler is a ring-lined barrel sampler containing 12 one-inch- (2.54-cm) long brass sample rings. The sampler is advanced into the soil using a drop hammer.
- GEOMORPHOLOGY** - The study, classification, description, nature, origin, and development of present landforms and their relationships to underlying structures and of the history of geologic changes as recorded by these surface features.
- GEOPHONE** - The instrument used to transform seismic energy into electrical voltage; a seismometer, jug, or pickup.
- GRABEN** - An elongated crustal block that has been downthrown along faults relative to the rocks on either side.
- GRAIN-SIZE ANALYSIS (GRADATION)** - A type of test to determine the distribution of soil particle sizes in a given soil sample. The distribution of particle sizes larger than 0.074 mm (retained on the No. 200 sieve) is determined by sieving, while the distribution of particle sizes smaller than 0.074 mm is determined by a sedimentation process using a hydrometer.
- GRANULAR** - See Coarse-Grained.
- GRAVEL** - Particles of rock that pass a 3-inch (76.2 mm) sieve and are retained on a No. 4 (4.75 mm sieve).
- GRAVITY** - The force of attraction between bodies because of their mass. Usually measured as the acceleration of gravity.
- GYPSIFEROUS** - Containing gypsum, a mineral consisting mostly of calcium sulfate.

HORST - An elongated crustal block that has been uplifted along faults relative to the rocks on either side.

INTERIOR DRAINAGE - Stream drainage system that flows into a closed topographic low (basin).

INTRUSIVE (rock) - A rock formed by the process of emplacement of magma (liquid rock) in preexisting rock (e.g., granite, granodiorite, quartz monzonite).

LACUSTRINE DEPOSITS - Materials deposited in a lake environment.

LINE - A linear array of observation points, such as a seismic line.

LINEAMENT - A linear topographic feature of regional extent that is thought to reflect crustal structure.

LIQUID LIMIT - See ATTERBERG LIMITS:

LOW STRENGTH SURFICIAL SOIL - Soil which will perform poorly as a road subgrade at its present consistency when used directly beneath a road section.

MOISTURE CONTENT - The ratio, expressed as a percentage, of the weight of water contained in a soil sample to the oven-dried weight of the sample.

N VALUE - Penetration resistance, described as the number of blows required to drive the standard split-spoon sampler for the second and third 6 inches (0.15 m) with a 140-pound (63.5-kg) hammer falling 30 inches (0.76 m) (ASTM D 1586-67).

OPTIMUM MOISTURE CONTENT - Moisture content at which a soil can be compacted to a maximum dry unit weight by a given compactive effort.

P-WAVE - See Compressional Wave.

PATINA (Desert Varnish) - A dark coating or thin outer layer produced on the surface of a rock or other material by weathering.

PAVEMENT/DESERT PAVEMENT - When loose material containing pebble-sized or larger rocks is exposed to rainfall and wind action, the finer dust and sand are blown or washed away and the pebbles gradually accumulate on the surface, forming a mosaic which protects the underlying finer material from wind attack. Pavement can also develop in finer-grained materials. In this case, the armored surface is formed by dissolution and cementation of the grains involved.

PERCHED GROUND WATER - Unconfined ground water separated from an underlying main body of ground water by an unsaturated zone.

PERMEABILITY - The property of soil and/or rock material which permits liquid to pass through.

pH - An index of the acidity or alkalinity of a soil in terms of the logarithm of the reciprocal of the hydrogen ion concentration.

PHI (ϕ) - Angle of internal friction.

PIEZOMETRIC SURFACE - An imaginary surface representing the static head of ground water and defined by the level to which water will rise in a well.

PITCHER TUBE SAMPLE - An undisturbed, 2.87-inch- (73-mm) diameter soil sample obtained from a drill hole with a Pitcher tube sampler. The primary components of this sampler are an outer rotating core barrel with a bit and an inner stationary, spring-loaded, thin-wall sampling tube which leads or trails the outer barrel drilling bit depending upon the hardness of the material being penetrated.

PLASTIC LIMIT - See ATTERBERG LIMITS.

PLASTICITY INDEX - See ATTERBERG LIMITS.

PLAYA/PLAYA DEPOSITS - A term used in the southwest U.S. for a dried-up, flat-floored area composed of thin, evenly stratified sheets of clay, silt, or fine sand, and representing the lowest part of a shallow, completely closed or undrained, desert lake basin in which water accumulates and is quickly evaporated, usually leaving deposits of soluble salts.

POORLY GRADED - A descriptive term applied to a coarse-grained soil if it consists predominantly of one particle size (uniformly graded) or has a wide range of sizes with some intermediate sizes obviously missing (gap-graded).

RANGE-BOUNDING FAULT - Usually a normal fault in which one side has moved up relative to the other and which separates the mountain front from the valley.

RELATIVE AGE - The relationship in age (oldest to youngest) between geologic units without specific regard to number of years.

RESISTIVITY (True, Intrinsic) - The property of a material which resists the flow of electric current. The ratio of electric-field intensity to current density.

ROCK UNITS - Distinct rock masses with different characteristics (e.g., igneous, metamorphic, sedimentary).

ROTARY WASH DRILLING - A boring technique in which advancement of the hole through overburden is accomplished by rotation of a heavy string of rods while continuous downward pressure is maintained through the rods on a bit at the bottom of the hole. Water or drilling mud is forced down the rods to the bit, and the return flow brings the cuttings to the surface.

S-WAVE - See Shear Wave.

SAND - Soil passing through No. 4 (4.75 mm) sieve and retained on No. 200 (0.075 mm) sieve.

SAND DUNE - A low ridge or hill consisting of loose sand deposited by the wind, found in various desert and coastal regions and generally where there is abundant surface sand.

SEISMIC - Having to do with elastic waves. Energy may be transmitted through the body of an elastic solid as P-waves (compressional waves) or S-waves (shear waves).

SEISMIC LINE - A linear array of travel time observation points (geophones). In this study, each line contains 24 geophone positions.

SEISMIC REFRACTION DATA - Data derived from a type of seismic shooting based on the measurement of seismic energy as a function of time after the shot and of distance from the shot, by determining the arrival times of seismic waves which have traveled nearly parallel to the bedding in high-velocity layers in order to map the depth to such layers.

SEISMOGRAM - A seismic record.

SEISMOMETER - See Geophone.

SHEAR STRENGTH - The maximum resistance of a soil to shearing (tangential) stresses.

SHEAR WAVE - A body wave in which the particle motion is perpendicular to the direction of propagation. Also called S-Wave or transverse wave.

SHEET FLOW - A process in which storm-born water spreads as a thin, continuous veneer (sheet) over a large area.

SHEET SAND - A blanket deposit of sand which accumulates in shallow depressions or against rock outcrops, but does not have characteristic dune form.

- SHOT - Any source of seismic energy; e.g., the detonation of an explosive.
- SHOT POINT - The location of any source of seismic energy; e.g., the location where an explosive charge is detonated in one hole or in a pattern of holes to generate seismic energy. Abbreviated SP.
- SILT - Fine-grained soil passing the No. 200 sieve (0.074 mm) that is nonplastic or very slightly plastic and that exhibits little or no strength when air-dried.
- SILT SIZE - That portion of the soil finer than 0.02 mm and coarser than 0.002 mm.
- SITE - Location of some specific activity or reference point.
- SPECIFIC GRAVITY - The ratio of the weight in air of a given volume of soil solids at a stated temperature to the weight in air of an equal volume of distilled water at a stated temperature.
- SPLIT-SPOON SAMPLE - A disturbed sample obtained with a split-spoon sampler with an outside diameter of 2.0 inches (5.1 cm). The sample consists of a split barrel which is driven into the soil using a drop hammer.
- SPREAD - The layout of geophone groups from which data from a single shot are recorded simultaneously. Spreads containing 24 geophones have been used in Fugro's seismic refraction surveys.
- STREAM CHANNEL DEPOSITS - See Fluvial Deposits.
- STREAM TERRACE DEPOSITS - Stream channel deposits no longer part of an active stream system, generally loose, moderately well graded sand and gravel.
- SULFATE ATTACK - The process during which sulfates, salts of sulfuric acid, contained in ground water cause dissolution and damage to concrete.
- SURFICIAL DEPOSIT - Unconsolidated residual colluvial and alluvial deposits occurring on or near the earth's surface.
- TEST PIT - An excavation made to depths of about 5 feet (1.5 m) by a backhoe. A test pit permits visual examination of undisturbed material in place.
- TRENCH - An excavation by a backhoe to depths of about 15 feet (4.5 m). A trench permits visual examination of soil in place and evaluation of excavation wall stability.

TRIAXIAL COMPRESSION TEST - A type of test to measure the shear strength of an undisturbed soil sample (ASTM D 2850-70). To conduct the test, a cylindrical specimen of soil is surrounded by a fluid in a pressure chamber and subjected to an isotropic pressure. An additional compressive load is then applied, directed along the axis of the specimen called the axial load.

Consolidated-drained (CD) Test - A triaxial compression test in which the soil was first consolidated under an all-around confining stress (test chamber pressure) and was then compressed (and hence sheared) by increasing the vertical stress. Drained indicates that excess pore water pressures generated by strains are permitted to dissipate by the free movement of pore water during consolidation and compression.

Consolidated-undrained (CU) Test - A triaxial compression test in which essentially complete consolidation under the confining (chamber) pressure is followed by a shear at constant water content.

UNCONFINED COMPRESSION - A type of test to measure the compressive strength of an undisturbed sample (ASTM D 2166-66). Unconfined compressive strength is defined as the load per unit area at which an unconfined prismatic or cylindrical specimen of soil will fail in a simple compression test.

UNIFIED SOIL CLASSIFICATION SYSTEM (USCS) - A system which determines soil classification for engineering purposes on the basis of grain-size distribution and Atterberg limits.

VALLEY FILL - See Basin-Fill Material/Basin-Fill Deposits.

VELOCITY - Refers to the propagation rate of a seismic wave without implying any direction. Velocity is a property of the medium and not a vector quantity when used in this sense.

VELOCITY LAYER - A layer of rock or soil with a homogeneous seismic velocity.

VELOCITY PROFILE - A cross section showing the distribution of material seismic velocities as a function of depth.

WASH SAMPLE - A sample obtained by screening the returned drilling fluid during rotary wash drilling.

WATER TABLE - The upper surface of an unconfined body of water at which the pressure is equal to the atmospheric pressure.

WELL-GRADED - A soil is identified as well-graded if it has a wide range in grain size and substantial amounts of most intermediate sizes.

Definitions were derived from the following references:

American Society for Testing and Materials, 1976, Annual book of ASTM standards, Part 19: Philadelphia, American Soc. for Testing and Materials, 484 p.

Fairbridge, Rhodes W., ed., 1968, The encyclopedia of geomorphology: Stroudsburg, Pennsylvania, Dowden, Hutchinson, and Ross, Inc., 1295 p.

Gary, M., McAfee, R., Jr., Wolf, C. L., eds., 1972, Glossary of geology: Washington, D.C., American Geological Institute, 805 p.

Merriam, G., and Merriam, C., 1977, Webster's new collegiate dictionary: Springfield, Mass., G. and C. Merriam Co., 1536 p.

Sheriff, R. E., 1973, Encyclopedic dictionary of exploration geophysics: Tulsa, Oklahoma, Society of Exploration Geophysicists, 266 p.

A2.0 EXCLUSION CRITERIA

The exclusion criteria used during the Verification Studies are based on both geotechnical and cultural considerations. Land excluded for geotechnical reasons includes areas of shallow rock, shallow water, and adverse terrain. Cultural exclusions include areas near towns, lands already withdrawn from public use, and regions with potentially high economic value. The exclusion criteria are defined in Table A2-1.

FN-TR-27-WA-I

| <u>CRITERIA</u> | | <u>DEFINITION AND COMMENTS</u> |
|--|---------------|---|
| SURFACE ROCK AND ROCK OCCURRING WITHIN 50 FEET (15m) AND 150 FEET (46m) OF THE GROUND SURFACE | | Rock is defined as any earth material which is not rippable by conventional excavation methods. Where available, seismic P-wave velocities were evaluated in the determination of rock conditions. |
| SURFACE WATER AND GROUND WATER OCCURRING WITHIN 50 FEET (15m) AND 150 FEET (46m) OF THE GROUND SURFACE | | Surface water includes all significant lakes, reservoirs, swamps, and major perennial streams. Water which would be encountered in a 50-foot and 150-foot excavation was considered in the application of this criterion. Depths to ground water resulting from deeper confined aquifers were not considered. |
| TERRAIN | Percent Grade | Areas having surface gradients exceeding 10 percent or a preponderance of slopes exceeding 10 percent as determined from maps at scales of 1:125,000, 1:62,500, and 1:24,000 and by field observation. |
| | Drainage | Areas averaging two or more 10-foot deep drainages per 1000 feet (measured parallel to contours, as determined from maps at scales of 1:24,000 or in the field). |
| CULTURAL | Land use: | All significant federal and state forests, parks, monuments, and recreational areas. |
| | | All significant federal and wildlife refuges, grasslands, ranges, preserves and management areas. |
| | | Indian reservations. |

EXCLUSION CRITERIA
VERIFICATION STUDIES, NEVADA-UTAH

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE - SMO

TABLE
A2-1

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A3.0 ENGINEERING GEOLOGIC PROCEDURES

The principal objectives of the field geology investigation were to:

1. Delineate surficial extent of soil types and geologic units;
2. Assess terrain conditions; and
3. Make observations helpful in defining depth to rock and water.

Aerial photographs (1:60,000 scale black and white; 1:25,000 scale color) served as the base on which all mapping was done. Field activities were directed toward checking the photogeologic mapping.

Field checking consisted chiefly of collecting data about surficial soils at selected locations in order to refine contacts and define engineering characteristics of photogeologic units. At each location, observations of grain-size distribution, color, clast lithology, surface soil development, and a variety of engineering parameters were recorded (see Volume II, Geotechnical Data). Observations were made in existing excavations (borrow pits, road cuts, stream cuts) or in hand-dug test pits. Extrapolation of this data, to determine surficial extent, was accomplished by geologic reconnaissance over existing roads.

Of the parameters listed, grain size is the most important for engineering purposes and, for this reason, is included in the geologic unit designation. However, grain size is not readily mapped on aerial photos, and much of the field work involved determination of the extent of surficial deposits of a particular grain-size category (gravel, sand, or fine-grained).

Terrain data were also taken at geologic field stations. Drainage width and depth were estimated and predominant surface slope was measured. Slopes were measured over a distance of 100 to 150 feet (31 to 46 m) with an Abney hand level. For additional data, depths of major drainages encountered during geologic reconnaissance between stations were recorded on the aerial photographs.

To help refine depth to rock interpretations, observations were concentrated along the basin margin to identify areas of shallow rock. Observations regarding depth to water were restricted to measurements in existing wells and identification of areas with water at the surface.

A4.0 GEOPHYSICAL PROCEDURES

A4.1 SEISMIC REFRACTION SURVEYS

A4.1.1 Instruments

Field explorations were performed with a 24-channel SIE Model RS-44 seismic refraction system which consisted of 24 amplifiers coupled with a dry-write, galvanometer-type recording oscillograph. Seismic energy was detected by Mark Products Model L-10 geophones with natural frequency of 4.5 Hz. Geophones were fitted with short spikes to provide good coupling with the ground. Cables with two takeout intervals were used to transmit the detected seismic signal from the geophones to the amplifiers. Time of shot was transmitted from shot point to recording system via an FM radio link.

The degree of gain was set on the amplifiers by the instrument operators and was limited by the background noise at the time of the shot. The amplifiers are capable of maximum gain of 1.1 million. The oscillograph placed timing lines on the seismograms at 0.01-second intervals. The timing lines form the basis for measuring the time required for the energy to travel from the shot to each geophone.

A4.1.2 Field Procedures

Each seismic refraction line consisted of a single spread of 24 geophones with a distance of 410 feet (125 m) between end points. Geophone spacing provided six intervals of 25 feet (7.6 m) at both ends of the line and 11 central intervals of 10 feet (3 m). Six shots were made per spread at locations 65 feet (20 m), 190 (58 m) and 305 feet (93 m) left and right of the spread center. The recording system was located between geophones 12 and 13.

The explosive used was "Kinestik" which was transported to the site as two nonexplosive components, a powder and a liquid. The components were mixed in the field to make a explosive compound. Charges ranged in size from one-third to five pounds and were buried from 1 to 5 feet (0.3 to 1.5 m) deep. Charges were detonated using Reynold's exploding bridge wire (EBW) detonators instead of conventional electric blasting caps. Use of EBWs provides maximum safety against accidental detonation and extremely accurate "time breaks" (instant of detonation). Relative elevations of geophones and shot points were obtained by level or transit where lines had more than 2 or 3 feet (0.6 to 0.9 m) of relief.

A4.1.3 Data Reduction

The travel times for compressional waves from the shots to the geophones were obtained from the seismograms by visual inspection. These times were plotted at their respective horizontal

distances and best fit lines were drawn through the points to obtain apparent velocities for materials below the seismic line.

A combination of delay time and ray tracing methods was used in a computer program to obtain depth to refracting horizons from the time-distance information.

A4.2 ELECTRICAL RESISTIVITY SURVEYS

A4.2.1 Instruments

Electrical resistivity measurements were made with a Bison Instrument model 2350B resistivity meter which provides current to the earth through two electrodes and measures the potential (voltage) drop across two other electrodes.

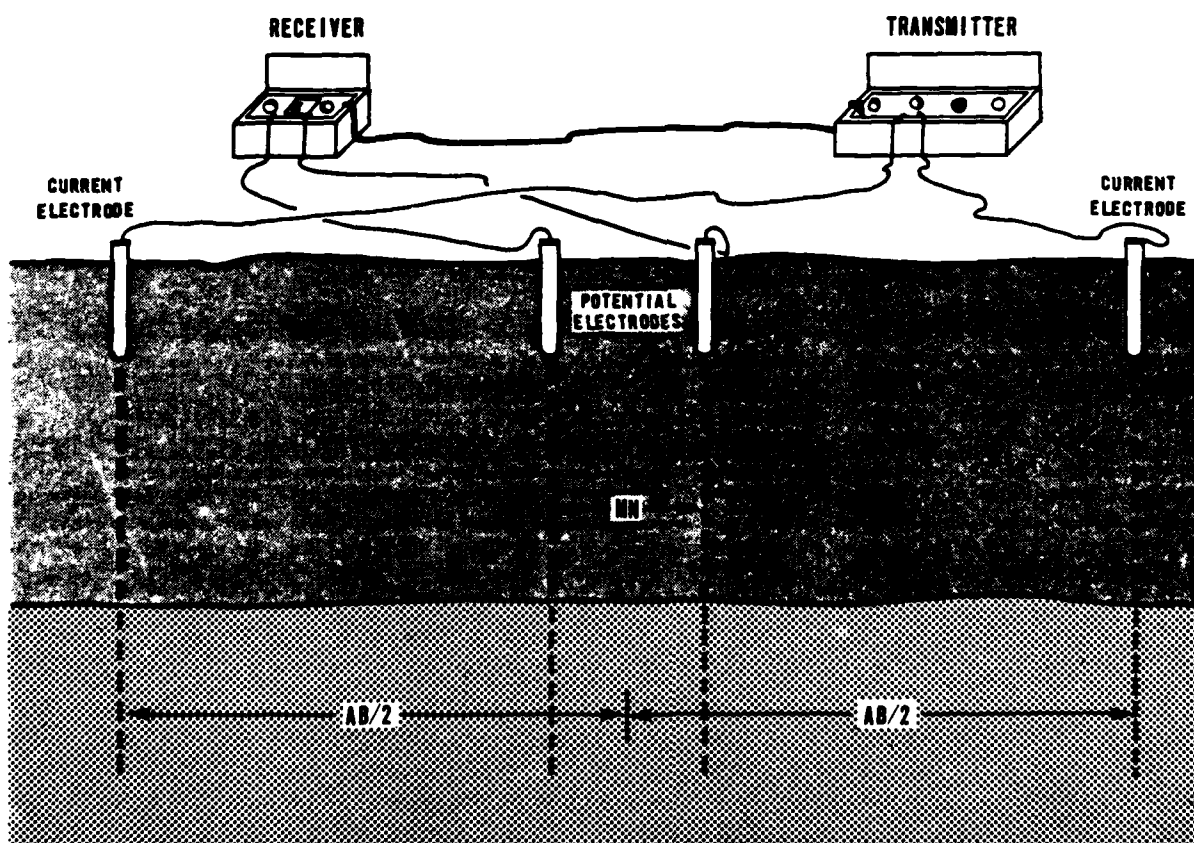
A4.2.2 Field Procedures

Electrical resistivity soundings were made using the Schlumberger electrode arrangement. Soundings are made by successive resistivity measurements which obtain information from deeper and deeper materials. The depth of penetration of the electrical current is increased by increasing the distance between the current electrodes. The arrangement of electrodes in the Schlumberger method is shown in Figure A4-1. The four electrodes are in a line with the two current electrodes on the ends. The distance between the current electrodes (AB) is always five or more times greater than the distance between the potential electrodes (MN).

The initial readings are made with MN equal to 5 feet (1.5 m) and AB equal to 30 feet (9 m). Successive readings were made with AB at 40, 50, 60, 80, 100, 120, 160, 200, 300, 400, 500, and 600 feet (12, 15, 18, 24, 30, 37, 49, 61, 91, 122, 152, and 183 m). MN spacing is sometimes increased one or two times as AB is expanded. This increase is required when the signal drops to a level below the meter's sensitivity. The potential drop is greater between more widely spaced electrodes (MN), so increasing MN increases the signal. When it becomes necessary to increase MN, the spacing of AB is reduced to the spacing of the previous reading. MN is then increased and a measurement is made. This provides two resistivity measurements at the same AB spacing but with different MN spacings.

A4.2.3 Data Reduction

Each apparent resistivity value is plotted versus one-half the current electrode spacing (AB/2) used to obtain it. Log-log graph paper is used to form the coordinates for the graph. A smooth curve is drawn through the points. This sounding curve forms the basis for interpreting the resistivity layering at the sounding location.



**SCHLUMBERGER ARRAY
ELECTRICAL RESISTIVITY SOUNDINGS
VERIFICATION SITES, NEVADA - UTAH**

MX SITING INVESTIGATION
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FIGURE
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A computer program that does iterative "curve-matching" is used to develop a layer model that has a theoretical resistivity curve that is similar to the field curve. An electronic digitizer is used to digitize the field curve for computer program input.

A5.0 ENGINEERING PROCEDURES

Soil engineering activities consisted of the following:

1. Field activities:

- o Borings
- o Trenches
- o Test Pits
- o Surficial Samples
- o Cone Penetrometer Tests
- o Field CBR Tests

2. Office activities:

- o Laboratory Tests
- o Data Analyses and Interpretations

The procedures used in the various activities are described in the following sections.

A5.1 BORINGS

A5.1.1 Drilling Techniques

The borings were drilled at designated locations using rotary techniques. A truck-mounted Failing 1500 drill rig with hydraulic pulldown was used. The borings were nominally 4 7/8 inches (124 mm) in diameter. A bentonite-water slurry was used to return soil cuttings to the surface. A tricone drill bit was used for coarse-grained soils and a drag bit for drilling in fine-grained soils. Depths drilled ranged from 160 to 200 feet (49 to 61 m) unless bedrock was encountered at lesser depth.

A5.1.2 Method of Sampling

A5.1.2.1 Sampling Intervals

Soil samples were obtained at the following nominal depths as well as at depths of change in soil type:

- 0' to 10' (0.0 to 3.0 m) - Pitcher or drive-samples at 3' intervals
- 10' to 30' (3.0 to 9.1 m) - Pitcher or drive-samples at 5' intervals
- 30' to 120' (9.1 to 36.6 m) - Pitcher or drive-samples at 10' intervals
- 120' to 200' (36.6 to 61.0 m) - Pitcher or drive-samples at 20' intervals

A5.1.2.2 Sampling Techniques

a. Fugro Drive Samples: Fugro drive samplers were used to obtain relatively undisturbed soil samples. The Fugro drive

sampler is a ring-lined barrel sampler with an outside diameter of 3.0 inches (76.2 mm) and inside diameter of 2.50 inches (65.5 mm). It contains 12 individual 1-inch- (25.4-mm-) long rings and is attached to a 12-inch- (30-cm-) long waste barrel.

The sampler was advanced using a downhole hammer weighing 300 pounds (136 kg) with a drop of 24 inches (61.0 cm).

The number of blows required to advance the sampler for a 6-inch (15-cm) interval were recorded. Samples obtained were retained in the rings, placed in plastic bags with manually twisted top ends and sealed in plastic sample containers. Each sample was identified with a label indicating job number, boring number, sample number, depth range, Unified Soil Classification Symbol (USCS), (Table A5-1) and date. Ring samples were placed in foam-lined steel boxes.

b. Pitcher Samples: The Pitcher sampler was used to obtain undisturbed soil samples. The primary components of this sampler are an outer rotating core barrel with a bit and an inner, stationary, spring-loaded, thin-wall sampling tube which leads or trails the outer barrel drilling bit, depending on the hardness of the material penetrated. The average inside diameter of the sampling tubes used was 2.87 inches (73 mm). Before placing the Pitcher tube in the outer barrel, the tube was inspected for sharpness and protrusions.

The Pitcher sampler was then lowered to the bottom of the boring and the thin-walled sampling tube advanced into the soil ahead of the rotating cutting bit by the weight of the drill rods and hydraulic pulldown. The thin-walled sampling tube was retracted into the core barrel and the sampler was brought to the surface. After removal of the sampling tube from the core barrel, the length of the recovered soil sample was measured and recorded. Before preparing and sealing the tube, the drilling fluid in the Pitcher tube was removed. Cap plugs were taped in place on the top and bottom of the Pitcher tube and sealed with wax. When Pitcher samples could not be retrieved without disturbance, they were clearly marked as "disturbed." Each sealed Pitcher tube was labeled as explained under "Fugro Drive Samples" and then placed vertically in foam-lined wooden boxes.

c. Bulk Samples: Bulk samples from rotary drilling were obtained by screening the returning drilling fluid to obtain wash samples. Recovered samples were placed in plastic bags and labeled as explained previously.

d. Split-Spoon Samples: Split-spoon samplers were used to obtain disturbed, but representative, soil samples continuously in the top 10.5 feet (3.2 m). Soil samples were classified and disposed of in the field. The split-spoon sampler consists of a barrel shoe, a split barrel or tube, a solid sleeve, and a sampler head. The inside diameter of the sampler shoe is 1.375 inches (35 mm) and the length is about 18 inches (45.7 cm).

| Field Identification Procedures (Excluding particles larger than 3 in. and basis fractions on estimated weights) | | | | Group Symbols | | Typical Names | | Information Required for Describing Soils | | Laboratory Classification Criteria | |
|--|--|--|--|---------------|--|---|--|---|--|---|--|
| Coarse-grained soils More than half of coarse fraction is larger than No. 200 sieve size (For values classification, the 3 in. size may be used as basis) | | | | GW | | Well graded gravel, gravel-sand mixtures, little or no fines | | Give typical name; indicate approximate percentages of sand and gravel; maximum size; surface condition; and other pertinent descriptive information. Use symbols in parentheses. | | $C_u = \frac{D_{60}}{D_{10}}$ Greater than 4 $C_u = \frac{D_{60}}{D_{10} \times D_{30}}$ Between 1 and 3 Not meeting all gradation requirements for GW | |
| Sands More than half of coarse fraction is larger than No. 4 sieve size | | | | GP | | Poorly graded gravel, gravel-sand mixtures, little or no fines | | For undisturbed soils add information on stratification, degree of compaction, cementation, and moisture conditions and drainage characteristics. | | Atterberg limits below "A" line with P_f between 4 and 7 are <i>borderline</i> cases requiring use of dual symbols Atterberg limits above "A" line with P_f greater than 7 are <i>borderline</i> cases requiring use of dual symbols | |
| Gravelly sands More than half of coarse fraction is larger than No. 4 sieve size | | | | GM | | Silty gravel, poorly graded gravel-sand mixtures | | Example: Silty sand, gravelly, about 20% gravel, maximum size rounded and subangular sand grains, plastic fines, about 10% organic, well compacted and moist in place, alluvial sand, (SM) | | Atterberg limits below "A" line with P_f between 4 and 7 are <i>borderline</i> cases requiring use of dual symbols Atterberg limits above "A" line with P_f greater than 7 are <i>borderline</i> cases requiring use of dual symbols | |
| Gravelly silts More than half of coarse fraction is larger than No. 4 sieve size | | | | GC | | Clayey gravel, poorly graded gravel-sand mixtures | | | | Atterberg limits below "A" line with P_f between 4 and 7 are <i>borderline</i> cases requiring use of dual symbols Atterberg limits above "A" line with P_f greater than 7 are <i>borderline</i> cases requiring use of dual symbols | |
| Gravelly silts More than half of coarse fraction is larger than No. 4 sieve size | | | | SW | | Well graded sands, gravelly sands, little or no fines | | | | $C_u = \frac{D_{60}}{D_{10}}$ Greater than 6 $C_u = \frac{D_{60}}{D_{10} \times D_{30}}$ Between 1 and 3 Not meeting all gradation requirements for SW | |
| Gravelly silts More than half of coarse fraction is larger than No. 4 sieve size | | | | SP | | Poorly graded sands, gravelly sands, little or no fines | | | | Atterberg limits below "A" line with P_f between 4 and 7 are <i>borderline</i> cases requiring use of dual symbols Atterberg limits above "A" line with P_f greater than 7 are <i>borderline</i> cases requiring use of dual symbols | |
| Gravelly silts More than half of coarse fraction is larger than No. 4 sieve size | | | | SM | | Silty sands, poorly graded sand-silt mixtures | | | | Atterberg limits below "A" line with P_f between 4 and 7 are <i>borderline</i> cases requiring use of dual symbols Atterberg limits above "A" line with P_f greater than 7 are <i>borderline</i> cases requiring use of dual symbols | |
| Gravelly silts More than half of coarse fraction is larger than No. 4 sieve size | | | | SC | | Clayey sands, poorly graded sand-clay mixtures | | | | Atterberg limits below "A" line with P_f between 4 and 7 are <i>borderline</i> cases requiring use of dual symbols Atterberg limits above "A" line with P_f greater than 7 are <i>borderline</i> cases requiring use of dual symbols | |
| Fine-grained soils More than half of material is smaller than No. 200 sieve size (The No. 200 sieve size is used in the chart for identification of fine-grained soils) | | | | ML | | Inorganic silt and very fine sand, rock flour, silty or sandy, fine sand with high plasticity | | Give typical name; indicate degree of plasticity, amount and maximum size of coarse fraction; color in wet condition; and other pertinent descriptive information, and symbol in parentheses. | | Plasticity index | |
| Fine-grained soils More than half of material is smaller than No. 200 sieve size (The No. 200 sieve size is used in the chart for identification of fine-grained soils) | | | | CL | | Inorganic clay of low to medium plasticity, gravelly clay, waxy clay, silty clay, lean clay | | Example: Clayey silt, brown, slightly plastic, small percentage of fine sand, numerous vertical root holes, firm and dry in place, loess, (ML) | | Liquid limit | |
| Fine-grained soils More than half of material is smaller than No. 200 sieve size (The No. 200 sieve size is used in the chart for identification of fine-grained soils) | | | | OL | | Organic silt and organic silty clay of low plasticity | | | | Plasticity chart for laboratory classification of fine grained soils | |
| Fine-grained soils More than half of material is smaller than No. 200 sieve size (The No. 200 sieve size is used in the chart for identification of fine-grained soils) | | | | MH | | Inorganic silt, micaceous or silty, silty sand, silty clay, silty clay of high plasticity | | | | | |
| Fine-grained soils More than half of material is smaller than No. 200 sieve size (The No. 200 sieve size is used in the chart for identification of fine-grained soils) | | | | CH | | Inorganic clay of medium to high plasticity | | | | | |
| Fine-grained soils More than half of material is smaller than No. 200 sieve size (The No. 200 sieve size is used in the chart for identification of fine-grained soils) | | | | OH | | Organic clay of medium to high plasticity | | | | | |
| Fine-grained soils More than half of material is smaller than No. 200 sieve size (The No. 200 sieve size is used in the chart for identification of fine-grained soils) | | | | PI | | Peat and other highly organic soil | | | | | |

Use the grain size curve in identifying the fractions as given under field identification

Plasticity index

Liquid limit

Plasticity chart for laboratory classification of fine grained soils

After removing particles larger than No. 40 sieve size, prepare a pat of soil moist and with a volume of about one-half cubic inch. Add enough water if necessary to make the soil soft but not sticky. Place the pat in the open palm of one hand and shake horizontally, striking repeatedly against the other hand. A clean, smooth surface of the soil will appear. If the soil is very moist, it will be squeezed between the fingers, the water and silt will disappear from the surface, the pat will stiffen and finally it cracks or crumbles. The rapidity of appearance of water during shaking and of its disappearance during squeezing are important factors in the identification of the soil. Very fine clay soils give the quickest and most distinct reactions whereas a plastic clay has no reaction. Inorganic silts, such as a typical rock flour, show a moderately quick reaction.

These procedures are to be performed on the basis No. 40 sieve size particles, approximately 1/4 in. For field classification purposes, screening is not intended, simply remove by hand the coarse particles that interfere with the test.

After removing particles larger than No. 40 sieve size, prepare a pat of soil moist and with a volume of about one-half cubic inch. Add enough water if necessary to make the soil soft but not sticky. Place the pat in the open palm of one hand and shake horizontally, striking repeatedly against the other hand. A clean, smooth surface of the soil will appear. If the soil is very moist, it will be squeezed between the fingers, the water and silt will disappear from the surface, the pat will stiffen and finally it cracks or crumbles. The rapidity of appearance of water during shaking and of its disappearance during squeezing are important factors in the identification of the soil. Very fine clay soils give the quickest and most distinct reactions whereas a plastic clay has no reaction. Inorganic silts, such as a typical rock flour, show a moderately quick reaction.

From Wiesner, 1971.

a. Boundary classification. Soils possessing characteristics of two groups are designated by combinations of group symbols. For example GW-GC, well graded gravel-sand mixture with clay binder.

Unified Soil Classification System

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TABLE A5-1

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UNIFIED SOIL CLASSIFICATION SYSTEM

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DEPARTMENT OF THE AIR FORCE - SANSO

TABLE
A5-1

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Sampling with the split barrel sampler is accomplished by driving the sampler into the ground with a 140-pound (63.6-kg) hammer dropped 30 inches (76 cm). The number of blows required

e. Rock Samples: Rock cores are obtained with a sampler which consists of a core barrel with a diamond cutting bit at its lower end. The bit cuts an annular hole in the rock mass, thereby creating a cylinder or core of rock which is recovered in the core barrel. Rock cores were obtained using rotary drilling methods and NX double-tube core barrels (core size 2.125 inches [54 mm]). When rock was encountered in a boring, approximately 15 feet (4.5 m) of core was obtained before abandoning the hole. The rock cores were removed from the core barrel, examined by a geologist, and placed in core boxes. The core boxes were labeled as explained above in "Fugro Drive Samples."

A5.1.3 Logging

All soils were classified in the field by the procedures outlined in Section A5.5, "Field Visual Soil Classification," of this Appendix. Rock encountered in the borings was described according to classifications given in Travis (1955) and Folk (1974). The following general information was entered on the boring logs at the time of drilling: boring number; project name, number, and location; name of drilling company and driller; name of logger and date logged; and method of drilling and sampling, drill bit type and size, driving weight and average drop as applicable. As drilling progressed, the soil samples recovered were visually classified as outlined in Section A5.5, "Field Visual Soil Classification," and the description was entered on the logs. Section A5.5 also discusses other pertinent data and observations made, which were entered on the boring logs, during drilling.

A5.1.4 Sample Storage and Transportation

Samples were handled with care, drive sample containers being placed in foam-lined steel boxes, while Pitcher samples were transported in foam-lined wooden boxes. Particular care was exercised by drivers while traversing rough terrain to avoid disturbing the samples. Whenever ambient air temperatures fell below 32°F, samples were stored in heated rooms during the field work and transported to Fugro National's Long Beach laboratory in heated cabins in back of pickup trucks.

A5.1.5 Ground-Water Observation Wells

When ground water was encountered during drilling or where a boring was located in an area estimated to have ground water within 150 feet (46 m) of the ground surface, the completed boring was cased with 2-inch-diameter- (51-mm-) polyvinyl-chloride (PVC) pipe to 160 feet (49 m). The PVC pipe was slotted

in the bottom 20 feet (6 m). Then the pipe, was flushed until the water was clear and the annulus was backfilled with pea gravel to approximately 30 feet (9 m) above the bottom of the boring. After equilibrium was reached, the water level was measured and recorded periodically.

A5.2 TRENCHES, TEST PITS, AND SURFICIAL SAMPLES

A5.2.1 Excavation Equipment

The trenches, test pits, and surficial samples were excavated using a rubber tire-mounted Case 580C backhoe with a maximum depth capability of 14 feet (4.3 m).

A5.2.2 Method of Excavation

Unless caving occurred during the process of excavation, the trench width was nominally 2 feet (0.6 m). Trench depths were typically 10 to 14 feet (3.0 to 4.3 m) and length 14 feet (4.3 m). Test pits were nominally 2 feet (0.6 m) wide, 5 feet (1.5 m) deep, and ranged from 5 to 10 feet (1.5 to 3.0 m) in length. Surficial sample excavations were typically 2 feet (0.6 m) wide, 2 to 3 feet (0.6 to 1.0 m) deep, and about 3 to 5 feet (0.9 to 1.5 m) long. The trench and test pit walls were vertical. However, where surface materials were unstable, the trench walls were sloped back to a safe angle to prevent sloughing during the completion of excavation and logging. The excavated material was deposited on one side at least 4 feet (1.2 m) from the edge of the trenches in order to minimize stress loads at the edges. The excavations were backfilled with the excavated material and the ground surface was restored to a condition as conformable with the surrounding terrain as practical.

A5.2.3 Sampling

The following sampling procedures were generally followed for all trenches, test pits, and surficial samples.

- o Representative bulk soil samples (large or small) were obtained in the top 2 feet (0.6 m). If the soil type changed in the top 2 feet, bulk samples of both the soil types were obtained. In addition, bulk samples of all soil types encountered at different depths in the excavation were obtained. For each soil type in the top 2 to 3 feet (0.6 to 0.9 m), two large bulk samples (weighing about 50 pounds [22.7 kg] each) were taken. Bulk samples from other depths were limited to one bag. When soils from two locations were similar, only a small bag sample weighing about 2 pounds (0.9 kg) was taken from the second location.
- o All large bulk samples were placed first in plastic bags and then in cloth bags. The small bulk samples were placed in small plastic bags. All sample bags of soil were tied tightly at the top to prevent spillage and tagged with the

following information: project number; trench, test pit, or surficial sample number; bulk sample number; depth range in feet; Unified Soil Classification Symbol; and date. The samples were transported to the field office for storage and then to Fugro National's Long Beach office in pickup trucks.

A5.2.4 Logging

The procedures for field visual classification of soil and rock encountered from the trenches, test pits, and surficial samples were basically the same as the procedures for logging of borings (Section A5.1.3). For excavations shallower than 4 feet (1.2 m) technicians entered the excavations and logged them. Logging of the excavations deeper than 4 feet (1.2 m) was accomplished from the surface and by observing the backhoe bucket contents. All trench walls were photographed prior to backfilling.

Each field trench, test pit, and surficial sample log included trench, test pit, or surficial sample number; project name, number and location; name of excavator; type of excavation equipment; name of logger; and date logged. As excavations proceeded, the soil types encountered were visually classified and described as outlined in Section A5.4, "Field Visual Soil Classification." Section A5.4 also discusses other pertinent data and observations made which were entered on the logs during excavation.

A5.3 CONE PENETROMETER TESTS

A5.3.1 Equipment

The equipment consisted of a truck-mounted [17.5 tons (15,877 kg) gross weight] electronic cone penetrometer equipped with a 15-ton (13,608 kg) friction cone (cone end resistance capacity of 15 tons (13,608 kg) and 4-1/2-ton (4082-kg) limit on the friction sleeve). All operating controls, recorder, cables, and ancillary equipment were housed in the specially designed vehicle which was completely self-contained. The penetrometer, the key element of the system, contained the necessary load cells and cable connections. One end of the unit was threaded to receive the first sounding rod. When carrying out the tests, hollow rods with an outside diameter of 1.42 inches (3.6 cm) and a length of 3.3 feet (1.0 m) were used to push down the cone. The hydraulic thrust system was mounted over the center of gravity of the truck, permitting use of the full 17.5-ton (15,877-kg) truck weight as load reaction.

The cone had an apex angle of 60° and a base area of 2.3 in² (15 cm²). The resistance to penetration was measured by a built-in load cell in the tip and was relayed to the surface recorder via cables in the sounding rods. The friction sleeve, having an area of 31.8 in² (205 cm²), was fitted above

the cone base. The local friction was measured by load cells mounted in the friction sleeve and recorded in the same manner as the end resistance. The end resistance and friction resistance were recorded on a strip chart.

A5.3.2 Test Method

Tests were performed in accordance with ASTM D 3441-75T, "Tentative Method for Deep, Quasi-Static, Cone and Friction-Cone Penetration Tests of Soil." Basically, the test was conducted by positioning the electronic cone penetrometer truck over the designated area for testing, setting the outriggers on the ground surface, checking the level of the rig, then pushing the cone into the ground at a rate of 0.79 in/sec (2 cm/sec) until refusal (defined as the capacity of the cone, friction sleeve, or hydraulics system) or the desired depth of penetration was reached. As a general rule, the depth of penetration did not exceed 33 feet (10 m). If refusal was reached within the top 2 or 3 feet, the test was performed again a few feet away from the first location. Details of the test such as refusal reached, depth, cone used, etc. were entered on a log sheet.

A minimum of three cone penetrometer tests were performed at all field California Bearing Ratio (CBR) test locations.

A5.4 FIELD CALIFORNIA BEARING RATIO (CBR) TESTS

A5.4.1 Equipment

The equipment used to conduct the field CBR tests was as described in the U.S. Army Corps of Engineers' Technical Manual 5-30. Other equipment for conducting a field density test by the sand cone method (ASTM D 1556-64, Test for Density of Soil in Place by the Sand-Cone Method) and the "Speedy Moisture Meter" for field determination of soil moisture content were also included. A backhoe and shovels were used to excavate the CBR test pits.

A5.4.2 Test Method

Field CBR tests were generally performed at four depths at each designated location. The procedures for conducting the CBR tests were as described in the U.S. Army Corps of Engineers' Technical Manual (TM) 5-30, pp. 2-86 to 2-96. Tests were performed in test pits at depths ranging from 1 to 4 feet (0.3 to 1.2 m) below ground surface. Testing was not attempted where numerous cobbles or heavily cemented soils were encountered. Three CBR tests were performed at each depth and the results recorded. Generally, a field density test (ASTM D 1556-64, Test for Density of Soil in Place by the Sand-Cone Method) and moisture content determination (by Speedy Moisture Meter Method) were performed at the CBR test depths.

A5.4.3 Sampling

At each CBR test location, large bulk samples of soils at test depths were obtained. See Section A5.2.3, "Sampling," for trenches, test pits, and surficial samples for details.

A5.4.4 Logging

Field CBR test results, field density test results, and moisture content determinations were recorded at the time of each test. All soil samples were classified and logged in accordance with the procedures outlined in Section A5.5, "Field Visual Soil Classification."

A5.5 FIELD VISUAL SOIL CLASSIFICATION

A5.5.1 General

All field logging of soils was performed in accordance with the procedures outlined in this section. Soil samples were visually classified in the field in general accordance with the procedures of ASTM D 2488-69, Description of Soils (Visual-Manual Procedure). The ASTM procedure is based on the Unified Soil Classification System (see Table A5-1). It describes several visual and/or manual methods which can be used in the field to estimate the USCS soil group for each sample. The following section details several of the guidelines used in the field for describing soils, drilling and excavating conditions, and unusual conditions encountered.

A5.5.2 Soil Description

Soil descriptions entered on the logs of borings, trenches, test pits, and surficial samples generally included those listed below.

Coarse-Grained Soils

USCS Name and Symbol
Color
Range in Particle Size
Gradation (well, poorly)
Density
Moisture Content
Particle Shape
Reaction to HCl

Fine-Grained Soils

USCS Name and Symbol
Color
Consistency
Moisture Content
Plasticity
Reaction to HCl

Some additional descriptions or information recorded for both coarse- and fine-grained soils included: degree of cementation, secondary material, cobbles and boulders, and depth of change in soil type.

Definitions of some of the terms and criteria used to describe soils and conditions encountered during the investigations follow.

a. USCS Name and Symbol: Derived from Table A5-1, the Unified Soil Classification System. The soils were first designated as coarse- or fine-grained.

Coarse-grained soils are those in which more than half (by weight) of the particles are visible to the naked eye. In making this estimate, particles coarser than 3 in. (76 mm) in diameter were excluded. Fine-grained soils are those in which more than half (by weight) of the particles are so fine that they cannot be seen by the naked eye. The distinction between coarse- and fine-grained can also be made by sieve analysis with the No. 200 sieve (.074 mm) size particle considered to be the smallest size visible to the naked eye. In some instances, the field technicians describing the soils used a No. 200 sieve to estimate the amount of fine-grained particles. The coarse-grained soils are further divided into sands and gravels by estimating the percentage of the coarse fraction larger than the No. 4 sieve (about 1/4 inch or 5 mm). Each coarse-grained soil is then qualified as silty, clayey, poorly graded, or well-graded as discussed under plasticity and gradation.

Fine-grained soils were identified in the field as clays or silts with appropriate adjectives (clayey silt, silty clay, etc.) based on the results of dry strength, dilatancy, and plastic thread tests (see ASTM D 2488-69 for details of these tests).

Dual USCS symbols and adjectives were used to describe soils exhibiting characteristics of more than one USCS group.

b. Color: Color descriptions were recorded using the following terms with abbreviations in parentheses.

| | |
|------------|-------------|
| White (w) | Green (gn) |
| Yellow (y) | Blue (bl) |
| Orange (o) | Gray (gr) |
| Red (r) | Black (blk) |
| Brown (br) | |

Color combinations as well as modifiers such as light (lt) and dark (dk) were used.

c. Range in Particle Size: For coarse-grained soils (sands and gravels), the size range of the particles visible to the naked eye was estimated as fine, medium, coarse, or a combined range (fine to medium).

d. Gradation: Well graded indicates a coarse-grained soil which has a wide range in grain size and substantial amounts of most intermediate particle sizes. A coarse-grained soil was identified as poorly graded if it consisted predominantly of one size (uniformly graded) or had a wide range of sizes with some intermediate sizes obviously missing (gap-graded).

e. Density or Consistency: The density or consistency of the in-place soil was estimated based on the number of blows required to advance the Fugro drive or split-spoon sampler, the drilling rate and/or hydraulic pulldown needed to drill, ease (or difficulty) of excavation of trench or test pit, or trench or test pit wall stability. For fine-grained soils, the field guides to shear strength presented below were also used to estimate consistency.

- o Coarse-grained soils - GW, GP, GM, GC, SW, SP, SM, SC (gravels and sands)

| <u>Consistency</u> | <u>N-Value (ASTM D 1586-67), Blows/Foot</u> |
|--------------------|---|
| Very Loose | 0 - 4 |
| Loose | 4 - 10 |
| Medium Dense | 10 - 30 |
| Dense | 30 - 50 |
| Very Dense | >50 |

- o Fine-grained Soils - ML, MH, CL, CH (Silts and Clays)

| <u>Consistency</u> | <u>Shear Strength</u> (ksf) (kN/m ²) | | <u>Field Guide</u> |
|--------------------|---|------------|---|
| Very Soft | <0.25 | <12 | Sample with height equal to twice the diameter, sags under own weight |
| Soft | 0.25-0.50 | 12.0-24.0 | Can be squeezed between thumb and forefinger |
| Firm | 0.50-1.00 | 24.0-48.0 | Can be molded easily with fingers |
| Stiff | 1.00-2.00 | 48.0-96.0 | Can be imprinted with slight pressure from fingers |
| Very Stiff | 2.00-4.00 | 96.0-192.0 | Can be imprinted with considerable pressure from fingers |
| Hard | >4.00 | >192.0 | Cannot be imprinted by fingers |

- f. Moisture Content: The following guidelines were used in the field for describing the moisture in the soil samples:

Dry : No feel of moisture
 Slightly Moist: Much less than normal moisture
 Moist : Normal moisture for soil
 Very Moist : Much greater than normal moisture
 Wet : At or near saturation

- g. Particle Shape: Coarse-grained soils

Angular : Particles have sharp edges and relatively plane sides with unpolished surfaces

- Subangular: Particles are similar to angular but have somewhat rounded edges
- Subrounded: Particles exhibit nearly plane sides but have well-rounded corners and edges
- Rounded: Particles have smoothly curved sides and no edges

h. Reaction to HCl: As an aid for identifying cementation, some soil samples were tested in the field for their reaction to dilute hydrochloric acid. The intensity of the HCl reaction was described as none, weak, or strong.

i. Degree of Cementation: Based on the intensity of the HCl reaction and observation, the degree of cementation of a soil layer was described as weak to strong. Also, the following stages of development of caliche (cemented) profile were indicated where applicable.

| Stage | Gravelly Soils | Nongravelly Soils |
|-------|---|--|
| I | Thin, discontinuous pebble coatings | Few filaments or faint coatings |
| II | Continuous pebble coatings, some interpebble fillings | Few to abundant nodules, flakes, filaments |
| III | Many interpebble fillings | Many nodules and internodular fillings |
| IV | Laminar horizon overlying plugged horizon | Increasing carbonate impregnation |

j. Secondary Material: Example - Sand with trace to some silt

| | |
|--------|------------------------|
| Trace | 5-12% (by dry weight) |
| Little | 13-20% (by dry weight) |
| Some | >20% (by dry weight) |

k. Cobbles and Boulders: A cobble is a rock fragment, usually rounded or subrounded, with an average diameter between 3 and 12 inches (76 and 305 mm). A boulder is a rock fragment, usually rounded by weathering or abrasion, with an average diameter of 12 inches (305 mm) or more. The presence of cobbles and/or boulders was identified by noting the sudden change in drilling difficulty or cuttings in borings or by visual observation in excavations. An estimate of the size, range, and percentage of cobbles and/or boulders in the strata was recorded on the logs.

l. Depth of Change in Soil Type: During drilling of borings, the depths of changes in soil type were determined by observing samples, drilling rates, changes in color or consistency of

drilling fluid, and relating these to depth marks on the drilling rods. In excavations, strata thicknesses were measured with a tape. All soil type interfaces were recorded on the logs by a horizontal line at the approximate depth mark.

In addition to the observations recorded relating to soil descriptions, remarks concerning drilling difficulty, loss of drilling fluid in the boring, water levels encountered, trench wall stability, ease of excavation, and other unusual conditions were recorded on the logs.

A5.6 LABORATORY TESTS

Laboratory tests were performed on selected representative undisturbed and bulk samples. All laboratory tests (except chemical tests) were performed in Fugro National's Long Beach laboratory. The chemical tests were conducted by Pomeroy, Johnson, and Bailey Laboratories of Pasadena, California. All tests were performed in general accordance with the American Society for Testing and Materials (ASTM) procedures. The types of tests performed and their ASTM designations are summarized as follows.

| <u>Type of Test</u> | <u>ASTM Designation</u> |
|--------------------------------------|-------------------------|
| Unit Weight | D 2937-71 |
| Moisture Content | D 2216-71 |
| Particle-Size Analysis | D 422-63 |
| Liquid Limit | D 423-66 |
| Plastic Limit | D 424-59 |
| Triaxial Compression | D 2850-70 |
| Unconfined Compression | D 2166-66 |
| Direct Shear | D 3080-72 |
| Consolidation | D 2435-70 |
| Compaction | D 1557-70 |
| California Bearing Ratio (CBR) | D 1883-73 |
| Specific Gravity | D 854-58 |
| Water Soluble Sodium | D 1428-64 |
| Water Soluble Chloride | D 512-67 |
| Water Soluble Sulfate | D 516-68 |
| Water Soluble Calcium | D 511-72 |
| Calcium Carbonate | D 1126-67 |
| Test for Alkalinity (pH) | D 1067-70 |

A5.7 DATA ANALYSIS AND INTERPRETATION

A5.7.1 Preparation of Final Logs and Laboratory and Field Test Summary Sheets

The field logs of all borings, trenches, test pits, and surficial sample excavations were prepared by systematically combining the information given on the field logs with the laboratory test results. The resultant logs include generally the following information: description of soil types encountered; sample

types of intervals, lithology (graphic soil column); estimates of soil density or consistency; depth locations of changes in soil types; remarks concerning trench wall stability; drilling difficulty, cementation, and cobbles and boulders encountered; and the total depth of exploration. Laboratory test results presented in the logs include dry density and moisture content; percent of gravel, sand, and fines; and liquid limit and plasticity index. Also, miscellaneous information such as surface elevation, surficial geologic unit, date of activity, equipment used, and dimensions of the activity are shown on the log.

Field CBR test summary sheets were prepared and include the following information for each test site: depth of test; USCS soil type; grain-size distribution and plasticity (from lab testing); in-situ dry unit weight and moisture content (from lab testing); average field CBR values; and remarks concerning cementation and induration.

Laboratory data were summarized in tables. All samples which were tested in the laboratory were listed. Results of sieve analyses, hydrometer, Atterberg limits, in-situ dry strength and moisture content tests, and calculated degree of saturation and void ratio were entered on the tables. Test summary sheets for triaxial compression, unconfined compression, direct shear, consolidation, chemical, CBR, and compaction tests were prepared separately.

The Cone Penetrometer Test results consist of continuous plots of cone resistance, friction sleeve resistance, and friction ratio versus depth from ground surface. Beside the plot is shown a soil column with USCS soil types encountered at the test location. Other information presented on the log includes surface elevation and surficial geologic unit.

Volume II titled "Geotechnical Data" presents the following finalized basic engineering data.

| | |
|--------------------------------|------------------|
| Boring Logs | Section II - 5.0 |
| Trench and Test Pit Logs | Section II - 6.0 |
| Surficial Sample Logs | Section II - 7.0 |
| Laboratory Test Results | Section II - 8.0 |
| Field CBR Results | Section II - 9.0 |
| Cone Penetrometer Test Results | Section II -10.0 |

A5.7.2 Soil Characteristics

A5.7.2.1 General

The soil characteristics are discussed in two parts, surface soils and subsurface soils. The following three tables were prepared and are presented in Sections 3.3 and 3.4 of the report.

1. Characteristics of Surficial Soils;
2. Thickness of Low Strength Surficial Soils; and
3. Characteristics of Subsurface Soils.

The following sections, A5.7.2.2 and A5.7.2.3, explain the data analyses and interpretation used in preparing the above tables.

A5.7.2.2 Surface Soils

In order to define the characteristics of the surficial soils, data from trenches, test pits, borings, surficial soil samples, cone penetrometer tests, field CBR tests and surficial geologic maps were reviewed in conjunction with the laboratory test results. The soils were then grouped into three categories of soils with similar general characteristics. These categories, their descriptions, and associated characteristics were tabulated. This table (Characteristics of Surficial Soils, Table 3-1) includes soil descriptions by the Unified Soil Classification System, predominant surficial geologic units, the estimated areal extent (percent) of each category, important physical properties summarized from laboratory test results, and certain road design related data.

The important physical properties summarized include the estimated cobbles content, grain-size analyses, and Atterberg limits. Ranges for these properties were determined from the field logs and laboratory test results. These ranges are useful for categorizing soils, evaluating construction techniques, and providing data for preliminary engineering evaluations and for use by other MX participants.

Road design data presented in Table 3-1 were developed from field and laboratory tests and consist of three distinct groups:

1. Laboratory test results;
2. Suitability of soils for road use; and
3. Low strength surficial soil.

These road design related data were considered important because roads (interconnecting and secondary) constitute a major portion of the geotechnically related costs. The following paragraphs briefly discuss the development of road design data.

a. Laboratory Test Results: These include ranges of maximum dry density, optimum moisture content (ASTM D 1557-70) and CBR (ASTM D 1883-73) at 90 percent relative compaction for each soil category. The maximum dry density and optimum moisture content are important quality control parameters during roadway construction. California Bearing Ratio is the ratio of the resistance to penetration developed by a subgrade soil to that developed by a specimen of standard crushed-rock base material and is the basis for many empirical road design methods used in this country.

b. Suitability of Soils for Road Use: Included in this group is suitability of soils for use as road subgrade, subbase, or

base. Parameters used to make these qualitative assessments were characteristics related to CBR, frost susceptibility, drainage, and volume change potential. The following guidelines were used in estimating the suitability of soils for road use.

1. Suitability as a road subgrade.

- Very Good - soils which can be compacted with little effort to high CBR values (CBR >30), exhibit low frost susceptibility, fair to good drainage, and low volume change potential.
- Good - soils which can be compacted with some effort to moderate CBR values (CBR 15-30), exhibit moderate frost susceptibility, fair drainage, and medium volume change potential.
- Fair - soils which can be compacted with considerable effort to moderate CBR values (CBR 15-30), exhibit moderate to high frost susceptibility, fair to poor drainage, and medium volume change potential.
- Poor - soils which require considerable effort for compaction to even low CBR values (CBR <15), exhibit high frost susceptibility, poor drainage, or high volume change potential. These soils should generally be removed and replaced with better quality material.

2. Suitability as road subbase or base.

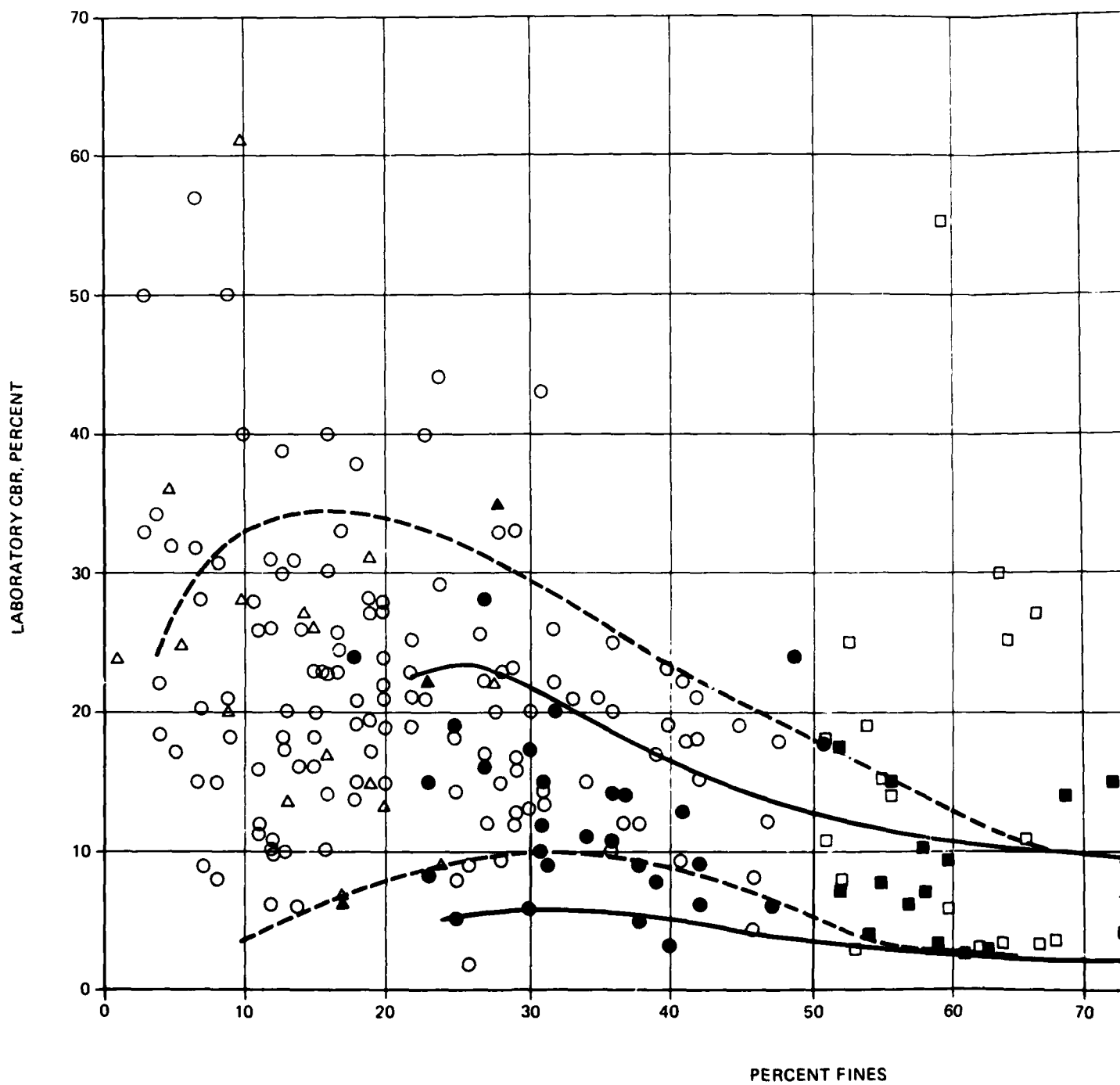
- Good - soils which exhibit negligible frost susceptibility, good drainage, and negligible volume change potential.
- Fair - soils which require some treatment or processing to upgrade for use.
- Poor - soils which would require relatively extensive processing or soil stabilization to upgrade for use.
- Not Suitable - soils which cannot be modified to give adequate roadway support.

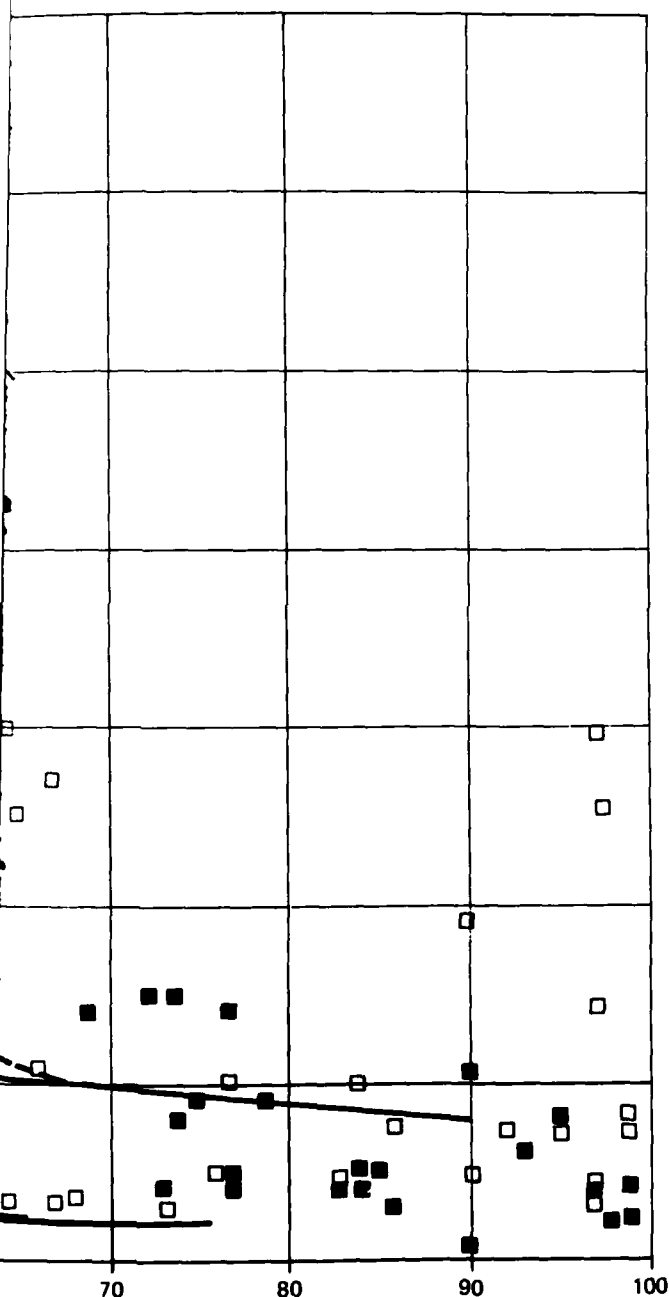
The parameters used in the aforementioned suitability ratings are discussed in the following paragraphs.

- i. CBR Characteristics: California Bearing Ratio, which is commonly used for road design, is dependent on soil

type. During previous verification studies, a limited number of CBR tests were performed on several soil types which were representative of the surficial soils in the various Verification Sites. Based on these test results, a relationship between CBR and percent fines (percent passing through No. 200 sieve) was established and is shown in Figure A5-1. Envelopes for clays and granular soils with plastic fines and silts and granular soils with nonplastic fines are shown in the figure. This plot was used to estimate the range of laboratory CBR values for the various surficial soil categories.

- ii. Other Characteristics: These characteristics pertain to frost susceptibility, drainage, and volume change potential. They were estimated based on the physical properties of the soils, results of consolidation tests (for volume change potential), published literature, and our experience. Following are the definitions of these characteristics.
1. Frost susceptibility is defined as potential for detrimental ice segregation upon freezing or loss of strength upon thawing.
 - Low - negligible to little potential
 - Moderate - some potential
 - High - considerable potential
 2. Drainage characteristics pertain to internal movement of water through soil.
 - Good - materials which drain rapidly and do not tend to plug with fines
 - Fair - natural internal drainage is fairly rapid but there is some tendency for plugging of voids with fines
 - Poor - internal drainage is somewhat slow and plugging with fines can often occur
 - Practically Impervious - materials which exhibit almost no natural internal drainage
 3. Volume change potential corresponds to soil swelling or shrinkage due to change in moisture content.
 - Low - 0 to 2 percent volume change
 - Medium - 2 to 4 percent volume change
 - High - > 4 percent volume change





EXPLANATION

- △ Gravels with nonplastic fines (GM, GW, GP, GP-GM, GW-GM)
- ▲ Gravels with plastic fines (GC, GC-GM)
- Sands with nonplastic fines (SP, SW, SM, SP-SM, SW-SM)
- Sands with plastic fines (SC, SC-SM)
- Silts (ML)
- Clays (CL, CH, CL-ML)
- Envelope for silts and granular soils with nonplastic fines
- Envelope for clays and granular soils with plastic fines

NOTES:

1. Fines correspond to soil passing through No 200 (0.074mm opening) sieve.
2. California Bearing Ratio at 90% relative compaction.
3. Soil types (GM, SC) are based on Unified Soil Classification System.

PLOT OF LABORATORY CBR
VERSUS PERCENT FINES
VERIFICATION SITES, NEVADA UTAH

MX SITING INVESTIGATION
DEPARTMENT OF THE AIR FORCE BMO

FIGURE
A5-1

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c. Low-Strength Surficial Soil: The roads for the MX system will be built on existing ground surface with minimum cut and fill. Therefore, the costs of roads depend on the consistency (or strength) of the surficial soil. In order to evaluate the strength of the surficial soils, cone penetrometer test results were used.

Low-strength surficial soil is defined as soil which will perform poorly (failure of subgrade) as a road subgrade at its present consistency when used directly beneath a road section. In order to define "low strength" using CPT results, the following four approaches were pursued. These approaches are subjective and qualitative and are based on our experience as well as published literature.

- i. Field visual observations: During logging of the borings, the excavation of trenches, test pits, and obtaining surficial soil samples, consistency or compactness of the surficial soils was described qualitatively. A detailed comparison of the CPT results (cone end resistance) and the consistency of the soils was done for different soil types. Using engineering judgement, an upper limit cone resistance was established which encompassed a majority of the soils likely to perform poorly as road subgrades.
- ii. Standard Penetration Test (SPT): SPT is very widely used and accepted in geotechnical engineering practice in this country. A study of available literature revealed that the ratio of cone resistance (q_c , tsf) to Standard Penetration Resistance (N, blows per foot) has a certain range for different soil types. In 1979 Verification studies, limited field SPTs were performed in Reveille-Railroad and Big Smoky sites. Ratios of q_c/N were computed for these tests and were found to be comparable to those reported in literature for similar soil types. Using the relationships applicable to the soils present in the Verification sites, an upper limit of cone resistance, equivalent to midrange of "medium dense" category, (SPT N-value = 10 to 30 blows per foot) was established for defining the "low-strength" surficial soils.
- iii. In-Situ Dry Density: A comparison was made between in-situ dry densities determined from Fugro Drive and Pitcher samples obtained from soil borings and CPT results at the same locations and depths. From this comparison, it was observed that identifiable trends do exist between cone resistance values and soil densities. In this case also, an upper limit of cone resistance equivalent to midrange of "medium dense" category (relative compaction), was established for defining the "low-strength" surficial soils.
- iv. Field CBR Tests: During Verification studies, field CBR tests were performed in Reveille, Railroad, Pine, Wah Wah,

Steptoe, Lake, Spring, Stone Cabin, Hot Creek, and Big Smoky valleys. The procedures for conducting the CBR tests were as described in the U.S. Army Corps of Engineers' Technical Manual (TM) 5-30, pp. 2-86 to 2-96. The test results were compared to Cone Penetrometer Tests performed at the same location. A plot of average field CBR and average cone resistance was prepared and is presented in Figure A5-2. The plot shows the results of the tests in sands only, since tests in gravel and fine-grained soils were very few. Although there is considerable scatter, the majority of the data points fall in a band which is shown in Figure A5-2. From this plot, a range of CPT resistance corresponding to low field CBR values (indicating low-strength surficial soils) was established.

As a result of the preceding four approaches, the following criteria for defining low strength surficial soil were established:

- $q_c < 120$ tsf (117 kg/cm²) for coarse-grained soils
- $q_c < 80$ tsf (78 kg/cm²) for fine-grained soils

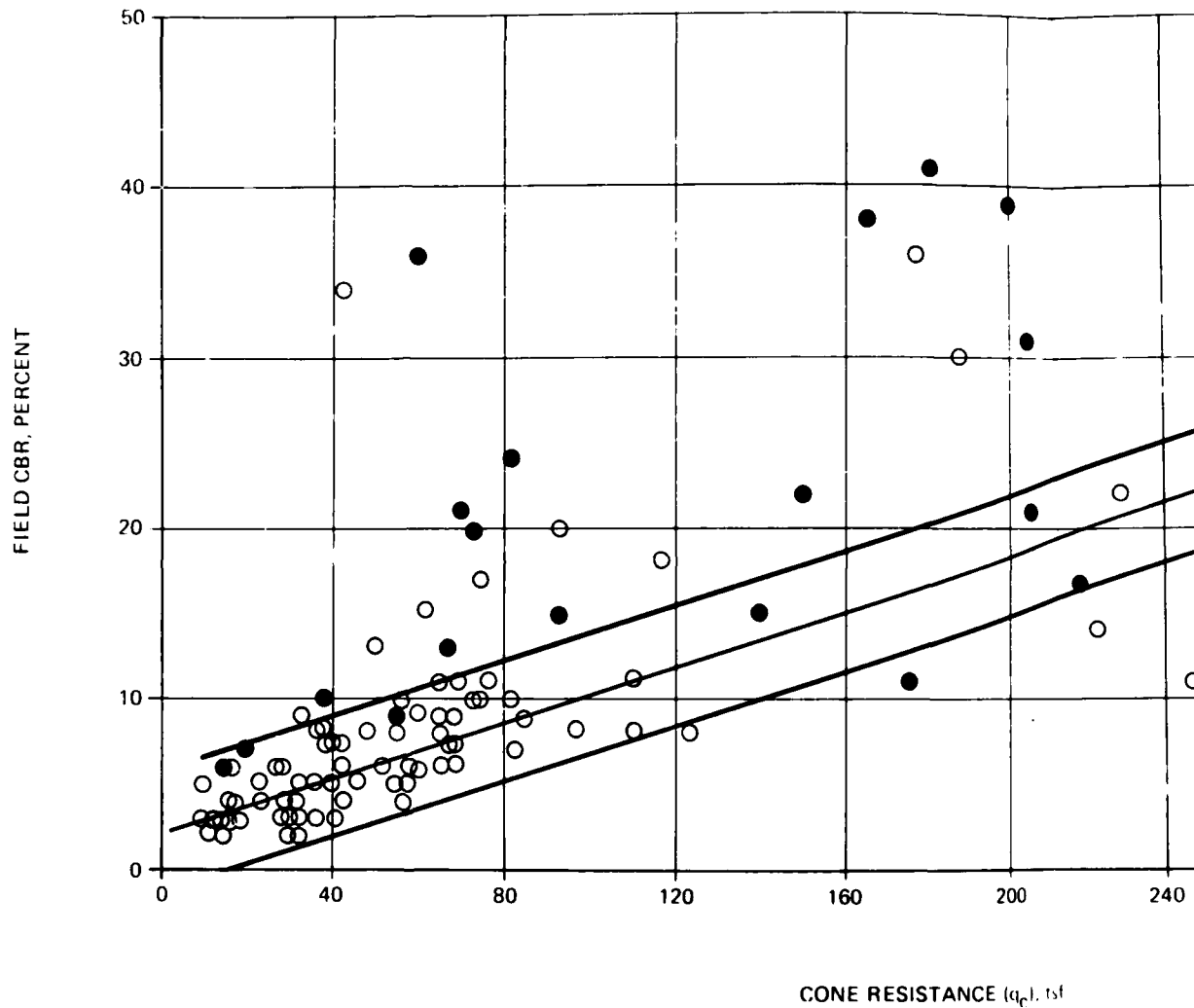
These criteria are preliminary at this stage and may be revised as more data become available from future verification studies. The criteria were used to determine the extent of low strength surficial soil at each CPT location. The results are tabulated in Table 3-2, "Thickness of Low-Strength Surficial Soil."

A5.7.2.3 Subsurface Soils

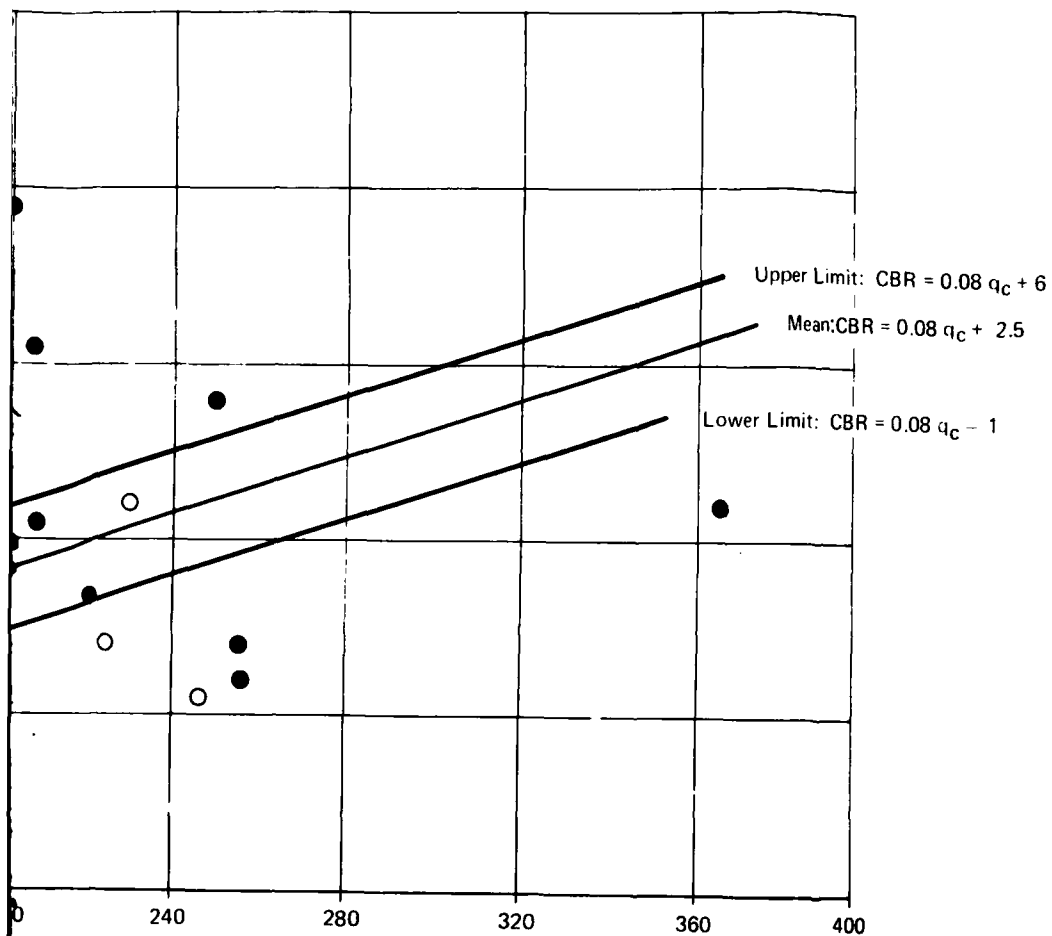
Characteristics of the subsurface soils were developed using data from seismic refraction surveys, borings, trenches, test pits, and laboratory tests.

The soils were divided into coarse-grained and fine-grained soils in two ranges of depth, 0 to 20 feet and 20 to 160 feet (0 to 6 m and 6 to 49 m). Physical and engineering properties of the soils were then tabulated as "Characteristics of Subsurface Soils" (Table 3-4) based on laboratory test results on representative samples. The table includes soil descriptions, Unified Soil Classification System symbols, the estimated subsurface extent of each soil group, comments on the degree of cementation, estimated cobbles content, and ranges of values from the following laboratory and field tests: dry density, moisture content, grain-size distribution, liquid limit, plasticity index, compressional wave velocity, unconfined compression, triaxial compression, and direct shear.

The excavatability and stability of excavation walls of a horizontal or a vertical shelter were evaluated from the subsurface data using seismic velocities, soil types, shear strength, presence of cobbles and boulders, and cementation. Problems encountered during trench and test pit excavations and drilling of borings were also considered in the evaluation.



- NOTES: 1. Data are for sands tested in Big Smoky, Reville Railroad, Pine, Wah Wah, Spring, Lake, Stone Cabin, Reville and Hot Creek Verification Sites.
2. Band between the upper and lower limits includes 74% of all the data points, and includes 85% non-caliche data points.
3. Solid points indicates caliche data points.



q_c), tsf

g, Lake, Stone Cabin,

d includes 85% non

2

RELATIONSHIP BETWEEN FIELD CBR
AND CPT CONE RESISTANCE
VERIFICATION VALLEYS, NEVADA-UTAH

MAINTENANCE INVESTIGATION
DEPARTMENT OF THE AIR FORCE BMO

FIGURE
A5-2

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